

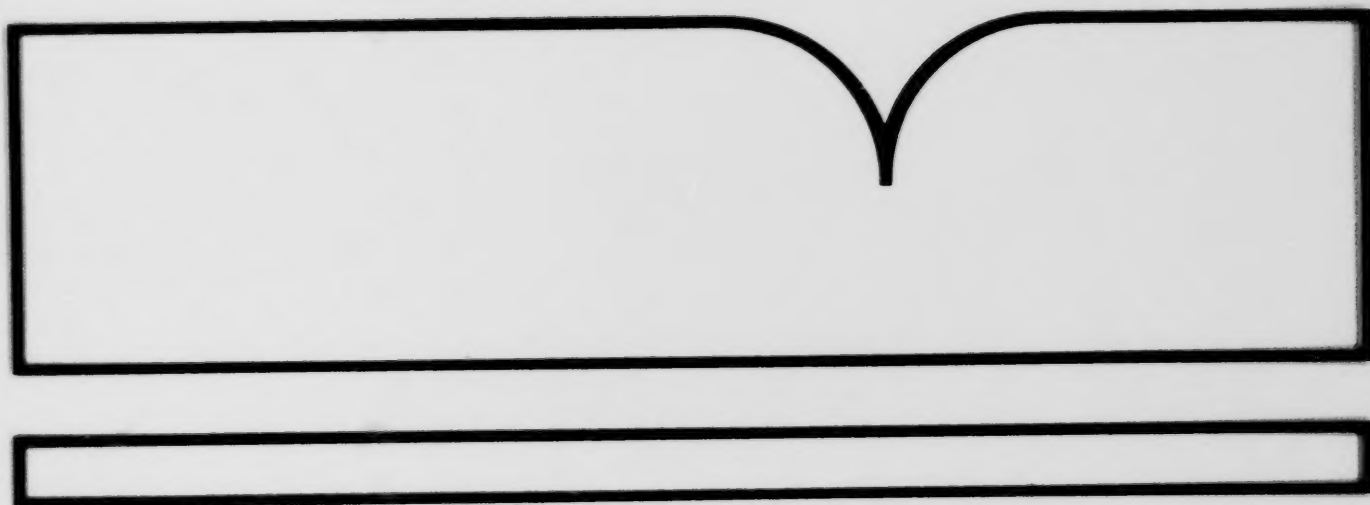
User's Guide for RAM
Second Edition

Aerocomp, Inc., Costa Mesa, CA

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SECOND EDITION

by

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ATMOSPHERIC SCIENCES RESEARCH LABORATORY
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PREFACE

An area of research within the Meteorology and Assessment Division is development, evaluation, validation, and application of models for air quality simulation, photochemistry, and meteorology. The models must be able to describe air quality and atmospheric processes affecting the dispersion of airborne pollutants on scales ranging from local to global. Within the Division, the Environmental Operations Branch adapts and evaluates new and existing meteorological dispersion models and statistical technique models, tailors effective models for recurring user application, and makes these models available through EPA's User's Network for Applied Modeling of Air Pollution (UNAMAP) system.

RAM is a Gaussian-plume model for predicting short-term (one hour to one day) air pollution levels in the near field of multiple point and area source facilities. The model has been upgraded to include a default option which initializes parameters for cases when the model is to be used in a regulatory mode.

Although attempts are made to thoroughly check computer programs with a wide variety of input data, errors are occasionally found. Revisions may be obtained as they are issued by completing and returning the form on the last page of this guide.

The first three sections of this document are directed to managers and project directors who wish to evaluate the applicability of the model to their needs. Sections 4, 5, 6, 7, and 10 are directed to engineers, meteorologists, and other scientists who are required to become familiar with the details of the model. Finally, Sections 8 through 11 are directed to persons responsible for implementing and executing the program.

Comments and suggestions regarding this publication should be directed to:

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Technical questions regarding use of the model should be directed to (919) 541-4564. Users within the Federal Government may call FTS 629-4564. Copies of the user's guide are available from the National Technical Information Service (NTIS), Springfield, VA 22161.

The magnetic tape containing FORTRAN source code for RAM is contained (along with other dispersion models) in UNAMAP (Version 6) (U. S. EPA, 1986), which is available from Computer Products, NTIS, Springfield, VA 22161 (phone number: (703) 487-4763). The NTIS accession number of UNAMAP (Version 6) is PB86-222 361/AS.

ABSTRACT

RAM is an air quality model based on the Gaussian-plume simplification of the diffusion equation which assumes time independence in the input meteorology and concentration. The model is primarily used to determine short-term (one hour to one day) concentrations from point and area sources. A maximum of 250 point sources and 100 area sources can be considered to yield pollutant concentrations at a maximum of 180 receptors. The simulation is done using hourly meteorological data for periods ranging from one hour to one year. A default option is available in the model for regulatory applications. Use of this option automatically sets certain parameters to preassigned values for consistency with the "Guideline on Air Quality Models (Revised)" (EPA, 1986).

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The authors wish to express their appreciation to Russell Lee for helpful comments regarding aspects of the work presented here. Special mention is made to Mr. John Crouch who assembled and corrected the text. Most of the text presented in this document was excerpted from publications dealing with RAM and MPTR over the past few years.

Support of Aerocomp by the Environmental Protection Agency, Contract No. 68-02-4106, is also gratefully acknowledged.

EXECUTIVE SUMMARY

The RAM algorithm is a Gaussian-plume dispersion model that calculates short-term pollutant concentrations from multiple point and/or area sources at a user-specified receptor grid in level or gently rolling terrain. Pollutants considered are relatively non-reactive, such as sulfur dioxide and suspended particulates. Both urban and rural situations can be simulated. In the rural mode, the model uses the Pasquill-Gifford dispersion parameters; in the urban mode, those proposed by Briggs based on the work of Pooler-McElroy are used. Plume rise is calculated following the methods of Briggs and both buoyancy rise and momentum rise are included. For point sources, concentrations are determined using distance crosswind and distance upwind from the receptor to each source. For area sources, the narrow plume simplification of Gifford and Hanna is used with the modification that the area sources are not at ground level, but have an effective height.

Inputs to the model are a set of options selected by the user, source parameters, meteorological data, and receptor information. Using the hourly meteorology, concentrations are calculated for receptor locations either specified by the user or generated by the program. Emissions and source parameters for point or area sources are required inputs. The meteorological data base, and hence the simulation, can vary from one hour to one year. Concentrations for 5 averaging periods can be computed. For long-term runs such as a year, a high-five tabulation can be obtained to determine the highest and second highest concentrations at each receptor for each of five averaging periods. Receptors can be specified by the user or they can be generated by the program. If they are input by the user, receptor name as well as coordinates may be provided on input.

For model execution, the user specifies parameters and options needed for the application. Required parameters are type of pollutant, number of sources, averaging period(s), power-law wind-profile exponents, and whether the urban or rural mode is to be used. Options are included for the treatment

of stack-tip downwash, gradual plume rise, and buoyancy-induced dispersion. The user also specifies types of sources and those that are significant, receptor configuration, characteristics of emission sources, and meteorological inputs. Whether the run is part of a segmented run, outputs desired, and use of the default feature are also specified by the user. The default feature sets parameters and options for regulatory application; final plume rise and momentum plume rise are used as are buoyancy-induced dispersion and stack-tip downwash. Calm wind conditions are treated following the "Calms Processor (CALMPRO) User's Guide" (U. S. EPA, 1984).

Both point and area sources are considered by the model. Their particulars can be included in the run stream or they can be read from disk or tape files. Source coordinates and parameters must be given, as well as emission rates. A total of 250 point sources and 100 area sources are permitted. Of these, up to 25 point sources and 10 area sources can be labeled significant to obtain their contribution at a receptor separately.

As with the data on emissions, the meteorology can be read as part of the input stream, from a file processed by the program RAMMET, or from a file having the format of RAMMET. Surface parameters and mixing height must be present for each simulation hour; the meteorological file is of a variable length from one hour to one year.

Receptors can be specified by the user or they can be generated by the model. If they are input by the user, receptor name as well as coordinates may be provided. If generated by the program, the user selects whether a polar coordinate grid of 180 receptors (36 radials by 5 distances) or a honeycomb receptor configuration is desired. Also, when significant sources are specified, the model selects two receptors downwind of each source where maxima are likely to occur. A total of 180 receptors are permitted.

On output, the model produces printed and disk or tape files. The printed output lists the options and source information including a ranking according to source height; those selected by the user as significant are properly identified. Receptors are next listed with their appropriate coordinates. This is followed by the meteorological parameters as input by the user. Model-calculated concentrations are tabulated by receptor. Various other output files can be obtained.

SECTION 1

INTRODUCTION

The RAM system is based on the Gaussian-plume equation which assumes steady state; it includes dispersion algorithms for both urban and rural situations. The algorithm can be used for short-term (one hour to one day) determination of urban air quality resulting from pollutants released from multiple point and area sources.

The algorithm was first described by Novak and Turner (1976). It is applicable to locations with level or gently rolling terrain where a single wind vector for each hour is a reasonable approximation of the flow over the source area considered. A single mixing height and a single stability class for each hour are assumed representative of the area. The use of RAM is restricted to relatively non-reactive pollutants and is usually applied to sulfur dioxide and total suspended particulates.

Emission information required of point sources consists of source coordinates, emission rate, physical height, stack diameter, stack gas exit velocity, and stack gas temperature. Emission information required of area source squares consists of south-west corner coordinates, source side length, total area emission rate, and effective area source height. Output consists of calculated air pollutant concentrations at each receptor for hourly averaging times and a longer averaging time specified by the user. Contributions to the concentration in the two categories -- point sources and area sources -- are also given on output. The contributions to the concentration from specific point and area sources can be obtained at the option of the user.

Computations are performed hour by hour as if the atmosphere had achieved steady-state condition. Therefore, errors will occur where there is a gradual buildup (or decrease) in concentrations from hour to hour, such as under light wind conditions. Also, with light wind conditions, the definition of wind direction is likely to be inaccurate; variations in the wind flow from

location to location in the area are quite probable.

Briggs' plume-rise equations are used to estimate effective height of point sources. Concentrations from the point sources are determined using distance crosswind and distance upwind from the receptor to each source.

Considerable time is saved in calculating concentrations from area sources by using a narrow plume simplification which considers sources at various distances on a line directly upwind from the receptor to be representative in the crosswind direction of the sources at those distances affecting the receptor. Area source sizes are used as given in the emission inventory in lieu of creating an inventory of uniform elements.

Options are available to allow the use of four different types of receptor locations:

- those with coordinates input by the user,
- those with coordinates determined by RAM and are downwind of significant point and area sources where maxima are likely to occur,
- those with coordinates determined by RAM to give good area coverage of a specific portion of the region, and
- those with coordinates determined by RAM to radially circle a designated point; radial distances are supplied by the user.

Options are also available to limit the output produced.

Urban planners may use RAM to determine the effects of new source locations and control strategies upon short-term air quality. If the input meteorological parameter values can be forecast with sufficient accuracy, control agency officials may use RAM to predict ambient air quality levels, primarily over the 24-hour averaging time, to locate mobile air sampling units, and to assist with emission reduction tactics. Diurnal and day-to-day emission variations must be considered in the source inventory input to the model, especially for control tactics. For most of these uses, the optional feature to assist in locating concentration maxima should be used. Computations are organized so that execution of the program is rapid, thus real-time computations are feasible.

This document is divided into three parts, each directed to a different reader: managers, dispersion meteorologists, and computer specialists. The first three sections are aimed at managers and project directors who wish to evaluate the applicability of the model to their needs. Sections 4, 5, 6, 7, and 10 are directed to dispersion meteorologists or engineers who are required to become familiar with details of the model. Finally, Sections 8 through 11 are directed toward persons responsible for implementing and executing the program. A listing of the FORTRAN source statements is included in Appendix A.

SECTION 2

DATA-REQUIREMENTS CHECKLIST

Model Options

RAM requires data on options, sources, meteorology, and receptors. The user must indicate which of the following options are to be used.

- . stack-tip downwash
- . gradual plume rise
- . buoyancy-induced dispersion
- . input of point and area sources
- . emissions from a previous run of RAM
- . meteorological data on card-image records
- . input of hourly point and area source emissions
- . specification of significant point and area sources
- . input of receptors by specifying coordinates
- . option for RAM to generate receptors downwind of significant point and area sources
- . option for RAM to generate a honeycomb array of receptors
- . input of radial distances to generate a polar coordinate receptor array.

The following are options to omit certain outputs. A number of these options should be used or the program will generate large quantities of printed information.

- . point source list
- . area source list and map
- . emissions with height table
- . resultant meteorological data summary for the averaging period
- . all hourly output (point, area, summaries)
- . hourly point contribution

- . meteorological data on hourly point contributions
- . plume height and distance to final rise on hourly point contributions
- . hourly area contributions
- . meteorological data on hourly area contributions
- . hourly summary
- . meteorological data on hourly summary
- . all averaging period output
- . point averaging period contributions
- . area averaging period contributions
- . averaging period summary
- . average concentrations and high-five table.

The following options can also affect the amount of output.

- . use of a default option
- . use of parts of segmented runs
- . output of partial concentrations to disk or tape
- . output of hourly concentrations to disk or tape
- . output of averaging period concentrations to a file
- . output of averaging period concentrations to card-image records.

Meteorological Data

The meteorological data required for the model are:

- . power-law wind profile exponents for each stability class
- . anemometer height
- . stability class at the hour of measurement
- . wind speed
- . air temperature
- . wind direction
- . mixing height.

Source Emissions Data

The information required of the emissions sources is:

- . coordinates of the point source
- . emission rate for sulfur dioxide
- . emission rate for suspended particulates
- . physical stack height
- . stack gas temperature
- . stack exit diameter
- . stack gas exit velocity
- . coordinates of SW corner of area source
- . side length of area source.

The user may also specify up to 25 point sources and up to 10 area sources as being significant (i.e. sources for which additional information is output).

Receptor Data

The user may also choose to input the coordinates of the receptors (up to 180) or enter one to five radial distances, in which case, RAM will generate 36 receptors for each distance entered. If the user specifies the array boundaries, RAM can also generate its own honeycomb array of receptors. Additionally, RAM can generate receptors downwind of significant point or area sources if the significant source option is used.

SECTION 3

FEATURES AND LIMITATIONS

USES

RAM is primarily a short-term (one hour to one day) urban or rural algorithm used to estimate air quality from point and area sources.

Effects of either control strategies or tactics for specific short-term periods may be examined by users. The expected effect of a proposed source or sources can also be determined. The spatial variation in air quality throughout the urban/rural area, or in a portion of the area, for specific periods can be evaluated readily.

In a forecast or predictive mode such as over a 24-hour period, the algorithm can assist in locating mobile or portable air samplers and can assist with emission reduction tactics. Successful use of RAM in the forecast mode is contingent on the validity of the algorithm assumptions and the ability to accurately forecast both the input meteorological parameter values and the input emission parameter values.

The model has the following added features:

- urban dispersion coefficients recommended by Briggs -- see Figure 7 and Table 8 of Gifford (1976),
- wind-profile exponents for urban and rural situations,
- optional treatment of calm conditions following methods developed by the EPA (1984),
- stack-tip downwash using the algorithm of Briggs (1974),
- momentum-plume rise to treat momentum-dominated plumes as suggested by Briggs (1969),
- buoyancy-induced dispersion following the method of Pasquill (1976), and a

- default option, primarily for regulatory application of the model.

These features were added to satisfy the requirements outlined in "Guideline on Air Quality Models (Revised)" (EPA, 1986). The default option is designed as a convenience for the user to help avoid inadvertent errors in setting the appropriate switches for regulatory use. The reader is cautioned to refer to the current regulatory guidance contained in the "Guideline on Air Quality Models".

Urban and Rural Modes

The urban dispersion parameter values are those recommended by Briggs and included in Figure 7 and Table 8 of Gifford (1976). They have been coded in a subroutine which yields dispersion coefficients as functions of atmospheric stability and downwind distance. Separate urban and rural default wind-profile exponents are used in the model. These exponents are used by the model when the user exercises the default option or when they have not been provided on input. The rural exponents correspond to a surface roughness of about 0.1 meters; the urban exponents result from a roughness of about 1 meter (plus urban heat release influences). For a more detailed discussion of wind profiles, the reader is referred to Irwin (1979).

ALGORITHM ASSUMPTIONS

Gaussian Plumes

Calculations of concentrations from point sources are made for emissions diluted according to the mean wind speed, assuming that the time-averaged plumes over 1-hour periods have Gaussian (normal) distributions perpendicular to the plume centerline in the horizontal and vertical.

Narrow Plume Simplification

Calculations of concentrations from area sources are made by considering that area sources at various distances on a line directly upwind from the receptor are representative of the sources at those distances that affect the receptor. This assumption is best fulfilled by gradual rather than abrupt changes in area emission rates from adjacent area sources. The narrow plume simplification is considered in more detail in the next section.

Meteorological Conditions Representative of the Region

The meteorological input for each hour consists of a value for each of the five parameters: wind direction, wind speed, temperature, stability class, and mixing height, all of which should be representative of the entire region containing the sources and receptors. Mixing height is required only if the atmospheric stability is neutral or unstable.

Steady-state

Calculations are made as if the atmosphere had reached a steady state. Concentrations for a given hour are calculated independently of conditions for the previous hour(s).

Concentration, Sum of Contributions

The total concentration for a given hour for a particular receptor is the sum of the estimated contributions from each source.

Vertical Stability

Except for stable layers aloft, which inhibit vertical dispersion, the atmosphere is treated as a single layer in the vertical with the same rate of vertical dispersion throughout the layer. Complete eddy reflection is assumed both from the ground and from the stable layer aloft given by the mixing layer.

Mixing Height

If vertical temperature soundings are available from a representative location, they should be used with hourly surface temperatures to estimate hourly mixing heights for periods with neutral or unstable stratification. If National Weather Service hourly data are used in the model, two values of mixing height per day are required. These are the maximum and minimum mixing heights as defined by Holzworth (1972). The preprocessor program RAMMET provides a crude interpolation to obtain hourly mixing heights; however, this interpolation does not consider hourly surface temperatures.

Wind Speeds and Directions

Wind speeds and directions should be hourly averages (National Weather Service hourly observations are not really hourly averages, but are averages of a few minutes at the time of the observation, usually 5 to 10 minutes prior to the hour). Input winds should be representative of the entire region. In addition to input winds, the user is required to give the anemometer height.

The increase of wind speed with height is included, based upon a power-law wind profile. The exponent is dependent upon the stability classification and surface roughness. (See Irwin, 1979) For any given hour, winds at various heights above ground are likely to deviate considerably from this climatological mean profile. If user-defined exponents are not supplied, default exponents are used by the model.

There is no inclusion of directional shear with height. This means that the direction of flow is assumed to be the same at all levels over the region. The taller the effective height of the emission, the larger the expected error in the direction of plume transport. Although the effects of surface friction are such that wind direction usually veers (turns clockwise) with height, the thermal effects (in response to the horizontal temperature gradient in the region) may cause increased veering or can overcome the effect of friction and cause backing (turning counterclockwise with height).

National Weather Service observations report wind to the nearest 10° . In order to avoid unrealistic results that would occur from having the wind come from exactly the same direction hour after hour, the program RAMMET, which processes the meteorological data, uses random numbers from 0 to 9 to add from -4° to $+5^\circ$ to the reported wind direction. The purpose of this is to prevent an extreme overestimate of concentration at a point downwind of a source during a period of steady wind when sequential observations show the same direction. Rather than allow the plume centerline to remain in exactly the same position for several hours, the alteration allows for some variation of the plume centerline within the 10° sector. Although this can in no way simulate the actual sequence of hourly events (wind direction to 1° accuracy cannot be obtained from wind direction reported to the nearest 10°), such alterations can be expected to result in concentrations over a period of record to be more representative than those obtained using winds to only the

10° increments reported. (Sensitivity tests of this alteration for single sources have indicated that, where a few hours of unstable conditions are critical to producing high concentrations, the resulting concentrations are extremely sensitive to the exact sequence of random numbers used, such as two wind directions 1° apart versus two wind directions 9° apart. Differences of 24-hour concentrations from a single source by 40 to 50 percent have appeared in the sensitivity tests due to the alteration.) It is, therefore, important to use accurate wind information as input to RAM.

Dispersion Parameter Values

The dispersion parameter values representative for urban areas are those recommended by Briggs and included in Figure 7 and Table 8 of Gifford (1976).

The dispersion parameter values representative for open countryside are the Pasquill-Gifford curves (Pasquill, 1961; Gifford, 1960) which appear in the Workbook of Atmospheric Dispersion Estimates (Turner, 1970). The subroutines used to determine the open countryside parameter values are the same as in the UNAMAP programs MPTER and PTPLU (Pierce and Turner, 1980; Pierce et al., 1982, Chico and Catalano, 1986).

Plume Rise

Plume rise from point sources is calculated using the methods of Briggs (1969, 1971, 1972, 1974, 1975). Although the plume rise from point sources is usually dominated by buoyancy, plume rise due to momentum is also taken into account. Merging of nearby buoyant plumes is not considered. Stack-tip downwash is considered, but building downwash is not.

The variation of effective height of emission from area sources as a function of wind speed is thought to be an important factor in properly simulating dispersion in urban areas. Since this effect is seldom considered in the compilation of urban area emission inventories, it is difficult to have the appropriate parameters to estimate this effect; however, it can be approximated in RAM. The methodology used is explained in Section 5.

Emission Inventories

For similar meteorological conditions, the contribution to the concentration at a receptor from a source is directly proportional to the

emission rate from that source. It is imperative, therefore, to have emissions expressed accurately. Many air pollutant sources vary emissions with time, such as by hour of the day or weekdays versus weekends, and attempts should be made to include these variations. For facilities with detailed emission inventories, hourly emissions can be determined external to RAM and entered via a separate file. Hourly exit velocities are calculated within RAM in proportion to annual exit velocities as hourly emissions are to annual emissions.

Removal or Chemical Reactions

Transformations of a pollutant primarily as a function of time resulting in loss of that pollutant throughout the entire depth of each plume can be approximated by RAM. This is accomplished by an exponential decrease with travel time from the source. The input parameter is the time expected to lose 50% (half-life) of the emitted pollutant. RAM does not have the capability to change this parameter value during a given run. If the loss to be simulated takes place through the whole plume without dependence upon concentration, then the exponential loss may provide a reasonable simulation if the loss rate is realistic. However, if the loss mechanism is selective, such as impaction with features on the ground, reactions with materials on the ground, or dependence on the concentration in a given small parcel of air (requiring consideration of contributions from all sources to this parcel), the loss mechanism built into RAM will not be adequate.

Topographic Influences

RAM is designed for application over level or gently rolling terrain where the assumption of a flat plane used in the algorithm is reasonable. Dispersion parameters for the urban algorithms, are representative of surface roughness over urban areas ($z_0 \approx 1\text{m}$). Dispersion parameters for the rural algorithms are representative of surface roughness over rural areas ($z_0 \approx 0.1\text{ m}$). The algorithms in RAM have no topographical influences incorporated, and some difficulties might be expected in attempting to use the model in terrain situations. Under unstable conditions, plumes may tend to rise over terrain obstructions; under stable conditions, leveled-off plumes may remain at nearly the same mean sea level height, but may be expected to alter the plume path in response to the terrain features, resulting in a

different wind direction locally than that specified for the region.

Fumigation

Fumigation is a transient phenomenon that eliminates the inversion layer containing a stable plume from below, causing mixing of pollutants downward and resulting in uniform concentrations with height beneath the original plume centerline. This phenomenon is not included in the calculations made by RAM. Conditions specified for each hour are calculated as if a steady state had been achieved.

Default Option

A default option is a feature of the model which facilitates compliance with regulatory requirements. For either rural or urban situations, exercising this option overrides other user-input selections and results in the following:

- final plume rise is used (gradual or transitional plume rise is not used for plume height, but it is used to calculate the magnitude of the buoyancy-induced dispersion),
- buoyancy-induced dispersion is used,
- stack-tip downwash is considered,
- default urban or rural wind-profile exponents are used as given in Table 1,
- default vertical potential temperature gradients for stable conditions are used,
- a decay half-life of four hours for SO₂ in urban mode is used, otherwise no decay,
- momentum-plume rise is calculated, and
- calms are treated according to methods developed by the EPA (1984). These are discussed next.

Optional Treatment of Calm Conditions

When the default option is exercised, calm conditions are handled according to methods developed by EPA. A calm hour is indicated in the preprocessed meteorological data as an hour with a wind speed of 1.0 m/sec and

a wind direction the same as the previous hour. When a calm is detected in the meteorological data, the concentrations at all receptors are set to zero. When calculating a multiple hour average concentration, the sum of the hourly concentrations is divided by the number of hours less the number of calm hours, provided that the divisor used in calculating the average is never permitted to be less than 75 percent of the averaging time being considered. This results in the following:

- 3-hour averages are always determined by dividing the sum of the hourly contributions by 3 (i.e., no change from prior methods);
- 8-hour averages are calculated by dividing the sum of the hourly contributions by the number of non-calm hours or 6, whichever is greater;
- 24-hour averages are determined by dividing the sum of the hourly contributions by the number of non-calm hours or 18, whichever is greater; and
- period of record averages are calculated by dividing the sum of all the hourly contributions by the number of non-calm hours during the period of record.

This calms procedure is not available in RAM outside of the default option. If not using the default, calms are treated as 1.0 m/s winds.

Summary

The closer the situation to be simulated agrees with the assumptions stated above, the greater the expectation of reasonable results. The narrow plume simplification is most reasonable for situations where there are no great variations in area emission rates for adjacent area sources.

The higher the effective height of a point source, the greater is the chance for poor results since actual directional shear in the atmosphere, not included in the algorithm, will cause plumes to move in directions different from the direction input to the model. Also, the higher the source height, the greater is the potential for encountering layers in the atmosphere having dispersion characteristics different from those being used. As stated above, it is necessary to properly consider variations in emissions.

Reliable meteorological inputs are also necessary. The light wind situation is most likely to violate assumptions, since variations in the flow over the region are likely to occur, and the slower transport may cause buildup of pollutants from hour to hour. Unfortunately, these are the conditions that are likely to be associated with maximum 3-hour and 24-hour concentrations in urban areas. These light wind situations do not conform to the assumptions of Gaussian steady-state models. The calms processing segment in RAM takes into account these deficiencies by calculating averages for periods longer than three hours in such a way that persistent light wind conditions do not cause a gross overestimate of concentrations at a given receptor.

RAM is not appropriate for making concentration estimates for topographic complications. The greater the departure from relatively flat terrain conditions, the greater the departure from the assumptions of the algorithm.

RAM is most applicable for pollutants that are quite stable chemically and physically. A general loss of pollutant with time can be accounted for by the algorithm. Selective removal or reaction at the plume-ground interface or dependence upon concentration levels may not be well handled by RAM.

SECTION 4

BASIS FOR RAM

The basis for RAM is also discussed in Novak and Turner (1976) which is included in Appendix B. The user may select use of either urban or rural parameters. The urban dispersion parameters σ_y and σ_z are those suggested by Briggs and reported by Gifford (1976). The urban σ 's are functions of distance between source and receptor and of atmospheric stability class where the class is specified by open country conditions.

The dispersion parameters for rural conditions are those of Pasquill-Gifford (Pasquill, 1961; Gifford, 1960), as used in the UNAMAP programs PTPLU, CRSTER, and MPTER. These values are equivalent to the dispersion parameter values given in Figures 3-2 and 3-3 of the Workbook of Atmospheric Dispersion Estimates (Turner, 1970).

DILUTION BY THE WIND

Emissions from continuous sources are assumed to be stretched along the direction of the wind by the speed of the wind. Thus the stronger the wind, the greater the dilution of the emitted plume. To approximate the increase in wind speeds with height from point of measurement to stack top, a power-law increase with height is used. The exponent used is a function of stability.

DISPERSION RESULTS IN GAUSSIAN-DISTRIBUTED CROSS SECTIONS

The time-averaged concentration distributions through a dispersed plume resulting from a continuous emission from a point source or an area element are considered to be Gaussian in both the horizontal and vertical directions. Modification of the vertical distribution by eddy reflection at the ground or at a stable layer aloft is considered. This eddy reflection is calculated by a "folding back" of the portion of the distribution that would extend beyond the barrier if it were absent. This is equivalent to a virtual-image source

beneath the ground (or above the stable layer).

STEADY-STATE CONDITIONS

Concentration estimates are made for each simulated hourly period using the mean meteorological conditions for that hour as if a steady-state condition had been achieved. Steady-state Gaussian plume equations are used for point sources, and the integrations of these equations are used for area sources.

SECTION 5

TECHNICAL DESCRIPTION

CONCENTRATION SUM OF INDIVIDUAL CONTRIBUTIONS

The total concentration of a pollutant at a receptor is taken as the sum of the individual concentration estimates from each point and area source affecting that receptor, that is, concentrations are additive. Concentration estimates for averaging time longer than one hour are determined by linearly averaging the hourly concentrations during the period.

WIND SPEED

In RAM the input wind speed data must include the height above ground of the measurements, and may include the exponents for the wind profile. If no exponents are given in the input, the values in Table 1 are used. The wind speed at the physical stack height h is calculated from:

$$u(h) = u (h/h_a)^p \quad (1)$$

where u is the input wind speed for this hour, h is the height of wind measurement, and the exponent p , for the wind profile, is a function of stability. If $u(h)$ is determined to be less than 1 m/s, it is set equal to 1 m/s.

TABLE 1. EXPONENTS FOR WIND PROFILES

Stability class	URBAN (RAM) exponent	RURAL (RAMR) exponent
A	0.15	0.07
B	0.15	0.07
C	0.20	0.10
D	0.25	0.15
E	0.30	0.35
F	0.30	0.55

PLUME RISE FOR POINT SOURCES

The use of the methods of Briggs to estimate plume rise and effective height of emission are discussed below.

First, actual or estimated wind speed at stack top, $u(h)$, is assumed to be available.

Stack Downwash

To consider stack downwash, the physical stack height is modified following Briggs (1973, p. 4). The h' is found from

$$h' = h + 2\{[v_s/u(h)] - 1.5\}d \text{ for } v_s < 1.5 u(h), \quad (2)$$

$$h' = h \text{ for } v_s \geq 1.5 u(h),$$

where h is physical stack height (meters), v_s is stack gas velocity (meters per second), and d is inside stack-top diameter (meters). This h' is used throughout the remainder of the plume height computation. If stack downwash is not considered, $h' = h$ in the following equations.

Buoyancy Flux

For most plume rise situations, the values of the Briggs buoyancy flux parameter, F (m^4/s^3) is needed. The following equation is equivalent to Briggs' (1975, p. 63) Eq. 12:

$$F = (g v_s d^2 \Delta T)/(4 T_s), \quad (3)$$

where g is the acceleration of gravity, 9.806 m/s^2 , $\Delta T = T_s - T$, T_s is stack gas temperature (Kelvin), and T is ambient air temperature (Kelvin) at stack top.

Unstable or Neutral: Crossover Between Momentum and Buoyancy

For cases with stack gas temperature greater than or equal to ambient air temperature, it must be determined whether the plume rise is dominated by momentum or buoyancy. The crossover temperature difference $(\Delta T)_c$ is determined for 1) F less than 55 or 2) F greater than or equal to 55. If the difference between stack gas temperature and ambient air temperature, ΔT , exceeds or equals the $(\Delta T)_c$, plume rise is assumed to be buoyancy dominated; if the difference is less than $(\Delta T)_c$, plume rise is assumed to be momentum dominated (see below).

The crossover temperature difference is found by setting Briggs' (1969, p. 59) Eq. 5.2 equal to the combination of Briggs (1971, p 1031) Eqs. 6 and 7 and solving for ΔT . For F less than 55,

$$(\Delta T)_c = 0.0297 v_s^{1/3} T_s/d^{2/3}. \quad (4)$$

For F equal to or greater than 55,

$$(\Delta T)_c = 0.00575 v_s^{2/3} T_s/d^{1/3}. \quad (5)$$

Unstable or Neutral: Buoyancy Rise

For situations where ΔT exceeds or is equal to $(\Delta T)_c$ as determined above, buoyancy is assumed to dominate. The distance to final rise x_f (in kilometers) is determined from the equivalent of Briggs' (1971, p. 1031) Eq. 7, and the distance to final rise is assumed to be $3.5x^*$, where x^* is the distance at which atmospheric turbulence begins to dominant entrainment. For F less than 55,

$$x_f = 0.049 F^{5/8}. \quad (6)$$

For F equal to or greater than 55,

$$x_f = 0.119 F^{2/5}. \quad (7)$$

The plume height, H (in meters), is determined from the equivalent of the combination of Briggs' (1971, p. 1031) Eqs. 6 and 7. For F less than 55,

$$H = h' + 21.425 F^{3/4}/u(h). \quad (8)$$

For F equal to or greater than 55,

$$H = h' + 38.71 F^{3/5}/u(h). \quad (9)$$

Unstable or Neutral: Momentum Rise

For situations where the stack gas temperature is less than the ambient air temperature, it is assumed that the plume rise is dominated by momentum. Also if ΔT is less than $(\Delta T)_C$ from Eq. 4 or 5, it is assumed that the plume rise is dominated by momentum. The plume height is calculated from Briggs' (1969, p. 59) Eq. 5.2:

$$H = h' + 3 d v_s/u(h). \quad (10)$$

Briggs (1969) suggests that this equation is most applicable when v_s/u is greater than 4. Since momentum rise occurs quite close to the point of release, the distance to final rise is set equal to zero.

Stability Parameter

For stable situations, the stability parameter s is calculated from the equation (Briggs, 1971, p. 1031):

$$s = g(\partial\theta/\partial z)/T \quad (11)$$

where θ is potential temperature. As an approximation, for stability class E (or 5), $\partial\theta/\partial z$ is taken as 0.02 K/m, and for stability class F (or 6), $\partial\theta/\partial z$ is taken as 0.035 K/m.

Stable: Crossover Between Momentum and Buoyancy

For cases with stack gas temperature greater than or equal to ambient air temperature, it must be determined whether the plume rise is dominated by momentum or buoyancy. The crossover temperature difference $(\Delta T)_C$ is found by setting Briggs' (1975, p.96) Eq. 59 equal to Briggs' (1969, p. 59) Eq. 4.28, and solving for ΔT . The result is

$$(\Delta T)_C = 0.019582 v_s T s^{1/2}. \quad (12)$$

if the difference between stack gas temperature and ambient air temperature (ΔT) exceeds or equals $(\Delta T)_C$, the plume rise is assumed to be buoyancy dominated; if ΔT is less than $(\Delta T)_C$, the plume rise is assumed to be momentum dominated.

Stable: Buoyancy Rise

For situations where ΔT is greater than or equal to $(\Delta T)_C$, buoyancy is assumed to dominate. The distance to final rise (in kilometers) is determined by the equivalent of a combination of Briggs' (1975, p. 96) Eqs. 48 and 59:

$$x_f = 0.0020715 u(h) s^{-1/2}. \quad (13)$$

The plume height is determined by the equivalent of Briggs' (1975, p. 96) Eq. 59:

$$H = h' + 2.6\{F/[u(h) s]\}^{1/3}. \quad (14)$$

The stable buoyancy rise for calm conditions (Briggs, 1975, pp. 81-82 is also evaluated:

$$H = h' + 4 F^{1/4} s^{-3/8}. \quad (15)$$

The lower of the two values obtained from Eqs. 14 and 15 is taken as the final effective height.

Stable: Momentum Rise

When the stack gas temperature is less than the ambient air temperature, it is assumed that the plume rise is dominated by momentum. If ΔT is less than $(\Delta T)_c$ as determined by Eq. 12, it is also assumed that the plume rise is dominated by momentum. The plume height is calculated from Briggs' (1969, p. 59) Eq. 4.28:

$$H = h' + 1.5 \{ (v_s^2 d^2 T) / [4 T_s u(h)] \}^{1/3} s^{-1/6}. \quad (16)$$

The equation for unstable or neutral momentum rise (10) is also evaluated. The lower result of these two equations is used as the resulting plume height.

All Conditions: Distance Less than Distance to Final Rise (Gradual Rise)

Where gradual rise is to be estimated for unstable, neutral or stable conditions, if the distance upwind from receptor to source x (in kilometers), is less than the distance to final rise, the equivalent of Briggs' (1971, p. 1030) Eq. 2 is used to determine height:

$$H = h' + (160 F^{1/3} x^{2/3}) / u(h). \quad (17)$$

This height is used only for buoyancy-dominated conditions; should it exceed the final rise for the appropriate condition, the final rise is substituted instead.

General

In working through the receptors to determine concentrations for a given hour, the first time a source is found to lie upwind of a receptor, the following quantities are determined and stored for that source: $u(h)$, h' , F , H , and x_f . These quantities are then used each time this source is encountered during this hour without recalculation. Only if the upwind receptor-source distance is less than x_f is the effective plume height determined for each occurrence by the last equation mentioned.

BUOYANCY-INDUCED DISPERSION FOR POINT SOURCES

For strongly buoyant plumes, entrainment as the plume ascends through the ambient air contributes to both vertical and horizontal spread, Pasquill (1976) suggests that this induced dispersion, σ_{z0} , can be approximated by the plume rise divided by 3.5.

$$\sigma_{z0} = \Delta h / 3.5 \quad (18)$$

where Δh is either the gradual plume rise as calculated by Eq. 5 for distances less than the distance to final rise, or the final rise for distances greater than that distance. The effective dispersion can then be determined by adding variances:

$$\sigma_{ze} = (\sigma_{z0}^2 + \sigma_z^2)^{1/2}, \quad (19)$$

where σ_{ze} is the effective dispersion, and σ_z is the dispersion due to ambient turbulence levels. At the distance of final rise and beyond, the induced dispersion is constant, based on the height of final rise. At distances closer to the source, gradual-plume rise is used to determine the induced dispersion.

Since in the initial growth phases of release, the plume is nearly symmetrical about its centerline, buoyancy-induced dispersion in the horizontal direction, σ_{y0} , equal to that in the vertical direction, is used,

$$\sigma_{y0} = \Delta h / 3.5 \quad (20)$$

To yield an effective lateral dispersion value, σ_{ye} , this expression is combined with that for dispersion due to ambient turbulence:

$$\sigma_{ye} = (\sigma_{y0}^2 + \sigma_y^2)^{1/2}. \quad (21)$$

EFFLUENT RISE FOR AREA SOURCES

RAM can include in effective height with wind speed for area sources. The input area source height, H_A , is assumed to be the average physical height of the area source plus the effluent rise with a wind speed of 5 m/s. The user specifies the fraction, f , of the input height that represents the physical height, h_p . This fraction is the same for all area sources in the inventory.

$$h_p = f H_A \quad (22)$$

The difference is the effluent rise for a wind speed of 5 m/s

$$\Delta H (u = 5) = H_A - h_p \quad (23)$$

If $f = 1$, there is no rise and the input height is the effective height for all wind speeds. For any wind speed, u , the rise is assumed to be inversely proportional to wind speed and is determined from:

$$\Delta H (u) = \frac{5(H_A - h_p)}{u}, \quad (24)$$

and the effective height is:

$$H_e (u) = h_p + \Delta H(u). \quad (25)$$

CONCENTRATION FORMULAS

Concentrations from Point Sources

The upwind distance x of the point source from the receptor and the crosswind distance, y , of the point source from the receptor are calculated as part of estimates for each source-receptor pair for each simulated hour. Both dispersion parameter values σ_y and σ_z are determined as functions of this upwind distance x and stability class. Figure 1 shows the coordinate system used.

The terms below are used in the equations that follow.

$$\begin{aligned}g_1 &= \exp (-0.5y^2/\sigma_y^2) \\g_2 &= \exp \left[-0.5(z - H)^2/\sigma_z^2 \right] + \exp \left[-0.5(z + H)^2/\sigma_z^2 \right] \\g_3 &= \sum_{N=-\infty}^{\infty} \left\{ \exp \left[-0.5(z - H + 2NL)^2/\sigma_z^2 \right] + \right. \\&\quad \left. \exp \left[-0.5(z + H + 2NL)^2/\sigma_z^2 \right] \right\}\end{aligned}$$

(This infinite series converges rapidly and evaluation with N varying from -4 to $+4$ is usually sufficient.) where

- H = effective height of emissions, meters
- L = mixing height, the top of the unstable layer, meters
- y = crosswind distance, meters
- z = receptor height above ground, meters
- σ_y = standard deviation of plume concentration distribution in the horizontal, meters
- σ_z = standard deviation of plume concentration distribution in the vertical, meters

One of three equations is used to estimate concentrations under various conditions of stability and mixing height. The equation

$$X_p = Qg_1g_2 / (2\pi\sigma_y\sigma_z u) \quad (26)$$

is used for stable conditions or for unlimited mixing where,

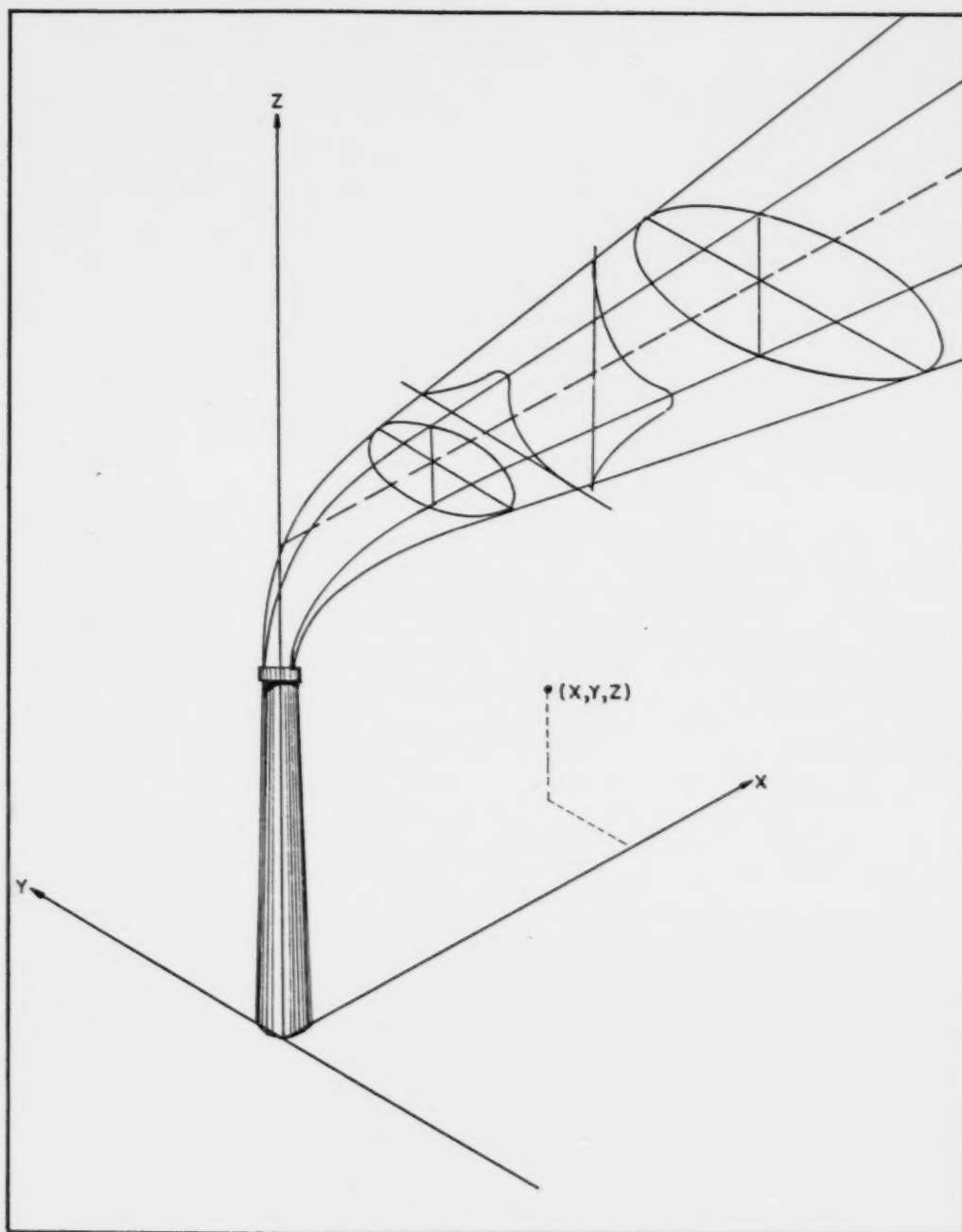


Figure 1. Coordinate system showing Gaussian distributions in the horizontal and vertical.

x_p = ground-level concentration from a single point source, g/m^3 , and
 Q = point source emission rate, g/sec .

In this equation, eddy reflection at the ground is assumed. For unstable or neutral conditions where vertical dispersion is great enough that uniform mixing is assured ($\sigma_z \geq 1.6L$) beneath an elevated inversion, the following equation is used.

$$x_p = Qg_1 / \sigma_y L u (2\pi)^{1/2} \quad (27)$$

(If H or z is above the mixing height, $x_p = 0$.)

For unstable or neutral conditions where uniform mixing is not assured ($\sigma_z < 1.6L$), the following equation is used.

$$x_p = Qg_1 g_3 / (2\pi \sigma_y \sigma_z u) \quad (28)$$

This equation incorporates multiple eddy reflections from the ground and the base of the stable layer aloft.

Concentrations from Area Sources

The total concentration at a receptor from the two-dimensional area source distribution is calculated using the narrow plume simplification discussed by Gifford and Hanna (1971). Figure 2 shows a configuration of area sources and map array scheme. This simplification is assumed because the upwind zone of influence affecting a receptor (an upwind oriented point source plume) is normally quite narrow in comparison with the characteristic length scale for appreciable changes in the magnitude of the area-source emission rate itself. Under these circumstances the two-dimensional integral that expresses the total area-source contribution to concentration at a receptor can be replaced approximately by a one-dimensional integral. This integral involves only:

- knowledge of the distribution of the area-source emission rates along the line in the direction of the upwind azimuth from the receptor location,
- the meteorologically dependent function that specifies the crosswind-integrated concentration in the Gaussian plume from a point source.

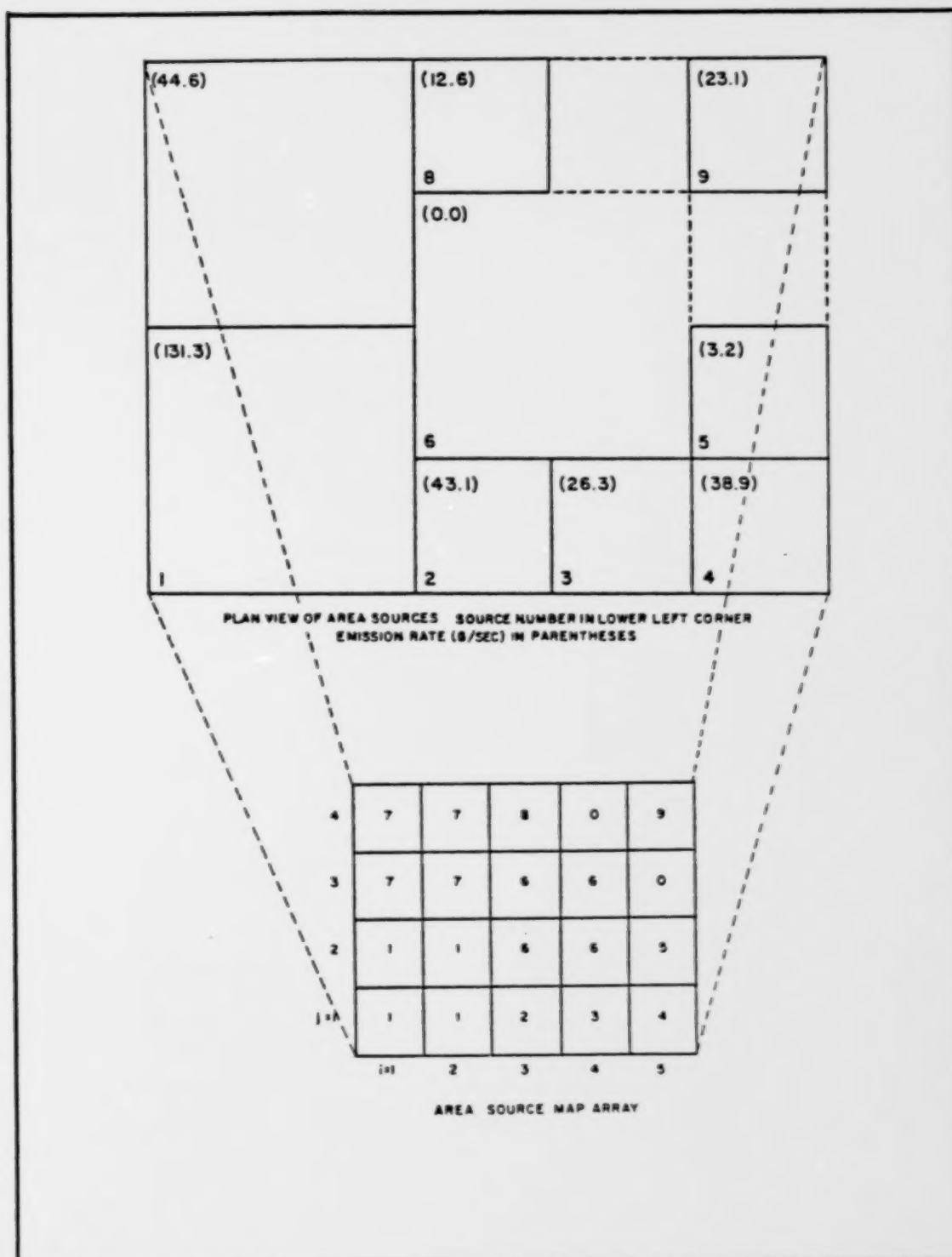


Figure 2. Configuration of area sources and area source map array.

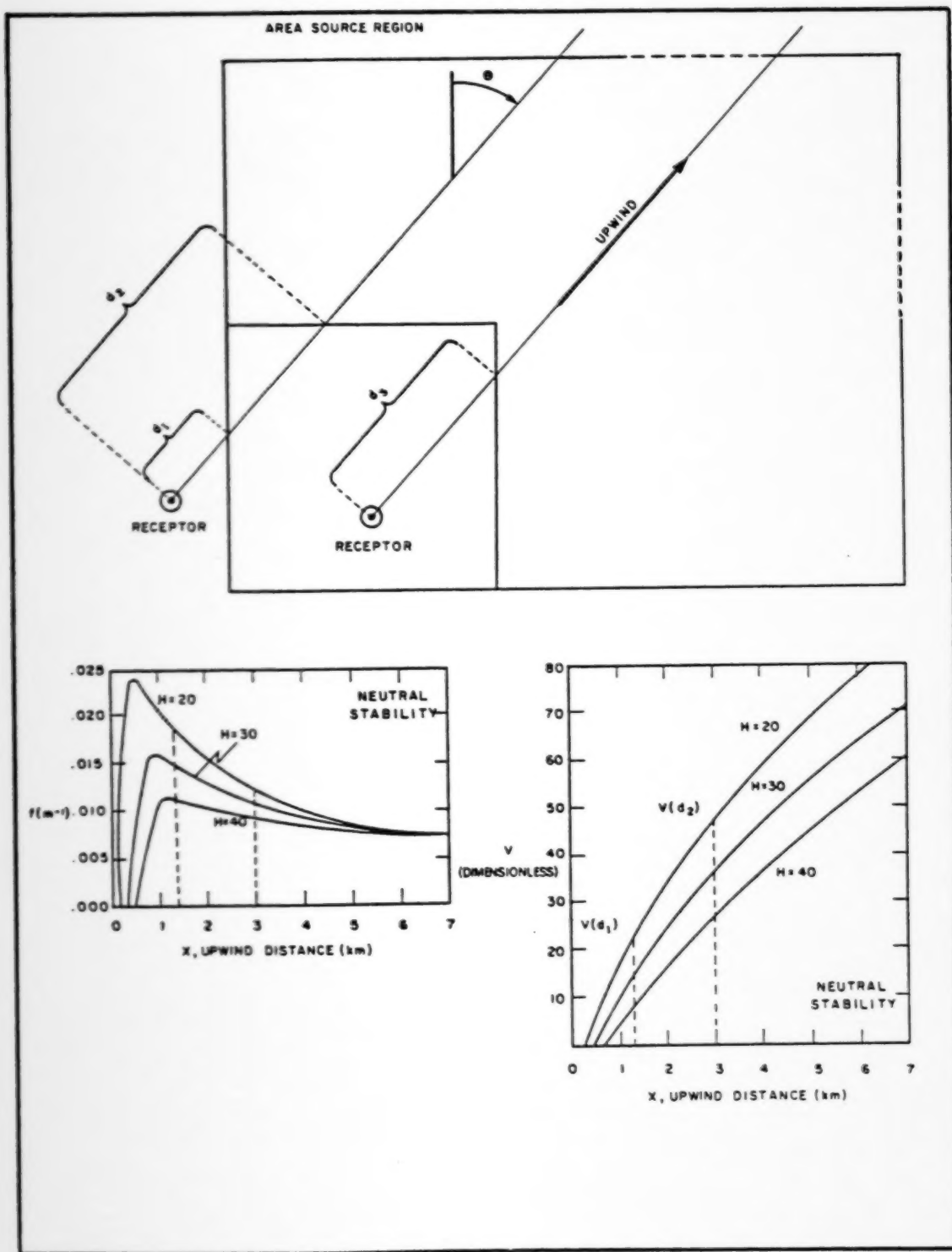


Figure 3. Features of area source estimates.

In using this area source technique, Gifford and Hanna assumed area-source emissions at ground level, allowing integration upwind to be accomplished analytically. In RAM the area sources are allowed to have an effective height, requiring the integration to be accomplished numerically. Figure 3 depicts features of the area source calculations. Equations used to perform the calculations are given in Appendix B. Internal tables of integrations for one to three effective area source heights are calculated at the beginning of each simulated hour using the specific meteorological conditions for that hour. The total concentration from all area sources is determined by performing the integration piecewise over each source in the upwind direction from the receptor until the farthest boundary of the source region is reached.

SECTION 6

VERIFICATION RUN

The example provided in this section serves to verify results of the run; it is expected that the user will implement the model and compare outputs with those given here. A more elaborate example showing uses of the model is given in Section 10. Figure 4 shows the job setup and order of statements. Figure 5 shows the run stream for model execution. Beyond the job control language, there are three title records which are followed by three records containing constants and options for the run. The option record is followed by one record that specifies anemometer height and power-law exponents for six stability categories to extrapolate wind speed to the height of pollutant release. This is followed by source parameters and emissions for 12 point sources and 15 area sources. Significant sources are listed next and are followed by user-specified receptors and meteorology. One averaging period of two hours is specified for the pollutant sulfur dioxide in an urban setting. Concentration contributions from five point sources and ten area sources are desired. The option record indicates that information on point and area sources is present in the input stream. Also, meteorological data is entered via the input stream. Significant source information is specified on input for point sources only. Receptors are specified on input and receptors downwind of significant point and area sources are required. Also, a honeycomb receptor grid is desired. All printed output is needed except average concentrations and high-five tables. The default option (for regulatory application of the model) and printed output to disk or tape are not desired.

Model output can be separated into three sections as shown in Figure 6. The first echoes the options used in the run. Source information for point and area sources are given next with corresponding ranking in order of source significance. A tabulation according to source height is given for the pollutant along with a cumulative fraction for both point and area sources. Significant point and area sources are listed next, followed by receptor

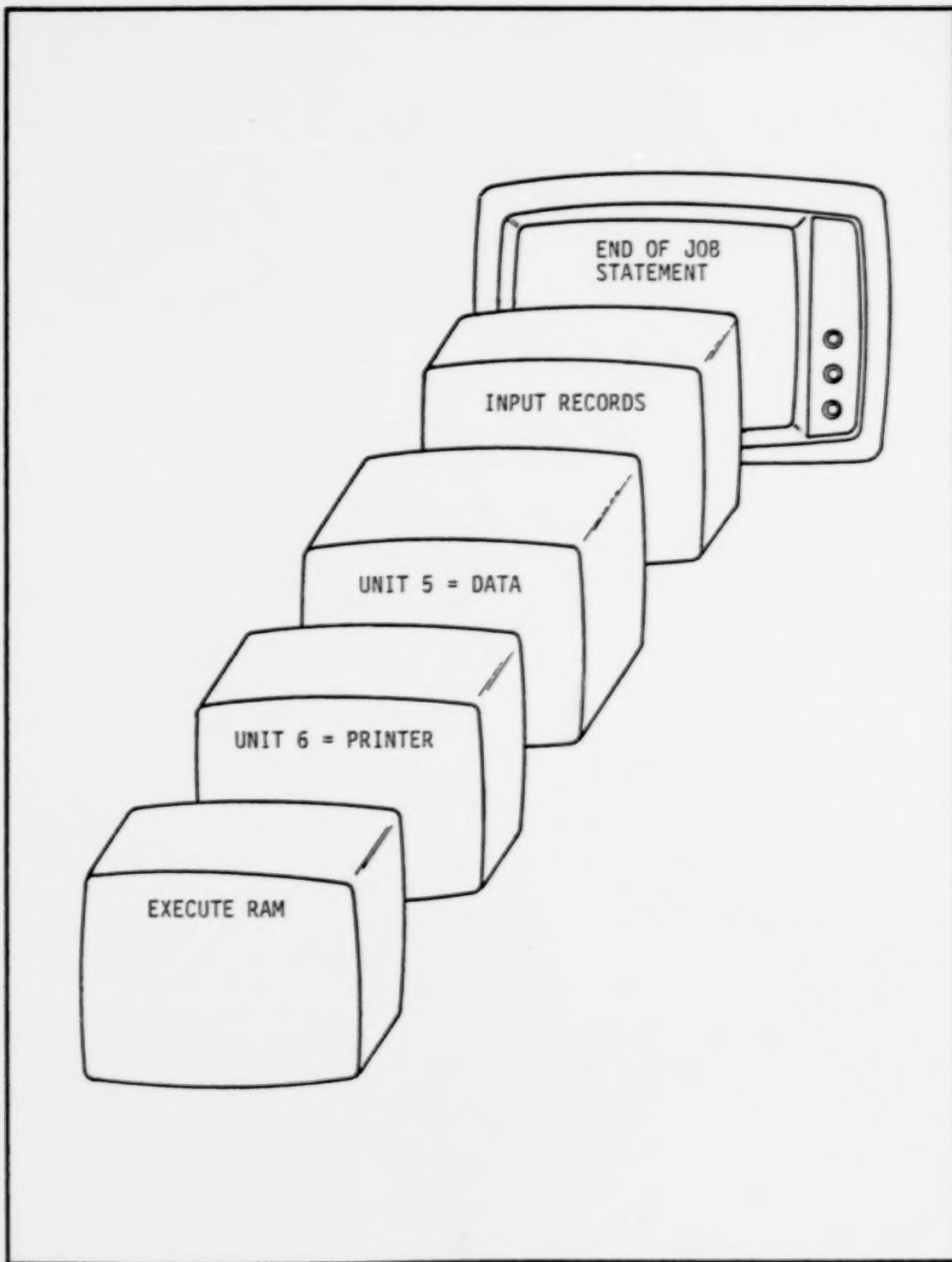


Figure 4. Sample job stream for RAM.

information on user-specified receptors. The meteorological parameters input by the user in record type 18 are listed by the input hour. The next tabulation gives coordinates of two receptors where maxima are expected to occur for each significant point source, either selected by the user or generated by RAM.

Only one significant receptor is given for each area source. If selected by the user, the honeycomb receptor grid generated by RAM is listed next. The locations of significant and honeycomb receptors are averaging-period dependent.

The next section of the output gives concentrations by hour of simulation. First, tables are given for the significant sources; then a summary is given for all sources for the hour. In the example here, the user exercised the option to obtain a concentration summary for the averaging period (two hours), which is provided at the end of the run.

The area source emission inventory has one source defined with a zero emission rate. This is area source 6. Time is saved in executing RAM by specifying areas of zero emission within the area source region that are larger than the smallest area source squares, with squares as large as possible. Note that point sources and receptor locations can be placed anywhere without regard to whether they are inside or outside the area source region.

The input information on area heights of emissions may be confusing to the user. Area source heights may be expected to vary with wind speed, but little information pertaining to this is included in most emission inventories. If the area source emission heights are to remain constant throughout the run with no variation in wind speed, the first variable on card type 10, the fraction of the area source height that is physical height, should be entered as 1. If the user wants to vary the area source height with wind speed, the area source heights should represent the effective emission height from each area at a wind speed of 5 m/sec. The fraction entered as the first variable on card type 10 should approximate as closely as possible the average physical height of each area source when the fraction is multiplied by the input area source height. To most effectively use this feature, the fact that both physical and effective heights are of interest should be known when preparing the emission inventory.

If the height of the emission is the effective height of the area source at a wind speed of 5 m/sec, and if the physical height of the source is a set fraction of this value, which is the same for all sources, it will be possible to consider the variation of effective height of an area source with wind speed in RAM. Otherwise, the fraction will be 1.0, and it will be assumed that the input height of emission is the effective height for all wind speeds.

```

@RUN,R/R 12DBT/70,XXXXXXXXXX/XXX,EOB/SIMRTDBT
@ASG,A EOB*RAM.
@BRKPT PRINT$EOBRAM
@ASG,A EOB*RAM.
@XQT EOB*RAM.SOURCE
TEST RUN: Lucille Bender
EMISSIONS: TEST CITY, 1973
SFC MET DATA: TEST CITY 1973; UPPER AIR: TEST CITY 1973
73,001,01,1,2,3,1,5,10,0,1.609344,2.,0.,14400.
00041101001031111090000000000000001700000004567890
10.,0.15,0.15,0.2,0.25,0.4,0.6
PLANT 1 579.50 4406.75 232.365 13.335 82.9 513.1 3.5 13.7
PLANT 2 575.25 4405.25 150.465 57.005 76.2 464.3 3.2 12.5
PLANT 3 571.25 4407.00 19.005 3.255 25.9 477.6 1.0 15.8
PLANT 4 571.75 4402.25 81.060 28.350 40.8 499.8 2.8 17.6
PLANT 5 579.50 4403.25 26.145 5.145 18.3 533.2 0.6 14.7
PLANT 6 567.14 4400.89 2.56 0. 26.5 505. 1.04 3.81
PLANT 7 564.70 4407.50 36.43 0. 48.8 464. 3.05 18.6
PLANT 8 577.45 4401.35 33.64 0. 26.5 428. 1.68 5.02
PLANT 9 576.75 4400.70 38.8 0. 6. 654. .79 24.89
PLANT 10 580.10 4412.00 299.5 0. 93. 405. 4.88 12.59
PLANT 11 583.0 4400.90 16.74 0. 18.1 506. 1.37 4.23
PLANT 12 574.0 4398.00 226.2 0. 93.6 483. 4.88 12.59
ENDP
AONE 570. 4400. 4. 1.25 0.0 10.
ATWO 574. 4400. 2. 3.05 0.0 10.
ATHREE 576. 4400. 2. 6.25 0.0 12.
AFOUR 578. 4400. 2. 8.85 0.0 15.
AFIVE 578. 4402. 2. 3.15 0.0 10.
ASIX 574. 4402. 4. 0.00 0.0 0.
ASEVEN 570. 4404. 4. 4.25 0.0 15.
AEIGHT 574. 4406. 2. 2.60 0.0 10.
ANINE 578. 4406. 2. 3.10 0.0 12.
ATEN 580. 4406. 2. 2.76 0.0 20.
AELEVEN 582. 4406. 2. .83 0.0 20.
ATWELVE 580. 4404. 2. 1.66 0.0 20.
ATHIRTEEN 582. 4404. 2. 1.90 0.0 20.
AFOURTEEN 580. 4402. 2. .51 0.0 20.
AFIFTEEN 582. 4402. 2. 1.48 0.0 20.
ENDA
1 7
.75, 25., 3, 11.,15.,20.
13., 17.
RECEP 1 566.00 4405.0
RECEP 2 564.00 4401.5
ENDR
2., 570., 580., 4400., 4408.
73,1,1,4,6.17,269.82,33.0,429.11
73,1,2,4,4.63,271.48,23.0,401.7
@BRKPT PRINT$
@FREE EOB*RAM.
@SYM,U EOB*RAM,,FD04PR
@FIN
@@
@@
@@

```

Constants and Options

Source Data

Significant Sources

Receptors

Meteorology

Figure 5. Run stream for the verification run.

OUTPUT FROM URBAN RAM (VERSION 85364)
 AN AIR QUALITY DISPERSION MODEL IN
 SECTION 1. GUIDELINE MODELS
 IN UNAHAP (VERSION 6) DEC 86
 SOURCE: FILE 5 ON UNAHAP MAGNETIC TAPE FROM NTIS.

TEST RUN: LUCILLE BENDER
 EMISSIONS: TEST CITY, 1973
 TWO HOURS NET DATA READ IN ON UNIT FIVE.

GENERAL INPUT INFORMATION

THIS IS THE URBAN VERSION(81352) OF RAM FOR THE POLLUTANT SO2 FOR 1 2-HOUR PERIODS.
 CONCENTRATION ESTIMATES BEGIN ON HOUR- 1, JULIAN DAY- 1, YEAR-1973.
 UNITS - THERE ARE 2.0000000 USER UNITS(INPUT UNITS) PER SMALLEST AREA SOURCE SQUARE SIDE LENGTH(INTERNAL UNIT)
 CONCHG - THERE ARE 1.6093440 KILOMETERS PER USER UNIT
 CONTHG - IT IS CALCULATED THAT THERE ARE 3.2166680 KILOMETERS PER SMALLEST AREA SOURCE SQUARE SIDE LENGTH(INTERNAL UNIT)
 RECEPTOR HEIGHT IS .0000000 METERS

A HALF-LIFE OF 14400.00 (SECONDS) HAS BEEN ASSUMED BY THE USER.

OPTION	OPTION LIST	OPTION SPECIFICATION : 0= IGNORE OPTION 1= USE OPTION
TECHNICAL OPTIONS		
1	NO STACK DOWNWASH	0
2	NO GRADUAL PLUME RISE.	0
3	USE BUOYANCY INDUCED DISPERSION	0
4	NOT USED THIS VERSION	4
INPUT OPTIONS		
5	WILL YOU INPUT POINT SOURCES?	1
6	WILL YOU INPUT AREA SOURCES?	1
7	WILL YOU USE EMISSIONS FROM PREVIOUS RUN? (UNIT 9)	0
8	KEY DATA CH CARDS? (FROM UNIT 11 OTHERWISE)	1
9	READ HOURLY PT. SOURCE EMISSIONS (UNIT 15).	0
10	READ HOURLY AREA SOURCE EMISSIONS (UNIT 16).	0
11	SPECIFY SIGNIF PT. SOURCES.	1
12	SPECIFY SIGNIF. AREA SOURCES.	0
13	NOT USED THIS VERSION	3
RECEPTOR OPTIONS		
14	WILL YOU ENTER RECEPTORS BY SPECIFYING COORDINATES?	1
15	DO YOU WANT RAM TO GENERATE RECEPTORS DOWNWIND OF SIGNIF. PT. SOURCES? (WILL DO SO BY AVG-PERIOD)	1
16	DO YOU WANT RAM TO GENERATE RECEPTORS DOWNWIND OF SIGNIF. AREA SOURCES?(WILL DO SO BY AVG-PERIOD)	1
17	DO YOU WANT RAM TO GENERATE A HONEYCOMB ARRAY OF RECEPTORS TO COVER A SPECIFIC AREA?	1
18	WILL YOU INPUT RADIAL DISTANCES(UP TO 5) TO GENERATE A POLAR COORDINATE RECEPTOR ARRAY	0
19	(26 RECEPTORS FOR EACH DISTANCE) NOT USED THIS VERSION	9
PRINTED OUTPUT OPTIONS		
20	DELETE POINT SOURCE LIST	0
21	DELETE AREA SOURCE LIST AND MAP	0
22	DELETE EMISSIONS WITH HEIGHT TABLE	0

***** Options specified by the
 * user are echoed here

Figure 6. Printed output for the verification run.

23 DELETE RESULANT MET. DATA SUMMARY FOR AVERAGING PERIOD 0
 24 DELETE ALL HOURLY OUTPUT (PT., AREA, & SUMMARIES) 0
 25 DELETE HOURLY POINT CONTRIBUTIONS 0
 26 DELETE MET. DATA ON HR. PT. CONTRIB. 0
 27 DELETE PLUME HT. AND DIST. TO FINAL RISE ON
 HR. PT. CONTRIB.
 28 DELETE HOURLY AREA CONTRIBUTIONS 0
 29 DELETE MET. DATA ON HR. AREA CONTRIB. 0
 30 DELETE HOURLY SUMMARY. 0
 31 DELETE MET. 'DATA ON HOURLY SUMMARY. 0
 32 DELETE ALL AVG-PERIOD OUTPUT. 0
 33 DELETE POINT AVG-PERIOD CONTRIBUTIONS. 0
 34 DELETE AREA AVG-PERIOD CONTRIBUTIONS. 0
 35 DELETE AVG-PERIOD SUMMARY. 0
 36 DELETE AVERAGE CONCENTRATIONS & HI-FIVE TABLE. 1
 37 NOT USED THIS VERSION. 7
 38 SET DEFAULT OPTION. 0

OTHER CONTROL AND OUTPUT OPTIONS:
 39 RUN IS PART OF A SEGMENTED RUN. 0
 40 WRITE PARTIAL CONC. TO DISK OR TAPE (UNIT 10). 0
 41 WRITE HOURLY CONC. TO DISK OR TAPE (UNIT 12). 0
 42 WRITE AVG-PERIOD CONC. TO DISK OR TAPE (UNIT 13). 0
 43 PUNCH AVERAGING-PERIOD CONC. ON CARDS (UNIT 1). 0
 44 NOT USED THIS VERSION. 4
 45 NOT USED THIS VERSION. 5
 46 NOT USED THIS VERSION. 6
 47 NOT USED THIS VERSION. 7
 48 NOT USED THIS VERSION. 8
 49 NOT USED THIS VERSION. 9
 50 NOT USED THIS VERSION. 0

POINT SOURCE INFORMATION

SOURCE	EAST COORD	NORTH COORD	S02(G/SEC) EMISSIONS	PART(G/SEC) EMISSIONS	STACK HT(M)	STACK TEMP(K)	STACK DIAM(M)	STACK VEL(M/SEC)	POTEN. (MICRO G/H*3)	IMPACT EFF	BUOY FLUX F
1 PLANT 1	579.500	4406.750	232.365	13.335	82.90	513.10	3.50	13.70	155.805	370.460	M*14/S**3 176.487
2 PLANT 2	575.250	4405.250	150.465	57.005	76.20	464.30	3.20	12.50	164.901	299.463	115.773
3 PLANT 3	571.250	4407.000	19.035	3.255	25.90	477.60	1.00	15.60	199.064	80.256	14.971
4 PLANT 4	571.750	4402.250	81.050	28.350	40.80	499.60	2.80	17.60	82.104	291.015	139.965
5 PLANT 5	579.500	4403.250	26.145	5.145	18.30	533.20	.60	14.70	818.139	45.144	5.844
6 PLANT 6	567.140	4400.890	2.560	.000	26.50	505.00	1.04	3.81	72.293	47.606	4.241
7 PLANT 7	564.700	4407.500	36.430	.000	43.80	454.00	3.05	18.60	31.983	316.174	156.385
8 PLANT 8	577.450	4401.350	33.640	.000	26.50	428.00	1.63	5.02	461.534	69.507	10.955
9 PLANT 9	576.750	4400.700	33.800	.000	6.00	654.00	.79	24.89	440.911	76.111	21.021
10 PLANT 10	500.100	4412.000	299.500	.000	93.00	405.00	4.83	12.59	405.993	203.266	
11 PLANT 11	503.000	4400.900	16.740	.000	19.10	506.00	1.37	4.23	339.303	52.635	8.193
12 PLANT 12	574.000	4393.000	226.200	.000	93.60	493.00	4.83	12.59	97.496	480.294	289.141

SIGNIFICANT S02 POINT SOURCES

RANK	CHI-MAX (MICROGRAMS/H*3)	SOURCE NO.
1	818.14	5

 * Point and area source data are
 * tabulated in the order the sources
 * were entered. They are then ranked
 * in order of their potential impact.
 * *****

Figure 6. continued

AREA SOURCE INFORMATION									
SOURCE	EAST COORD (USER UNITS)	NORTH COORD (USER UNITS)	SOURCE EMISSIONS (GRAMS/H**2/SEC)	PART EMISSIONS (GRAMS/H**2/SEC)	SIDE LENGTH (USER UNITS)	EFFECTIVE HEIGHT (METERS)	EFFECTIVE SIGNIFICANCE (G/H/SEC)		
2	461.53	8							
3	448.91	9							
4	389.31	11							
5	199.06	3							
6	171.83	10							
7	155.81	1							
8	144.90	2							
9	97.50	12							
10	82.10	4							
11	72.30	6							
12	31.99	7							
1	ADRE	570.000 4400.000	3.0164-008	.0000	4.000	10.000	1.9418-004		
2	ATWO	574.000 4400.000	2.5440-007	.0000	2.000	10.000	9.4759-004		
3	ATHREE	576.000 4400.000	6.0328-007	.0000	2.000	12.000	1.9418-003		
4	AFOUR	578.000 4400.000	8.5425-007	.0000	2.000	15.000	2.7496-003		
5	AFIVE	578.000 4402.000	3.0406-007	.0000	2.000	10.000	9.7866-004		
6	ASIX	574.000 4402.000	.0000	.0000	4.000	.0000	.0000		
7	ASEVEN	570.000 4404.000	1.0256-007	.0000	4.000	15.000	6.6021-004		
8	AEIGHT	574.000 4406.000	2.5097-007	.0000	2.000	10.000	8.0773-004		
9	ANINE	580.000 4406.000	2.9923-007	.0000	2.000	12.000	9.6313-004		
10	ATEN	580.000 4406.000	2.6641-007	.0000	2.000	20.000	8.5749-004		
11	AELEVEN	582.000 4406.000	8.0116-009	.0000	2.000	20.000	2.5787-004		
12	ATWELVE	580.000 4404.000	1.6023-007	.0000	2.000	20.000	5.1574-004		
13	ATHIRTEEN	582.000 4404.000	1.8340-007	.0000	2.000	20.000	5.9030-004		
14	AFOURTEEN	580.000 4402.000	4.9228-009	.0000	2.000	20.000	1.5845-004		
15	AFIFTEEN	582.000 4402.000	1.4286-007	.0000	2.000	20.000	4.5981-004		

AREA SOURCE MAP ARRAY (IA)

4	7	7	8	0	9	10	11
3	7	7	6	6	0	12	13
2	1	1	6	6	5	14	15
1	1	1	2	3	4	0	0
1	2	3	4	5	6	7	

THE ORIGIN IN INTERNAL UNITS IS (284.00, 2199.00)
 THE SIZE OF THE AREA SOURCE ARRAY IS (7, 4)
 RMIN= 205.00 RMAX= 297.00 SMIN= 2200.00 SHAX= 2204.00 (IN INTERNAL UNITS)

SIGNIFICANT SOURCE AREA SOURCES

RANK	Q-LENGTH (G/H/SEC)	SOURCE NO.
1	2.7496-003	4
2	1.9418-003	3
3	9.7266-004	5
4	9.6313-004	9
5	9.4759-004	2

 * The relative location of the
 * sources in the array is shown
 * in this map

 * This ranking lists the area sources in
 * their order of emission significance

Figure 6. continued

6 8.5749-004 10
7 8.0778-004 8
8 6.6021-004 7
9 5.9030-004 13
10 5.1574-004 12

TOTAL S02 EMISSION AND CUMULATIVE FRACTION ACCORDING TO HEIGHT

HEIGHT(M)	EMISSIONS(G/S)	CUMULATIVE FRACTION	TOTAL AREA EMISSIONS(G/S)	CUMULATIVE FRACTION
0 - 5	.00	.000	.00	.000
6 - 10	39.80	.033	10.05	.241
11 - 15	.00	.033	22.45	.780
16 - 20	42.83	.070	9.14	1.000
21 - 25	.00	.070	.00	1.000
26 - 30	55.20	.118	.00	1.000
31 - 35	.00	.118	.00	1.000
36 - 40	.00	.118	.00	1.000
41 - 45	81.06	.187	.00	1.000
46 - 50	36.43	.219	.00	1.000
51 - 55	.00	.219	.00	1.000
56 - 60	.00	.219	.00	1.000
61 - 65	.00	.219	.00	1.000
66 - 70	.00	.219	.00	1.000
71 - 75	.00	.219	.00	1.000
76 - 80	150.47	.348	.00	1.000
81 - 85	232.36	.548	.00	1.000
86 - 90	.00	.548	.00	1.000
91 - 95	525.70	1.000	.00	1.000
96 -100	.00	1.000	.00	1.000
TOTAL	1162.91		41.64	

* For the pollutant selected, the
* emissions are listed cumulatively
* by source height

ADDITIONAL INFORMATION ON SOURCES. POINT SOURCE INFORMATION

EMISSION INFORMATION FOR 12 (HPT) POINT SOURCES HAS BEEN INPUT
5 SIGNIFICANT POINT SOURCES (INSIGP) ARE TO BE USED FOR THIS RUN

USER SPECIFIED 1 (HPT) SIGNIFICANT POINT SOURCES AS LISTED BY POINT SOURCE NUMBER:

7
THE ORDER OF SIGNIFICANCE (IHPS) FOR 25 OR LESS POINT SOURCES USED IN THIS RUN AS LISTED BY POINT SOURCE NUMBER:
7 5 8 9 11

AREA SOURCE INFORMATION

EMISSION INFORMATION FOR 15 (NAS) AREA SOURCES HAVE BEEN DETERMINED BY RAM
10 SIGNIFICANT AREA SOURCES (INSIGA) ARE TO BE USED FOR THIS RUN

NUMBER OF AREA HEIGHT CLASSES (NHT) = 3
REPRESENTATIVE AREA SOURCE HEIGHTS FOR EACH HEIGHT CLASS (HHT) IN METERS = 11.00 15.00 20.00

REPRESENTATIVE AREA SOURCE HEIGHTS FOR EACH HEIGHT CLASS (HHT) IN METERS = 13.00 17.00

REPRESENTATIVE AREA SOURCE HEIGHTS FOR EACH HEIGHT CLASS (HHT) IN METERS = .750

FRACTION OF AREA SOURCE HEIGHT WHICH IS PHYSICAL HEIGHT (FH) = 25.000

LIMIT OF DISTANCE FOR AREA SOURCE INTEGRATION TABLES (XLIM) IN USER UNITS:

BOUNDARIES OF THE AREA SOURCE GRID IN USER UNITS: PHIN= 570.000 RMAX= 524.000 SHIN= 4400.000 SHAX= 4400.000

Figure 6. continued

SIZE(I,RSIZE X I,SSIZE) OF AREA SOURCE MAP ARRAY(IA) IN INTERNAL UNITS = 7 EAST-WEST 'BY 4 NORTH-SOUTH
 THE ORDER OF SIGNIFICANCE (IMAS) FOR 10 OR LESS AREA SOURCE IS LISTED BY AREA SOURCE NUMBER:

4 3 5 9 2 10 6 7 13 12

RECEPTOR INFORMATION

RECEPTOR	IDENTIFICATION	EAST COORD (USER UNITS)	NORTH COORD (USER UNITS)
1 I	RECEP 1	566.000	4405.000
2 I	RECEP 2	564.000	4401.500

 * Receptors input by the user (letter I)
 * following the receptor number) are
 * listed here

Figure 6. continued

INPUT MET DATA FOR 2-HR PERIOD STARTING AT HOUR: 1, YEAR 73, JULIAN DAY 1

HOUR THETA SPEED MIXING TEMP STABILITY
 (DEG) (H/S) HEIGHT(M) (DEG-K) CLASS

1 33.00 6.17 429.11 269.62 4
 2 23.00 4.63 401.70 271.48 4

RESULTANT MET CONDITIONS

WIND DIRECTION= 28.71 RESULTANT WIND SPEED= 5.30
 AVERAGE WIND SPEED= 5.40 AVERAGE TEMP= 270.65
 WIND PERSISTENCE= .99% MODAL STABILITY= 4

SIGNIFICANT POINT RECEPTORS

RECEPTOR #	EAST	NORTH	PREDICTED MAX CONC. (MICROGRAMS/H*3)	MAX. DIST (KM)	EFF. HT (M)	U(PHY HT) (M/SEC)
3 P 7	564.431	4407.008	39.39	.982	156.385	8.026
4 P 7	564.161	4406.517		1.804	156.385	8.026
5 P 5	579.451	4403.160	839.47	.166	32.007	6.281
6 P 5	579.401	4403.069		.331	32.007	6.281
7 P 8	577.376	4401.214	448.58	.249	47.506	6.890
8 P 8	577.301	4401.078		.499	47.506	6.890
9 P 9	576.668	4400.550	619.39	.276	52.296	4.753
10 P 9	576.585	4400.400		.551	52.296	4.753
11 P 11	582.944	4400.798	427.63	.187	35.952	6.263
12 P 11	582.888	4400.696		.374	35.952	6.263

 Two receptors are
 given for each
 significant
 point source

SIGNIFICANT AREA SOURCE RECEPTORS

RECEPTOR # EAST NORTH

13 A 4 578.420 4399.941
 14 A 3 576.426 4399.953
 15 A 5 570.431 4401.961
 16 A 9 578.426 4405.953
 17 A 2 574.431 4399.961
 18 A 10 580.409 4405.920
 19 A 8 574.431 4405.961
 20 A 7 570.672 4403.941
 21 A 13 582.409 4403.920
 22 A 12 580.409 4403.920

 One receptor is given for each
 significant area source in this
 case generated by the program

GENERATED HONEYCOMB RECEPTORS

THE AREA TO BE COVERED BY HONEYCOMB RECEPTORS IS BOUNDED BY:

RMIN= 570.000 RMAX= 580.000 SMIN= 4400.000 SMAX= 4408.000

DISTANCE BETWEEN HONEYCOMB RECEPTORS (GRIDSP) IN USER UNITS= 2.000

RECEPTOR	EAST	NORTH
23 H	572.000	4400.866
24 H	574.000	4400.866
25 H	580.000	4400.866
26 H	571.000	4402.598

 If requested in the options, a
 grid of equally-spaced receptors
 is generated by the program in a
 honeycomb pattern

Figure 6. continued

27 H	573.000	4402.598
28 H	575.000	4402.590
29 H	577.000	4402.598
30 H	572.000	4404.330
31 H	574.000	4404.330
32 H	576.000	4404.330
33 H	578.000	4404.330
34 H	571.000	4406.062
35 H	573.000	4406.062
36 H	577.000	4406.062
37 H	572.000	4407.794
38 F	574.000	4407.794
39 H	576.000	4407.794
40 H	578.000	4407.794
41 H	580.000	4407.794

PLEASE NOTE: THE RECEPTOR NUMBERS AND LOCATIONS GENERATED FOR THIS AVERAGING TIME PERIOD ARE DIFFERENT FROM THOSE GENERATED FOR THE PRECEDING AVERAGING PERIOD.

Figure 6. continued

TEST RUN: LUCILLE BENDER
EMISSIONS: TEST CITY, 1973
THO HOURS MET DATA READ IN ON UNIT FIVE.

502 CONTRIBUTION(MICROGRAMS/H*3) FROM SIGNIFICANT AREA SOURCES 73/ 1 : HOUR 1

HOUR	THETA (DEG)	SPEED (M/S)	MIXING HEIGHT(M)	TEMP (K)	STABILITY CLASS	AREA HTS:	10.508,	14.201,	18.661;	SEPARATION HTS:	12.400,	15.991	TOTAL SIGNIF AREA	TOTAL ALL AREA SOURCES
1	33.00	6.17	429.11	269.82	4	ANEMOM HT: 10.00	PL: .25							
RANK	1	2	3	5	4	5	6	7	8	9	10	12		
SOURCE #	4	3	5	9	2	10	6	7	7	13	12			
RECEP #														
1	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
2	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
3	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
4	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
5	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
6	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
7	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
8	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
9	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
10	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
11	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
12	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
13	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
14	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
15	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
16	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
17	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
18	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
19	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
20	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
21	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
22	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
23	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
24	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
25	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
26	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
27	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
28	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
29	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
30	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
31	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
32	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
33	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
34	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
35	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
36	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
37	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
38	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000

Figure 6. continued

TEST RUN: LUCILLE BENDER
EMISSIONS: TEST CITY, 1973
TWO HOURS MET DATA READ IN ON UNIT FIVE.

S02 SUMMARY CONCENTRATION TABLE (MICROGRAMS/H*3)

SOL SUMMARY CONCENTRATION TABLE(MICROGRAMS/H**3)									
HOUR	THETA (DEG)	SPEED (M/S)	MIXING HEIGHT(H)	TEMP (K)	STABILITY CLASS	73/ 1 : HOUR	1 : HOUR	1 : HOUR	1 : HOUR
1	33.00	6.17	429.11	269.82	4	ANEMOM HT: 10.00	PL: .25		
RECEPTOR NO.									
		EAST		AREA HTS:		10.508, 14.201,		SEPARATION HTS:	
		NORTH		TOTAL FROM SIGNIF POINT SOURCES		TOTAL FROM SIGNIF AREA SOURCES		TOTAL FROM ALL SOURCES	
1 I 0	RECEP 1	566.000	4405.000	.0000	.0000	.0000	.0000	.0000	41
2 I 0	RECEP 2	564.000	4401.500	.0000	.0000	.0000	.0000	.0000	40
3 P 7		564.431	4407.008	35.7987	35.7987	.0000	.0000	35.7987	11
4 P 7		564.161	4406.517	18.2026	18.2026	.0000	.0000	18.2026	15
5 P 5		579.451	4403.160	723.7571	723.7571	1.4215	1.4667	725.2238	1
6 P 5		579.401	4403.069	368.0437	368.0437	1.4665	1.4929	369.5415	5
7 P 8		577.376	4401.214	431.7621	432.2024	2.7281	2.7281	434.9305	3
8 P 8		577.301	4401.078	204.7343	205.1913	2.8280	2.8280	209.0193	7
9 P 9		576.668	4400.550	710.0658	712.6823	2.9602	2.9602	715.6425	2
10 P 9		576.585	4400.400	291.1613	293.7612	3.0427	3.0427	296.8038	6
11 P 11		582.944	4400.798	433.3493	433.3493	.0000	.0483	433.3975	4
12 P 11		582.858	4400.696	194.8263	194.8263	.0000	.0445	194.8708	8
13 A 4		578.420	4399.941	.0837	.0837	3.2543	3.4000	3.4837	24
14 A 3		576.426	4399.953	49.8623	51.6765	3.0883	3.0883	54.7674	9
15 A 5		578.431	4401.961	7.9795	7.9795	1.7745	1.8009	9.7811	21
16 A 9		578.426	4405.953	.0000	.7536	1.1665	1.1665	1.9200	25
17 A 2		574.431	4399.961	.0000	13.8309	1.6338	1.6338	15.4727	17
18 A 10		590.409	4405.920	.0000	.0000	.8464	.8464	.8464	29
19 A 8		574.431	4405.961	.0000	.5625	1.0529	1.0529	1.6154	26
20 A 7		570.872	4403.941	.0000	.0000	.4950	.5121	.5121	33
21 A 13		592.409	4403.920	.0000	.0000	.5493	.6120	.6120	31
22 A 12		590.409	4403.920	.0000	.0000	.5444	.6414	.6414	30
23 H 0		572.000	4400.866	.0000	26.2047	.1834	.3421	26.5468	13
24 H 0		574.000	4400.866	.0000	8.6049	1.2702	1.2702	9.0749	20
25 H 0		570.000	4400.866	.0000	.0000	.2272	.3489	.3489	37
26 H 0		571.000	4402.593	.0000	.0214	.3706	.4090	.5104	34
27 H 0		573.000	4402.593	.0000	19.4521	.2353	.3536	19.6057	14
28 H 0		575.000	4402.593	.0000	9.4123	.1610	.1610	9.5734	22
29 H 0		577.000	4402.593	.0000	29.5180	.3822	.3822	29.9002	12
30 H 0		572.000	4404.330	.0000	.0028	.5696	.5696	.5724	32
31 H 0		574.000	4404.330	.0000	7.2120	.2753	.2753	7.4953	23
32 H 0		576.000	4404.330	.0000	10.9582	.1240	.1240	11.0931	19
33 H 0		573.000	4404.330	.0000	45.5402	.4121	.4121	45.9603	10
34 H 0		571.000	4406.662	.0000	.8200	.3788	.3788	1.1929	27
35 H 0		573.000	4406.662	.0000	.0001	.4319	.4319	.4320	36
36 H 0		577.000	4406.662	.0000	12.9563	.0959	.0959	13.0522	13
37 H 0		572.000	4407.794	.0000	.0000	.1342	.1342	.1342	39
38 H 0		574.000	4407.794	.0000	.0000	.4364	.4364	.4364	35
39 H 0		576.000	4407.794	.0000	.9420	.0000	.0000	.0000	28
40 H 0		578.000	4407.794	.0000	15.2102	.4971	.4971	15.7073	16
41 H 0		593.000	4407.794	.0000	.0000	.2645	.2645	.2645	33

Summary con-
centrations
for each hour
are given per
option 30

TEST RUN: LUCILLE BENDER
EMISSIONS: TEST CITY, 1973
THO HOURS MET DATA READ IN ON UNIT FIVE.

SO2 CONTRIBUTION(MICROGRAMS/H*3) FROM SIGNIFICANT POINT SOURCES 73/ 1 : HOUR 2

HOUR	THETA (DEG)	SPEED (M/S)	MIXING HEIGHT(M)	TEMP (K)	STABILITY CLASS	ANEHOM HT:	10.00	PL:	25	7	8	9	10
2	23.00	4.63	401.70	271.48	4								
		1	2	3	4								
FINAL HT (M)		199.03	169.69	56.06	161.86	34.25	173.95	48.72	59.91	222.05			
FINAL HT (M)		36.91	246.37										
DIST FIN HT (KM)		.978	.835	.265	.894	.156	.128	.240	.341	1.070			
DIST FIN HT (KM)		.194	1.198										
RANK	1	2	3	4	5								
SOURCE #	7	5	8	9	11								
RECEP #													
1	.000	.000	.000	.000	.000				.000	.000			
2	.003	.000	.000	.000	.000				.003	.003			
3	29.231	.000	.000	.000	.000				29.231	29.231			
4	18.745	.000	.000	.000	.000				18.745	18.745			
5	.000	684.939	.000	.000	.000				684.939	684.939			
6	.000	417.785	.000	.000	.000				417.785	417.785			
7	.000	.001	399.482	.000	.000				399.483	435.730			
8	.000	.001	228.979	.000	.000				228.980	265.410			
9	.000	.000	.297	.000	.000				572.106	609.730			
10	.000	.000	.434	.000	.000				294.605	331.675			
11	.000	.000	.000	.000	.000				394.135	394.135			
12	.000	.000	.000	.000	.000				217.816	217.816			
13	.000	.000	.000	.000	.000				5.793	5.793			
14	.000	.001	2.253	104.778	.000				107.032	143.421			
15	.000	.555	.000	.000	.000				.555	3.605			
16	.000	.000	.000	.000	.000				.000	6.777			
17	.000	.000	.000	.000	.000				.000	22.261			
18	.000	.003	.000	.000	.000				.000	.000			
19	.000	.000	.000	.000	.000				.000	.000			
20	.000	.000	.000	.000	.000				.000	.067			
21	.000	.000	.000	.000	.000				.000	.000			
22	.000	.000	.000	.000	.000				.000	.000			
23	.000	.000	.000	.000	.000				.000	.000			
24	.000	.000	.000	.000	.000				.000	.190			
25	.000	.000	.000	.000	.000				.000	14.746			
26	.000	.000	.000	.000	.000				.000	.000			
27	.000	.000	.000	.000	.000				.000	.001			
28	.000	.000	.000	.000	.000				.000	.102			
29	.000	.000	.000	.000	.000				.000	8.552			
30	.000	.000	.000	.000	.000				.000	22.515			
31	.000	.000	.000	.000	.000				.000	.000			
32	.000	.000	.000	.000	.000				.000	.001			
33	.000	.000	.000	.000	.000				.000	13.645			
34	.000	.000	.000	.000	.000				.000	22.552			
TOTAL									TOTAL	TOTAL			
SIGNIF									SIGNIF	SIGNIF			
POINT									POINT	POINT			
SOURCES									SOURCES	SOURCES			

Figure 6. continued

34	.000	.000	.000	.000	.000	.000	14.716
35	.000	.000	.000	.000	.000	.000	.000
36	.000	.000	.000	.000	.000	.000	23.870
37	.000	.000	.000	.000	.000	.000	.000
38	.000	.000	.000	.000	.000	.000	.000
39	.000	.000	.000	.000	.000	.000	43.276
40	.000	.000	.000	.000	.000	.000	.000
41	.000	.000	.000	.000	.000	.000	.001

Figure 6. continued

TEST RUN: LUCILLE BENDER
EMISSIONS: TEST CITY, 1973
THO HOURS NET DATA READ IN ON UNIT FIVE.

S02 CONTRIBUTION(MICROGRAMS/H**3) FROM SIGNIFICANT AREA SOURCES												73/	1 :	1 :	HOUR 2	
HOUR	THETA (DEG)	SPEED (M/S)	MIXING HEIGHT(M)	TEMP (K)	STABILITY CLASS	AREA HTS:				SEPARATION HTS:				TOTAL SIGNIF AREA		TOTAL ALL AREA SOURCES
2	23.00	4.63	401.70	271.48	4	11.366, 15.182, 19.879;				13.282, 17.069						
						ANEMOM HT: 10.00				PL: .25						
RANK	1	2	3	4	5	6	7	8	9	10	11	12				
SOURCE #	4	3	5	9	2	10	8	7	13	12						
RECEP #																
1	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	
2	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	
3	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	
4	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	
5	.000	.000	1.255	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	
6	.000	.000	1.304	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	
7	.000	2.319	.412	.363	.000	.123	.000	.000	.000	.000	.000	.000	.000	.000	.000	
8	.000	2.463	.391	.373	.000	.114	.000	.000	.000	.000	.000	.000	.000	.000	.000	
9	.000	2.894	.090	.511	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	
10	.000	2.995	.077	.509	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	
11	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	
12	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	
13	3.831	.000	.439	.000	.000	.403	.000	.000	.000	.000	.000	.000	.000	.000	.000	
14	.000	3.050	.097	.505	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	
15	.073	.000	1.648	.000	.000	.417	.000	.000	.000	.000	.000	.000	.000	.000	.000	
16	.000	.000	.000	1.513	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	
17	.000	.000	.000	.000	1.596	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	
18	.000	.000	.000	.000	.000	1.030	.000	.000	.000	.000	.000	.000	.000	.000	.000	
19	.000	.000	.000	.000	.000	.000	1.361	.000	.000	.000	.000	.000	.000	.000	.000	
20	.000	.000	.000	.000	.000	.000	.000	.639	.000	.000	.000	.000	.000	.000	.000	
21	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	
22	.000	.000	.000	.000	.000	.364	.000	.000	.000	.000	.000	.000	.000	.000	.000	
23	.000	.000	.000	.000	.000	.000	.451	.133	.000	.000	.000	.000	.000	.000	.000	
24	.000	.000	.000	.000	1.356	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	
25	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	
26	.000	.000	.000	.000	.000	.000	.000	.362	.000	.000	.000	.000	.000	.000	.000	
27	.000	.000	.000	.000	.000	.000	.466	.095	.000	.000	.000	.000	.000	.000	.000	
28	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	
29	.000	.000	.000	.531	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	
30	.000	.000	.000	.000	.000	.000	.000	.636	.000	.000	.000	.000	.000	.000	.000	
31	.000	.000	.000	.000	.000	.000	.494	.000	.000	.000	.000	.000	.000	.000	.000	
32	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	
33	.000	.000	.000	.564	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	
34	.000	.000	.000	.000	.000	.000	.000	.479	.000	.000	.000	.000	.000	.000	.000	
35	.000	.000	.000	.000	.000	.000	.000	.479	.000	.000	.000	.000	.000	.000	.000	
36	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	
37	.000	.000	.000	.000	.000	.000	.000	.159	.000	.000	.000	.000	.000	.000	.000	
38	.000	.000	.000	.000	.000	.000	.526	.000	.000	.000	.000	.000	.000	.000	.000	

Figure 6. continued

TEST RUN: LUCILLE BENDER
EMISSIONS: TEST CITY, 1973
TWO HOURS NET DATA READ IN ON UNIT FIVE.

S02 SUMMARY CONCENTRATION TABLE(MICROGRAMS/H**3)

73/ 1 : HOUR 2

HOUR	THETA (DEG)	SPEED (M/S)	MIXING HEIGHT(M)	TEMP (K)	STABILITY CLASS	RECEPTOR NO.	AREA HTS: NORTH	AREA HTS: EAST	ANEMOM HT: 10.00	PL: .25	SEPARATION HTS: TOTAL FROM SIGNIF AREA SOURCES	TOTAL FROM ALL SOURCES	13.282, 17.069 TOTAL FROM ALL SOURCES	CONCENTRATION RANK
2	23.00	4.63	401.70	271.48	4									
1 I 0	RECEP 1						4405.000	566.000	.0000	.0000	.0000	.0000	.0000	41
2 I 0	RECEP 2						4401.500	564.000	.0025	.0000	.0000	.0000	.0025	39
3 P 7							29.2308	564.431	29.2308	.0000	.0000	.0000	29.2308	11
4 P 7							18.7447	564.161	18.7447	.0000	.0000	.0000	18.7447	16
5 P 5							684.9385	579.451	684.9407	1.9007	1.9007	686.6414	1	1
6 P 5							4403.160	579.401	417.7882	1.9407	1.9407	419.7239	4	4
7 P 8							4401.214	577.376	435.7305	3.2176	3.2176	438.9479	3	3
8 P 8							4401.078	577.301	265.4095	3.3406	3.3406	268.7501	7	7
9 P 9							4400.550	576.668	609.7302	3.4947	3.4947	613.2249	2	2
10 P 9							4400.400	576.585	331.6750	3.5814	3.5814	335.2564	6	6
11 P 11							4400.793	582.944	394.1352	.0000	.1700	394.3052	5	5
12 P 11							4400.696	582.888	217.8158	.0000	.1692	217.9850	8	8
13 A 4							4399.941	578.420	5.8530	4.9734	4.9856	10.8396	20	20
14 A 3							4399.953	578.426	143.4206	3.6524	3.6524	147.0729	9	9
15 A 5							4401.961	578.431	3.6050	2.1820	2.1820	5.7870	23	23
16 A 9							4405.953	578.426	8.7774	1.5130	1.5130	10.2905	21	21
17 A 2							4399.961	574.431	22.2611	1.5960	1.5960	23.8571	13	13
18 A 10							4405.920	580.409	.0000	1.0770	1.0770	1.0770	25	25
19 A 8							4405.961	574.431	.0000	1.3605	1.3605	1.3605	24	24
20 A 7							4403.941	570.872	.0670	.6390	.6566	.7236	30	30
21 A 13							4403.920	582.409	.0000	.7092	.8604	.8604	28	28
22 A 12							4400.866	572.000	.0000	.9336	.7921	.7921	26	26
23 H 0							4400.866	574.000	.1903	1.0191	1.0191	1.0191	27	27
24 H 0							4400.866	574.000	14.7456	1.3561	1.3561	16.1017	17	17
25 H 0							4402.593	571.000	.0000	.2621	.4739	.4739	36	36
26 H 0							4402.593	573.000	.0005	.5115	.5115	.5115	33	33
27 H 0							4402.593	575.000	.1024	.7108	.7108	.8131	29	29
28 H 0							4402.593	577.000	8.5524	.0000	.0000	8.5524	22	22
29 H 0							4402.593	572.000	22.5152	.5312	.5312	23.0464	15	15
30 H 0							4404.330	572.000	.0000	.6356	.6356	.6356	31	31
31 H 0							4404.330	574.000	.0011	.4943	.4943	.4955	34	34
32 H 0							4404.330	576.000	13.8445	.0000	.0000	13.8445	19	19
33 H 0							4404.330	578.000	.0000	.5631	.5631	23.1156	14	14
34 H 0							4406.082	571.000	14.7163	.4789	.4789	15.1952	18	18
35 H 0							4405.062	573.000	.0000	.4789	.4789	.4789	35	35
36 H 0							4406.062	577.000	23.0704	.0000	.0000	23.8704	12	12
37 H 0							4407.794	572.000	.0000	.1591	.1591	.1591	38	38
38 H 0							4407.794	574.000	.0000	.5260	.5260	.5260	32	32
39 H 0							4407.794	576.000	.0001	.0000	.0000	.0000	40	40
40 H 0							4407.794	578.000	43.2750	.5992	.5992	43.0750	10	10
41 H 0							4407.794	580.000	.0013	.3073	.3073	.3086	37	37

Figure 6. continued

TEST RUN: LUCILLE BENDER
EMISSIONS: TEST CITY, 1973
TWO HOURS MET DATA READ IN

2-HOUR AVERAGE SO2 CONTRIBUTION(MICROGRAMS/M**3) FROM SIGNIFICANT POINT SOURCES

ANEMOM HT: 10. PL: A- .15 B- .15C- .20 D- .25 E- .40 F- .60

73/ 1 START HOUR: 1

TOTAL SIGNIF POINT	TOTAL ALL POINT SOURCE\$
--------------------------	--------------------------------

SOURCE #	7	5	8	9	11
1	.000	.000	.000	.000	.000
2	.001	.000	.000	.000	.001
3	32.515	.000	.000	.000	32.515
4	18.474	.000	.000	.000	18.474
5		704.348	.000	.000	704.348
6	.000	392.917	.000	.000	392.917
7	.000	.179	415.444	.000	415.622
8	.000	.233	216.625	.000	216.857
9	.000	.669	4.122	636.895	661.086
10	.000	.091	4.934	287.898	292.923
11	.000	.000	.000	.000	413.742
12	.000	.000	.000	.000	206.321
13	.000	2.939	.000	.000	2.939
14	.000	.268	7.879	70.300	78.447
15	.000	.000	.000	.000	4.267
16	.000	.000	.000	.000	.000
17	.000	.000	.000	.000	.000
18	.000	.000	.000	.000	.000
19	.000	.000	.000	.000	.000
20	.000	.000	.000	.000	.000
21	.000	.000	.000	.000	.000
22	.000	.000	.000	.000	.000
23	.000	.000	.000	.000	.000
24	.000	.000	.000	.000	.000
25	.000	.000	.000	.000	.000
26	.000	.000	.000	.000	.011
27	.000	.000	.000	.000	.000
28	.000	.000	.000	.000	.000
29	.000	.000	.000	.000	.000
30	.000	.000	.000	.000	.000
31	.000	.000	.000	.000	.000
32	.000	.000	.000	.000	.000
33	.000	.000	.000	.000	.000
34	.000	.000	.000	.000	.000
35	.000	.000	.000	.000	.000
36	.000	.000	.000	.000	.000
37	.000	.000	.000	.000	.000
38	.000	.000	.000	.000	.000
39	.000	.000	.000	.000	.000
40	.000	.000	.000	.000	.000
41	.000	.000	.000	.000	.000

 ** As requested in option 33, **
 ** point source contributions **
 ** for the averaging period **
 ** are listed here **

As requested in option 33,
point source contributions
for the averaging period
are listed here

Figure 6. continued

TEST RUN: LUCILLE BEIDER
EMISSIONS: TEST CITY, 1973
THO HOURS MET DATA READ IN ON UNIT FIVE.

2-HOUR AVERAGE SO2 CONTRIBUTION(MICROGRAMS/H*H*3) FROM SIGNIFICANT AREA SOURCES														73/ 1 START HOUR: 1
RANK	1	2	3	4	5	6	7	8	9	10	11	12	TOTAL SIGNIF AREA	TOTAL ALL AREA SOURCES
SOURCE #	1	2	3	4	5	6	7	8	9	10	11	12		
RECEP #	1	2	3	4	5	6	7	8	9	10	11	12		
1	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
2	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
3	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
4	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
5	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
6	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
7	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
8	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
9	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
10	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
11	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
12	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
13	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
14	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
15	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
16	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
17	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
18	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
19	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
20	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
21	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
22	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
23	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
24	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
25	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
26	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
27	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
28	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
29	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
30	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
31	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
32	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
33	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
34	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
35	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
36	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
37	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
38	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
39	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
40	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000
41	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000	.000

Figure 6. continued

TEST RUN: LUCILLE BENDER
EMISSIONS: TEST CITY, 1973
THO HOURS NET DATA READ IN ON UNIT FIVE.

2-HOUR AVERAGE SO2 SUMMARY CONCENTRATION TABLE(MICROGRAMS/H*H*3)										73/ 1	START HOUR: 1
RECEPTOR NO.	EAST	NORTH	15 B-	15 C-	20 D-	25 E-	40 F-	60	TOTAL FROM ALL SOURCES	CONCENTRATION RANK	
			TOTAL FROM SIGNIF ALL SOURCES	TOTAL FROM POINT SOURCES	TOTAL FROM SIGNIF ALL SOURCES	TOTAL FROM POINT SOURCES	TOTAL FROM SIGNIF ALL SOURCES	TOTAL FROM POINT SOURCES			
1 X 0	RECEP 1	566.000	4405.000	.0000	.0000	.0000	.0000	.0000	.0000	41	
2 X 0	RECEP 2	564.000	4401.500	.0013	.0013	.0000	.0000	.0000	.0013	40	
3 P 7		564.431	4407.003	32.5148	32.5148	.0000	.0000	.0000	32.5148	11	
4 P 7		564.161	4406.517	18.4737	18.4737	.0000	.0000	.0000	18.4737	15	
5 P 5		579.451	4403.160	704.3470	704.3489	1.6611	1.6637	706.0326		1	
6 P 5		579.401	4403.069	392.9156	392.9184	1.6936	1.7168	394.6352		5	
7 P 8		577.376	4403.214	415.6223	433.9664	2.9728	2.9728	436.9392		3	
8 P 8		577.301	4401.078	216.8572	235.3004	3.0643	3.0643	238.3847		7	
9 P 9		576.668	4400.550	641.0858	661.2062	3.2274	3.2274	664.4337		2	
10 P 9		576.585	4400.400	292.9232	312.7181	3.3120	3.3120	316.0301		6	
11 P 11		592.944	4400.798	413.7422	413.7422	.0000	.0000	413.6514		4	
12 P 11		582.888	4400.696	206.3210	206.3210	.0000	.0000	206.4279		8	
13 A 4		576.420	4399.641	2.9305	2.9683	4.1139	4.1933	7.1616		24	
14 A 3		576.426	4399.653	78.4472	97.5496	3.3706	3.3706	100.9202		9	
15 A 5		578.431	4401.961	4.2674	5.7926	1.9723	1.9914	7.7641		23	
16 A 9		578.426	4405.953	.0000	4.7655	1.3397	1.3397	6.1052		25	
17 A 2		574.431	4399.961	.0000	18.0500	1.6149	1.6149	19.6649		14	
18 A 10		550.409	4405.920	.0000	.0000	.9617	.9617	.9617		28	
19 A 8		574.431	4405.961	.0000	.0000	1.2067	1.2067	1.4850		27	
20 A 7		570.872	4403.941	.0000	.0335	.5670	.5943	.6179		31	
21 A 13		582.409	4403.920	.0000	.0000	.6292	.7362	.7362		30	
22 A 12		550.409	4403.920	.0000	.0000	.7640	.8303	.8303		29	
23 H 0		572.800	4400.866	.0000	13.1975	3.562	.5671	13.7646		17	
24 H 0		574.000	4400.865	.0000	11.6752	1.3131	1.3131	12.9833		18	
25 H 0		580.000	4400.866	.0000	.0000	.2447	.4113	.4113		37	
26 H 0		571.000	4402.593	.0000	.0110	.3662	.5002	.5112		33	
27 H 0		573.000	4402.593	.0000	9.7772	.3682	.5322	10.3994		20	
28 H 0		575.000	4402.593	.0000	8.9524	.0008	.0005	9.0529		21	
29 H 0		577.000	4402.593	.0000	26.0166	.4567	.4567	26.4733		13	
30 H 0		572.000	4404.330	.0000	.0014	.6026	.6026	.6040		32	
31 H 0		574.000	4404.330	.0000	3.6096	.3548	.3548	3.9944		26	
32 H 0		576.000	4404.330	.0000	12.4064	.0624	.0624	12.4638		19	
33 H 0		578.000	4404.330	.0000	34.0503	.4976	.4976	34.5379		10	
34 H 0		571.000	4406.062	.0000	7.7601	.4289	.4289	8.1970		22	
35 H 0		573.000	4406.062	.0000	.0301	.4554	.4554	.4555		36	
36 H 0		577.000	4406.062	.0000	18.4134	.0479	.0479	18.4613		16	
37 H 0		572.000	4407.794	.0000	.0000	.1466	.1466	.1466		39	
38 H 0		574.000	4407.794	.0000	.0000	.4312	.4312	.4812		36	
39 H 0		576.000	4407.794	.0000	.0000	.0000	.0000	.4711		35	
40 H 0		578.000	4407.794	.0000	.0000	.0000	.0000	29.7912		12	
41 H 0		559.000	4407.794	.0000	29.2430	.5432	.5432	29.7912		33	
					.0007	.2059	.2059	.2059			

THIS RUN HAS TERMINATED NORMALLY.

A summary is
provided for
all sources for
the averaging
period at the
end of the run

SECTION 7

USES OF RAM

RAM simulates pollutants from point and area sources in urban or rural settings over periods of one hour to one year. The meteorological data can be entered on cards, with one card for each simulated hour, or on magnetic media by using option 8. General emission information can also be on the input stream or from disk or tape files using option 9 or 10.

Point and area sources are specified by options 5 and 6. The locations of receptors may be specified by the user (option 14).

The use of options 15 and 16 to locate additional receptors downwind of significant point and area sources assists in determining locations of maximum concentration. Since the resultant wind vector for the averaging period selected is used to determine the direction of these receptors from the sources, averaging times that contain significant wind shifts may result in misleading averages. The user should note that when options 15 and 16 are used to locate receptors downwind from significant sources, the locations for these receptors will shift for each averaging period, dependent upon the resultant meteorological conditions for each period. Therefore, receptors with the same numbers will be at different locations for different averaging times.

If the user desires to cover a specific area so that pollutant patterns are discerned, option 17 can be used to place additional receptors. The pattern used is such that adjacent receptors are equidistant; this is referred to as a honeycomb pattern. The distance between receptors is selected by the user as are the boundaries of the area covered. If the boundaries are entered as zeros, the boundaries are set to coincide with the boundaries of the area source map array. Since the honeycomb receptors are set for each averaging time, they may be different from one averaging time to another. The model can be executed for an hour without receptors downwind of significant sources in

order to obtain a list of receptors for good area coverage. Their coordinates can then be input for a longer period run where it is desired to have receptors in fixed positions.

It should be noted that concentration gradients may be very steep, especially those due to point source plumes. Therefore, the addition of more receptors will result in a more complex concentration pattern and some hot spots. The user, when searching for maximum concentrations, must decide on receptor spacing commensurate with resources, analysis time, and the purpose of the project before including additional receptors.

For the typical run, hourly output would be desired, so option 24 should be set for hourly output. If option 24 is not set, no hourly output is printed. The use of option 40 to write partial concentrations onto a disk file should be used only if additional computer analysis is intended using the individual contributions of sources upon particular receptors. Computer programs to perform this analysis must be written by the individual user to suit his or her purpose.

Option 30 is checked only if option 24 is used to obtain hourly summaries. The use of option 30 will print a summary page for each hour. This summary provides the total concentration for each receptor, the contribution to the concentration from all point sources, the contribution to the concentration from all area sources, the contribution from all the significant point sources combined, and the contribution from all the significant area sources. Information that will be obtained by using option 24, but not option 30, are the contributions to the concentrations at each of the receptors from each of the significant sources. The maximum of 10 significant area sources results in an additional page of output per simulated hour. The maximum of 25 significant point sources results in three additional pages of output per simulated hour (one page for every 10 significant point sources or fraction thereof). Unless the concentration contributions are specifically needed for analysis of contributions from particular sources, option 30 should be zero to reduce the quantity of output.

Option 8 would be set to one to enter meteorological data as part of the run stream rather than reading an external file using unit 11. Options 9 and 10 are set to one to enter hourly emissions. If the contribution at a

receptor from particular sources is of interest, and if these particular sources are not high enough to be included in the significant source list from RAM, options 11 and 12 may be used to specify the sources of interest. If option 11 or 12 is used to obtain concentration contributions for the averaging time, it is desirable to leave option 30 off to obtain hourly output.

Option 41 or 42 would not usually be employed unless concentrations at each receptor are required for further analysis or are to be used with graphics software to produce concentration isopleth maps.

SECTION 8

COMPUTER ASPECTS OF THE MODEL

STRUCTURE OF RAM

RAM consists of three sections: preprocessing subroutines, main logic, and output subroutines. Actual source code for the program is included in Appendix A.

Figure 7 is a system flowchart for the model. Inputs are assumed to be from disk files; outputs either go to disk or printer. Options and program control are read from FORTRAN unit 5; processing is then controlled through specifications in this file. If so specified in the control file, meteorology and emissions can be obtained from units 11, 15, and 16, respectively. The program uses two temporary files for intermediate work, but they are not temporary in the JCL sense, i.e., they are not deleted at the end of the job step and should be deleted by the user when they are no longer needed. As the program calculates concentrations, they are averaged and written to units 1, 10, 12, and 13 as noted in the option list. Tabular output is written to unit 6 which is usually the default for printed files.

Section I (page A-22) contains preprocessing subroutines to initialize variables. These subroutines are called to determine dispersion parameter values as functions of stability class and source-receptor distance. The data produced are coefficients and exponents for the various ranges of effective height of emission and are used to determine maximum xu/Q (relative concentration normalized for wind speed) for point sources and distance to maximum concentration for point and area sources as functions of stability class and effective height of emission.

Section J-K (pages A-25 - A-31) process the emission data. Their principal task is to set up the area source map array. The area source map array provides correspondence between locations (referred to by coordinates) and area source

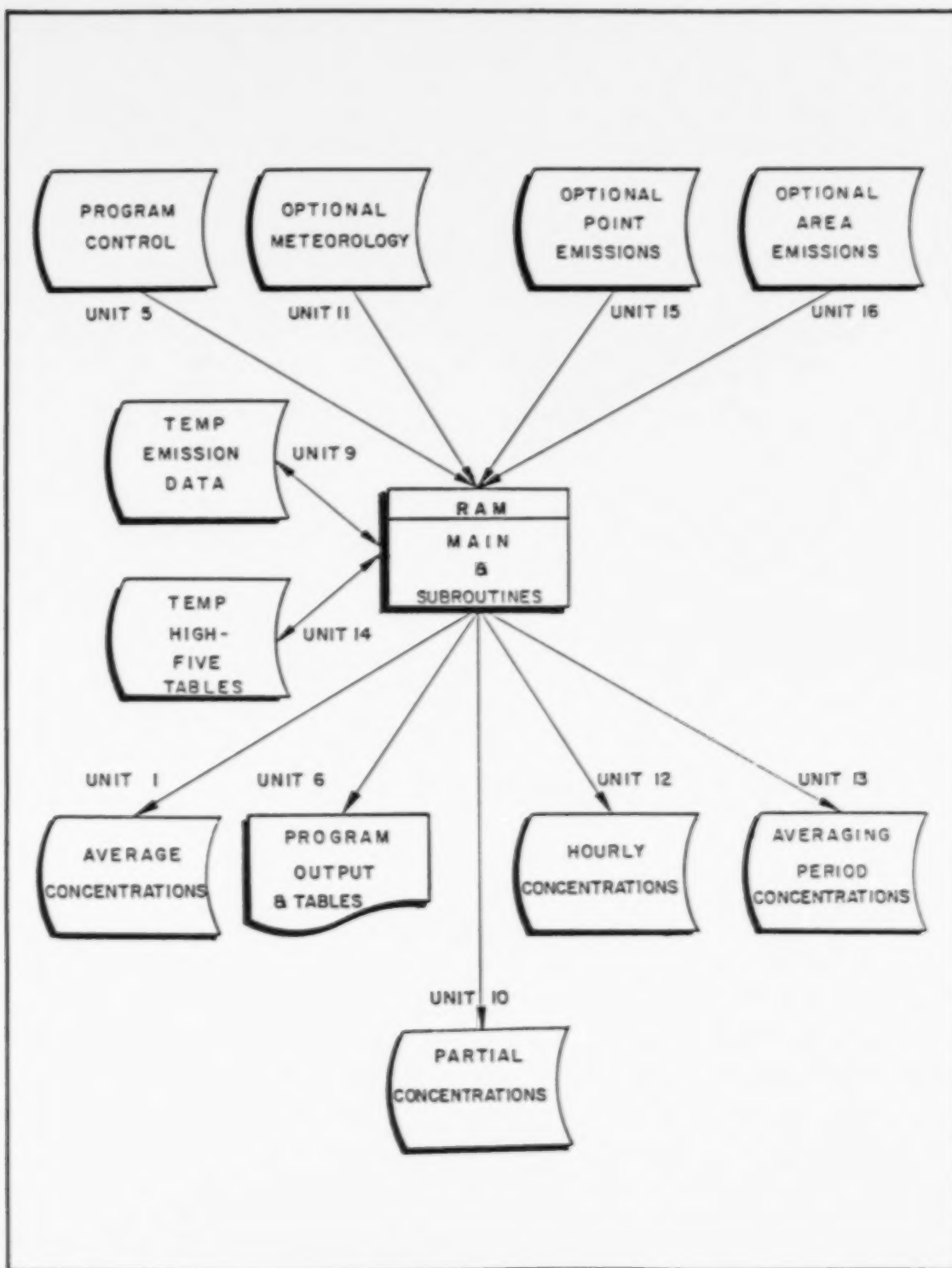


Figure 7. System flow for the model.

number. Other tasks, such as ranking sources according to set criteria, are also accomplished.

RAM expects hourly meteorological input data, including mixing height and stability class. This and other values can be entered in the input stream or from a preprocessed file. The auxiliary program RAMMET can process raw meteorological data into the needed format using hourly surface data and mixing heights from the National Climatic Data Center. Input consists of one year of surface data (one observation per hour) and one maximum and one minimum mixing height per day. RAMMET determines hourly stability and performs interpolations to estimate hourly mixing heights. The output data are organized to produce a single record for each day.

The output subroutines are OUTPT and OUTAV. OUTPT provides hourly concentrations in micrograms per cubic meter, including the contributions from significant point sources along with a summary table. OUTAV provides the same information for the averaging period.

PROGRAM MODULES

The main structure is given in Figure 8. After initialization, the flow is governed by three loops: calendar days, averaging time, and hours. A minimum of one hour and a maximum of 8,784 hours can be processed by the model. A brief description of the main program and subroutines follows.

MAIN - The main program determines X_u/Q maxima and distance to the point of maximum for point sources as functions of stability class and effective height of emissions. Coefficients and exponents relating these two parameters to effective height of emission are determined for various stability and effective height range combinations. These coefficients and exponents, as well as ones for determining the distance of the maximum concentration downwind from the edge of an area source, are calculated for use in the emissions module which processes emission inventory information for later use. An important aspect of this is the construction of the area source map array which allows a correspondence between any location in the area source region and the number of the area source at that location. All source coordinates in units convenient to the user (user units)

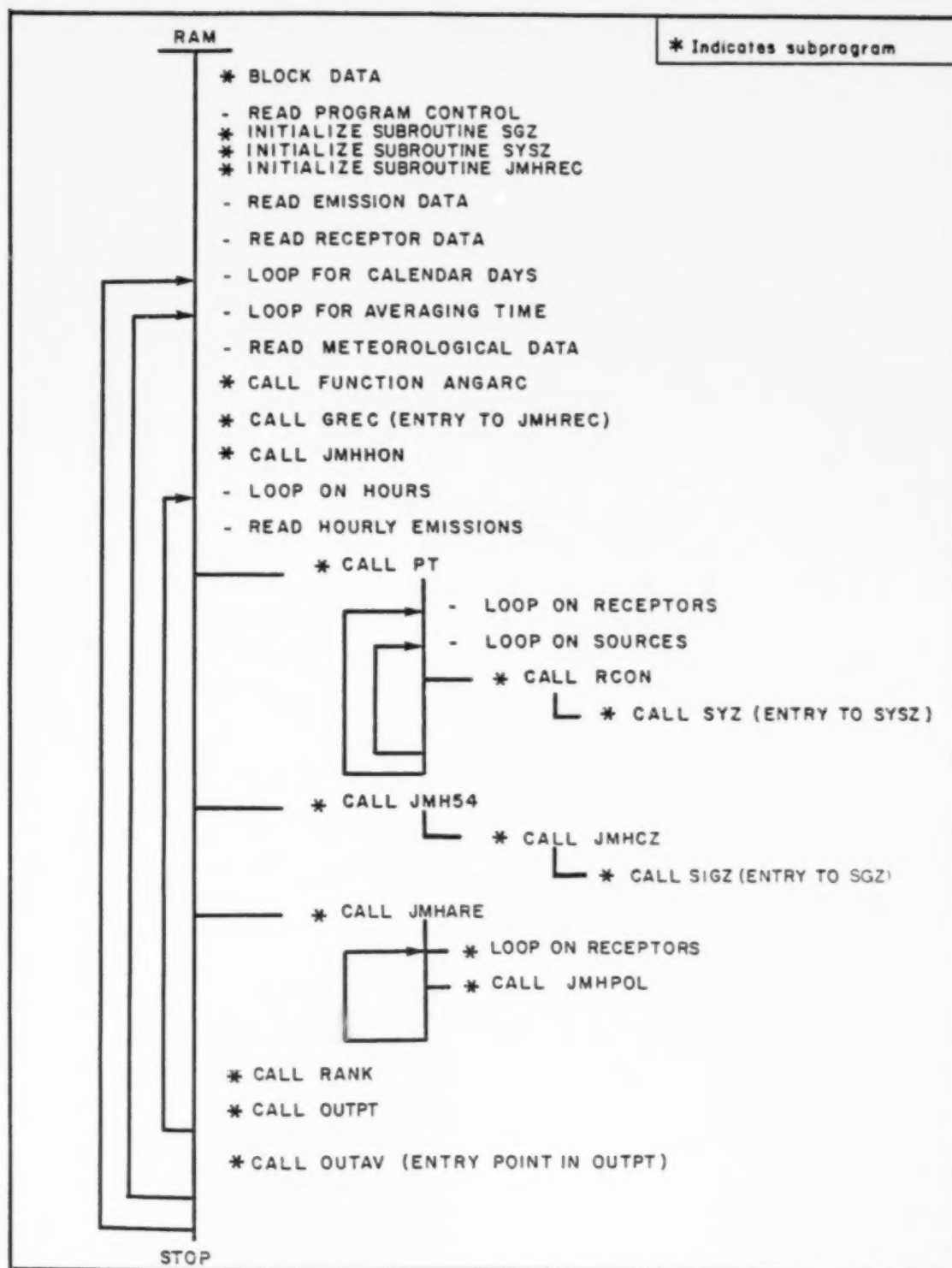


Figure 8. Structure of RAM.

are converted to internal units. An internal unit is a length such that any area source side length used in a given run can be expressed as an integer multiple of an internal unit. The internal unit is generally equal to the length of the side of the smallest area in the emission inventory. The user must determine the internal unit length and specify it in user units. Both point and area sources are ranked according to expected impact at ground level. The 25 point sources and the 10 area sources with the greatest expected ground-level impact are listed. Also, the total emissions from various physical heights for both point and area sources are listed. This helps the user in determining area source heights and the number to be used.

BRIEF DESCRIPTION OF SUBROUTINES

The subroutine and function descriptions that follow are called by RAM to perform specific tasks.

- ANGARC - This function determines the appropriate arctan of the east resultant wind component over the north resultant wind component with the resulting angle between 0° and 360° .
- JMHREC - This subroutine and entry point GREC called by RAM determine receptor locations downwind of significant sources based upon the resultant meteorological conditions for the averaging period, usually 3 or 24 hours. Plume rise and effective height of emission are calculated. The distance of the maximum concentration is determined as a function of the stability and the effective height of emission in order to locate the position of a receptor. Two receptors are generated for each significant point source, one at the expected distance of maximum concentration and one at twice this distance. One receptor is generated for each significant area source at the expected distance of maximum concentration.
- JMHON - This subroutine called by RAM generates additional receptors within a specified area in order to give adequate coverage of that area with the minimum number of receptors. Receptors are placed

equidistant from nearby receptors, resulting in a honeycomb array. The distance between receptors is an input to the main program. Proposed honeycomb receptors located closer than half this distance to any other receptor are not included.

- PT - This subroutine calculates concentrations from point sources. Subroutines RCON and SYZ (ENTRY point in SYSZ) are called to complete the computations.
- RCON - This subroutine called by PT calculates X/Q , the relative concentrations from point sources. This subroutine calls SYZ.
- SYZ - This subroutine called by RCON calculates the standard deviation of the concentration in the y- and z- directions. It employs the Briggs urban dispersion parameters for urban conditions, and the Pasquill-Gifford parameters for rural conditions.
- JMH54 - This subroutine called by RAM generates tables of Xu/q_A (relative concentration normalized for wind speed) from area sources that extend from a receptor to various upwind distances. A table is produced for each area source height. One to three heights can be used. This subroutine calls subroutine JMH CZ.
- JMH CZ - This subroutine called by JMH54 calculates concentrations from infinite crosswind line sources at a distance x upwind from a receptor. To obtain the vertical dispersion parameter value σ_z , subroutine SIGZ is called.
- SIGZ - This subroutine called by JMH CZ determines the value of the vertical dispersion parameter σ_z for a given upwind distance of a receptor to the source. The parameter values for urban areas are those put into equation form by Briggs. The parameter values for rural areas are from Pasquill-Gifford.
- JMHARE - This subroutine performs the integration along the line upwind from the receptor to obtain the effect of all area sources along the line. This is accomplished by finding the nearest and farthest distance of each source along the path and calling subroutine JMHPOL for each distance.

- JMHPOL - This subroutine called by JMHARE interpolates for a given distance from the values in the tables generated by subroutine JMH54. This yields the effect of an area source at the given height extending upwind to this distance.
- RANK - This subroutine arranges concentrations of various averaging times into tables of the highest five concentrations for each receptor for each averaging time (high-five tables).
- OUTPT - This subroutine produces output concentrations in micrograms per cubic meter for each hour for significant sources and for the summaries.
- OUTAV - This subroutine called by RAM gives concentrations for the averaging period. Contributions and/or summary information are also generated by OUTAV.

PROCESSOR PROGRAM RAMMET

If option 8 specifies that meteorological data should be expected from a file, a peripheral program RAMMET can be used to generate the file. RAMMET processes meteorological data for one year. The data input consists of hourly meteorological records in the standard card format 144 of the National Climatic Data Center and twice-a-day estimates of mixing height (minimum and maximum). Hourly stability class is determined using the objective method of Turner (1964) based on Pasquill's technique (Pasquill, 1961). Shifts by only one stability class are allowed for adjacent hours. Hourly mixing height is interpolated from the twice-a-day estimates. Hourly meteorological data of wind direction, wind speed, temperature, stability class, and mixing height are written into a file with one record per day for the entire year. Random numbers can be read from a file or generated by the computer used. RANDU is a library subroutine of UNIVAC 1110's MATH-PACK. (For use on other computers, this call must be replaced by a call to a suitable random number generator.) For regulatory applications, the file of random numbers included with RAMMET Test 1 in the UNAMAP (Version 6) U. S. EPA, 1986 should be used.

SECTION 9

INPUT DATA PREPARATION

In this section, the general input data requirements are listed. There are 18 record types in the input stream. Each record type consists of one or more records.

Table 2 describes the input data; in some cases an explanation follows the entry.

TABLE 2. RECORD INPUT SEQUENCE FOR RAM

Record type and variable	Column	Format	Variable description	Units
Record type 1				
LINE1	1-80	20A4	80-character title	---
Record type 2				
LINE2	1-80	20A4	80-character title	---
Record type 3				
LINE3	1-80	20A4	80-character title	---
RECORDS 1 - 3. Each card image has up to 80 alphanumeric characters. The input title appears on all output and can suit the user. Normal use has been to identify the user and run date on card-image 1, the location and date of the emissions data on card-image 2, and the location and dates of both surface and upper air meteorological data on card-image 3.				
RAM-RECORD TYPE 4 - 14 variables				
Record type 4				
IDATE(1)	---	FF*	2-digit year	---

*FF is free format.

Record type and variable	Column	Format	Variable description	Units
IDATE(2)	---	FF	Starting Julian day	---
IHSTRT	---	FF	Starting hour	---
NPER	---	FF	Number of averaging per- iods	---
NAVG	---	FF	Number of hours in an averaging period (com- monly 24)	---
IPOL	---	FF	Pollutant indicator: 3, sulfur dioxide 4, suspended particulate	---
MUOR	---	FF	Model indicator: 1, urban mode 2, rural mode	---
NSIGP	---	FF	Number of point sources from which concentration contributions are desired (maximum=25)	---
NSIGA	---	FF	Number of area sources from which concentration contributions are desired (maximum=10)	---
NAV5	---	FF	Additional averaging time for high-five table. Usu- ally 2, 4, 6, or 12.	---
CONONE	---	FF	Multiplier to convert user units to kilometers.	---

Example multipliers are: 3.048×10^{-4} for feet to kilometers; 1.609347 for miles to kilometers; 1.0×10^{-3} for meters to kilometers.

UNITS	---	FF	Number of user units per smallest area source side length. Should equal 1 if no area sources. (Internal units)	---
-------	-----	----	--	-----

Record type and variable	Column	Format	Variable description	Units
Z	---	FF	Receptor height	m
HAFL	---	FF	Pollutant half-life	sec

An entry of zero in HAFL will cause RAM to skip pollutant loss calculations.

RAM-RECORD TYPE 5 - The values are for 50 different options; 1 is used to employ the option and a zero indicates non-use.

Record type 5

IOPT(1)	1	I1	No stack downwash	---
IOPT(2)	2	I1	No gradual plume rise	---
IOPT(3)	3	I1	Use buoyancy induced dispersion	---
IOPT(4)	4	I1	Not used	---
IOPT(5)	5	I1	Input point sources	---
IOPT(6)	6	I1	Input area sources	---
IOPT(7)	7	I1	Use emissions from previous run. Data accessed from Unit 9.	---
IOPT(8)	8	I1	Meteorology data in input stream. Otherwise, input from Unit 11.	---
IOPT(9)	9	I1	Read hourly point source emissions (Unit 15)	---
IOPT(10)	10	I1	Read hourly area source emissions (Unit 16)	---
IOPT(11)	11	I1	Specify significant point sources	---

Option 11 will allow the examination of the individual contributions to each receptor from each of the specified sources. Both point and area sources may be specified. (See IOPT(12))

Record type and variable	Column	Format	Variable description	Units
IOPT(12)	12	I1	Specify significant area sources	---
IOPT(13)	13	I1	Not used	---
IOPT(14)	14	I1	Enter receptors by specifying coordinates	---
IOPT(15)	15	I1	RAM generates receptors downwind of significant point sources	---
IOPT(16)	16	I1	RAM generates receptors downwind of significant area sources	---
IOPT(17)	17	I1	RAM generates honeycomb array of receptors to cover specified area	---

RAM generates a honeycomb array of receptors, placed equidistant in staggered rows over a specified area. This insures good area coverage. Candidate receptor positions are checked against other receptors (either input or generated by other options of the program) and if the distance between the proposed receptor is less than one-half the normal distance between honeycomb receptors, then the candidate receptor is not added to the list. The boundaries of the area to be covered by these receptors are specified by the user.

IOPT(18)	18	I1	Input radial distances to generate polar coordinate receptor array. 36 receptors for each distance.	---
IOPT(19)	19	I1	Not used	---

Printed output is controlled by the options that follow.
Options 20 through 36 are all options to omit output. In

Record type and variable	Column	Format	Variable description	Units
-----------------------------	--------	--------	----------------------	-------

the program default, most of these options to omit output are used since some of the options can generate large amounts of printed output.

IOPT(20)	20	I1	Omit point source list	---
IOPT(21)	21	I1	Omit area source list and map	---
IOPT(22)	22	I1	Omit emissions with height table	---
IOPT(23)	23	I1	Omit resultant meteorology data summary for averaging period	---
IOPT(24)	24	I1	Omit all hourly output (point, area, summaries)	---
IOPT(25)	25	I1	Omit hourly point contribu- tions	---
IOPT(26)	26	I1	Omit meteorology data on hourly point contribu- tions	---
IOPT(27)	27	I1	Omit plume height and distance to final rise on hourly point contribution	---
IOPT(28)	28	I1	Omit hourly area contributions	---
IOPT(29)	29	I1	Omit meteorology data on hourly area contributions	---
IOPT(30)	30	I1	Omit hourly summary	---
IOPT(31)	31	I1	Omit meteorological data on hourly summary	---
IOPT(32)	32	I1	Omit all averaging period output	---
IOPT(33)	33	I1	Omit point averaging period contributions	---

Record type and variable	Column	Format	Variable description	Units
IOPT(34)	34	I1	Omit area averaging period contributions	---
IOPT(35)	35	I1	Omit averaging period summary	---
IOPT(36)	36	I1	Omit average concentrations and highest five concen- trations table	---
IOPT(37)	37	I1	Not used	---

The remaining options control the flow of the program and the amount of output. This is especially so for Option 40, in which a large file can be generated by employing this option.

IOPT(38)	38	I1	Set default option for regulatory application	---
----------	----	----	--	-----

Option 38 sets a series of options and parameters when the model is to be used for regulatory application.

IOPT(39)	39	I1	Part of segmented run	---
IOPT(40)	40	I1	Write partial concentra- tions to disk or tape (Unit 10)	---

The user will need to write the software to process this output. Although it is unlikely that Options 39 and 40 will be employed on the same run, it is possible to do so. However, the second and subsequent segments will not skip over previously generated partial concentration files. Therefore, unless Unit 10 accesses a different file on each segment, any previously generated partial concentration files will be overwritten.

IOPT(41)	41	I1	Write hourly concentrations to disk or tape (Unit 12)	---
----------	----	----	--	-----

Record type and variable	Column	Format	Variable description	Units
-----------------------------	--------	--------	----------------------	-------

IOPT(42)	42	I1	Write averaging-period concentration to disk or tape (Unit 13)	---
----------	----	----	--	-----

The output files generated by Options 41 and 42 are useful only when the receptors are set for the run and not varying from one averaging period to another. Therefore, these options can be used with Options 14 and 18, but a program termination will occur in trying to use Option 41 or 42 in combination with any of Options 15, 16, or 17.

IOPT(43)	43	I1	Write averaging-period concentrations in card- image format (80 bytes) to Unit 1.	---
----------	----	----	--	-----

IOPT(44)	44	I1	Not used this version	---
IOPT(45)	45	I1	Not used this version	---
IOPT(46)	46	I1	Not used this version	---
IOPT(47)	47	I1	Not used this version	---
IOPT(48)	48	I1	Not used this version	---
IOPT(49)	49	I1	Not used this version	---
IOPT(50)	50	I1	Not used this version	---

RAM-RECORD TYPE 6 - 2 variables, 1 to 7 values. Selection of the default option (Option 38) causes wind exponents to be set to the default values for the appropriate urban or rural cases. This record is still required to input the anemometer height; all other data on the record will be ignored when Option 38 is set.

Record type 6

HANE	---	FF	Anemometer height	m
PL(I)	---	FF	Wind speed power law exponents	---

Record type and variable	Column	Format	Variable description	Units
-----------------------------	--------	--------	----------------------	-------

RAM-RECORD TYPE 7 - 9 variables, 8 values (one of these records for each point source). This is used if Option 5 = 1 (the user inputs point sources) and Option 7 = 0 (no emissions are entered from a previous run).

Record type 7

PNAME(I,NPT)	1-12	3A4	12 character point source identification	---
SOURCE(1,NPT)	13-20	F8.2	East coordinate of point source (user units)	---
SOURCE(2,NPT)	21-28	F8.2	North coordinate of point source (user units)	---
SOURCE(3,NPT)	29-36	F8.2	Sulfur dioxide emission rate	g/sec

Emission rates for pollutants other than sulfur dioxide and particulates may be substituted. If substitutions are made, changes in data statements are necessary in order to have the proper pollutant names on the printed output.

SOURCE(4,NPT)	37-44	F8.2	Particulate emission rate	g/sec
SOURCE(5,NPT)	45-52	F8.2	Physical stack height	m
SOURCE(6,NPT)	53-60	F8.2	Stack gas temperature	K
SOURCE(7,NPT)	61-68	F8.2	Stack inside diameter	m
SOURCE(8,NPT)	69-76	F8.2	Stack gas exit velocity	m/sec

To indicate the end of point source records, the word "ENDP" is placed in record columns 1 to 4.

RAM-RECORD TYPE 8 - 7 variables, 6 values (one of these records is required for each area source). This is used if Option 6 = 1 (the user inputs area sources) and Option 7 = 0 (no emissions input from previous run).

Record type and variable	Column	Format	Variable description	Units
Record type 8				
ANAME(J,NAS)	1-12	3A4	12 character area source identification	---
ASORC(1,NAS)	13-22	F10.2	East coordinate of SW corner of area source (user units)	---
ASORC(2,NAS)	23-32	F10.2	North coordinate of SW corner of area source (user units)	---
ASORC(5,NAS)	33-42	F10.2	Side length of area source (user units)	---
Note that ASORC(5,NAS) - side length, is read out of order to conform with the existing order of IPP emissions data.				
ASORC(3,NAS)	43-52	F10.2	Sulfur dioxide emission rate for entire area	g/sec
ASORC(4,NAS)	53-62	F10.2	Particulate emission rate for entire area	g/sec
Particulate Emission Rate for entire area is a total rate for the entire area. It is later transformed into $\text{gm/sec}^{-1}\text{m}^{-2}$. As with point sources, emission rates for other pollutants may be substituted for sulfur dioxide and particulates, with appropriate name changes made in the data statements to modify titles on the printouts.				
ASORC(6,NAS)	63-72	F10.2	Area source height	m

Although only one pollutant can be considered for a given run of RAM, both of the entered emission rates are listed in the output. One of the emission rates may be left off and will appear as zeros in the output.

Record type and variable	Column	Format	Variable description	Units
-----------------------------	--------	--------	----------------------	-------

Area sources can vary in size, but certain requirements must be met. There must be a definable internal unit such that the side length of all other area sources is an integer multiple of the side length of this internal unit. For example, if an emission inventory consists of area source squares having side lengths of 1, 2.5, 5, and 10 km, the internal unit must be chosen to equal 0.5 km. It is better to conduct emission inventories so that area source squares have side lengths that are multiples of the side lengths of the smallest area source squares. Also, if a grid is constructed of unit squares, squares having side length of one internal unit, the boundaries of all area sources must coincide with lines in that grid; there can be no overlap of one area source over another. Although these statements may seem restrictive, the area source entries to RAM are quite versatile. Concentrations from area sources are calculated by performing computations for each area source encountered in proceeding from a receptor in the upwind direction until the upwind boundary of the area source is encountered. If there are large areas (larger than the unit square) of zero emissions within the rectangle that includes all area sources (area source region), it is desirable to define these as area sources with zero emissions in squares as large as possible. This will result in considerable savings in computer processing time.

If the height of emission is the effective height of the area source at a wind speed of 5 m/sec, and if the physical height of the source is a set fraction of this value, which is the same for all area sources, it will be

Record type and variable	Column	Format	Variable description	Units
-----------------------------	--------	--------	----------------------	-------

possible to consider the variation of effective height of area sources with wind speed in RAM. Otherwise, the fraction will be 1.0 and it will be assumed that the input height of emission is the effective height for all wind speeds.

RAM-RECORD TYPE 9 - 2 variables. This record is required only if Option 11 is used (i.e., the user will specify significant point sources).

Record type 9

INPT	1-3	I3	Number of user specified significant sources	---
------	-----	----	---	-----

The maximum number of user specified significant point sources is 25 - this number must be non-zero.

MPS(I)	4-78	I3	INPT point source numbers the user wants considered significant (max = 25)	---
--------	------	----	--	-----

There will be as many sources in this list as indicated in INPT.

RAM-RECORD TYPE 10 - 4 variables - 4 values. Information for area sources. This record is required only if Option 6 is employed (user will input area sources).

Record type 10

FH	---	FF	Fraction of area source height which is physical height	---
XLIM	---	FF	Distance limit on inte- gration for area source (user units)	---

The distance XLIM should be equal to or exceed the greatest possible distance from a receptor (including receptors generated by RAM) to the farthest corner of the

Record type and variable	Column	Format	Variable description	Units
area source region for this run, but cannot exceed 116 kilometers.				
NHTS	---	FF	Integer number of heights to be used for area sources (min=1, max=3)	---
HINT	---	FF	Height(s) for area source integrations. Same number as NHTS.	m

RAM-RECORD TYPE 11 - 1 variable - 1 or 2 values. This record is required only if record type 10 is used.

Record type 11

BPH	---	FF	Breakpoint heights between area source heights	m
-----	-----	----	--	---

These values are to be used as boundaries between the specified area source heights used for calculations. If only one area source height is to be used, only one BPH value is entered; it should be greater than any area source height of the area source data. If NHTS is 2, the single value for BPH should be between the two HINT values. If NHTS is 3 and the three HINT values are, for example, 15, 25, and 35; the two values for BPH might be 20 and 30.

RAM-RECORD TYPE 12 - 2 variables - 1 to 11 values. This record is required only if Option 12 is used (i.e., user specifies significant area sources).

Record type 12

INAS	1-3	I3	Number of user specified significant area sources (max=10)	---
MAS	4-33	I3	INAS area source numbers the user wants to consider significant	---

Record type and variable	Column	Format	Variable description	Units
-----------------------------	--------	--------	----------------------	-------

RAM-RECORD TYPE 13 - 4 variables. Used if Option 8 = 0
(meteorological data will be input on Unit 11).

Record type 13

ISFCD	---	FF	Surface Met. Station Identifier	---
-------	-----	----	------------------------------------	-----

ISFCD is a 5-digit identification of the meteorological
tape to be used. For tapes generated by the National
Climatic Data Center, this will normally be the surface
station number.

ISFCYR	---	FF	Year of surface meteorology data	---
IMXD	---	FF	Upper-air Station Identifier	---
IMXYR	---	FF	Year of mixing height data (2 digits)	---

RAM-RECORD TYPE 14 - 3 variables - 7 values. This record
is used with Option 18 (input of polar coordinates) if the
user chooses to input receptor positions according to a
radial distance from a coordinate source.

Record type 14

RADIL(I)	---	FF	One to five radial distances (user units)	---
----------	-----	----	---	-----

RADIL(I) is one to five radial distances (with the
remaining distances entered as zeros) centered on any
location. Each radial distance generates 36 receptors at
each radial distance at azimuths of 10 to 360 degrees.

CENTX	---	FF	East coordinate about which radials are centered (user units)	---
-------	-----	----	--	-----

Record type and variable	Column	Format	Variable description	Units
CENTY	---	FF	North coordinate about which radials are cen- tered (user units)	---

RAM-RECORD TYPE 15 - 3 variables. If Option 14 (user specifies receptor coordinates) is used there will be one record for each receptor that the user specifies.

Record type 15

RNAME(I)	1-8	2A4	8 digit alphanumeric station identification	---
RREC	9-18	F10.3	East coordinate of receptor (user units)	---
SREC	19-28	F10.3	North coordinate of receptor (user units)	---

Both coordinates of receptors should be positive. Receptors may be either inside or outside the area source region. A record with "ENDR" in columns 1 - 4 signals that the receptor list has been completed.

RAM-RECORD TYPE 16 - 5 variables - 5 values. This record is needed only if Option 17 is used to generate additional receptors for area coverage.

Record type 16

GRDSPU	---	FF	Grid spacing between honeycomb receptors (user units)	---
HRMIN	---	FF	Minimum east coordinate (user units)	---
HRMAX	---	FF	Maximum east coordinate (user units)	---
HSMIN	---	FF	Minimum north coordinate (user units)	---
HSMAX	---	FF	Maximum north coordinate (user units)	---

Record type	and variable	Column	Format	Variable description	Units
-------------	--------------	--------	--------	----------------------	-------

If HRMIN, HRMAX, HSMIN, HSMAX are entered as zero, the boundaries considered for these receptors will be the same as those of the area source region. However, if no area sources are input and if honeycomb receptors are to be generated, this record must have boundaries included to provide the bounds for receptor generation.

RAM-RECORD TYPE 17 - 2 variables. This record is needed only if Option 39 is used (i.e., this run is part of a segmented run).

Record type 17

IDAY	---	FF	Number of days previously processed	---
LDRUN	---	FF	Last day to be processed in this run	---

RAM-RECORD TYPE 18 - 8 variables - 8 values.
Meteorology. Used if Option 8 = 0.

Record type 18

JYR	---	FF	Year of meteorology data (2 digits)	---
DAY1	---	FF	Julian day of meteorology data	---
JHR	---	FF	Hour of meteorology data	---
IKST	---	FF	Stability class for this hour	---
QU	---	FF	Wind speed for this hour	m/sec
QTEMP	---	FF	Ambient air temperature for this hour	K
QTHETA	---	FF	Wind direction for this hour (degrees azimuth from which winds blows)	deg
QHL	---	FF	Mixing height for this hour	m

Emissions Data

In the emissions file either point sources, area sources, or both may be included. When both types are included, the user still has the option to select one or both source types. Any rectangular coordinate system is allowed provided that the positive quadrant is used, that is, all coordinate values are positive and a single coordinate system is used for both point and area sources. The scale of the coordinate system is arbitrary. An option is also available in which the user can specify radial coordinates of receptors by specifying up to five radial distances.

To account for variability in emission rates with time in order to simulate emissions most accurately, it is possible to enter new emission rates for each of the sources for each simulated hour using Option 9 and/or Option 10. In order to employ this option, emissions for each source must have been determined and written on two tape or disk files (one for point sources and one for area sources) with one record for each hour that is to be simulated. The emission information from RAM is still required and must be a "normal" emission rate in order that the exit velocity of the source can be scaled up or down in proportion to the hourly emission rate. Also, all permanent information about sources such as coordinates, physical stack height, and diameter are furnished on record type 8.

Meteorological Data and RAMMET

As noted previously, meteorological data for RAM can be furnished in either of two ways: 1) records containing the meteorological data for each simulated hour (one record per hour), or 2) magnetic disk or tape output from program RAMMET.

Meteorological data output from RAMMET may be used as input to RAM. RAMMET requires one year of hourly surface observations and one year plus two days of daily maximum and minimum mixing height data. The hourly surface data normally on magnetic tape in card image format, CARD DECK 144, can be obtained from the National Climatic Center in Asheville, NC.

All required surface data for each hour must be included on the tape; therefore, all data flagged as missing by RAMMET must be accounted for,

determined, and included in the data set before proceeding. The data used from the surface observation tape for each hour are: year, month, day, hour, cloud ceiling code, wind direction, wind speed, temperature, and opaque cloud cover.

The mixing height data is expected in card image format for RAMMET, one card per day containing the minimum and maximum mixing height for that day.

When using meteorological data from RAMMET, there are greater restrictions on certain input parameters than there are when meteorological data from cards are used. Using RAMMET data, one averaging time must be used, and it must be evenly divisible into 24. The start hour must be 1. Periods must be sequential in the time series. The starting day may be any day included in the file. The file will be positioned to the correct start day.

One averaging time must be used when using meteorological data with the run stream, but it can be any integer value from 1 to 24. The start hour can be any hour from 1 to 24. Day and hour values must be entered correctly and must be in sequence within each period. Data from period to period needs to be in sequence; for example, calculations for two 2-hour periods can be done first: day 181, hour 24, followed by day 182, hour 1.

SECTION 10

EXECUTION OF THE MODEL AND SAMPLE TEST

RAM produces an error-free compile on Univac EXEC 8, IBM MVS, and DEC VAX/VMS computers with comparable output results.

Job Control Language (JCL) for model execution on a Univac EXEC 8 system would have the following form:

```
@RUN,R/R JOB-ID, etc.  
@ASG,A MODELS*LOAD  
@XQT MODELS*LOAD.RAM  
  (Input records)  
@FIN
```

On an IBM system under MVS, the JCL would be as follows,

```
//JOBID    JOB  (PROJ,ACCT,OTHER),TIME=1  
//RAM      EXEC PGM=RAM,TIME=(,20)  
//STEBLIB  DD   DSN=USERID.MODELS.LOAD,DISP=SHR  
//FT06F001 DD   SYSOUT=A  
//FTD5F001 DD   *  
  (Input records)  
//
```

Sample Test

The example given here uses one year of meteorological data processed by RAMMET, and uses the default option for regulatory application in the urban mode. Because the default option is exercised, the following features apply:

- urban dispersion parameters are used,
- final plume rise is used,
- bouyancy-induced dispersion is accounted for,
- urban-profile exponents of .15, .15, .20, .25, .30 and .30 are used,
- stack-tip downwash is calculated,
- calms are processed according to regulatory guidance,
- options 7, 8, 11, 12, 15, 16 and 39 through 43 are set to zero, and
- output options 23 through 35 are set to 1.

The input stream is given on the following page. Four averaging periods are requested with a high-five concentration table for each. It should be noted that the default option overrides user input in most cases, for example, NAV5 is given as 6 in the run stream, but since the default option does not allow a fifth averaging time, the request is overridden.

Hardcopy output produced by RAM follows the run stream. Notations are made where appropriate to illustrate the application.


```

@RUN,D/R 12EDK/80,[ACCT. NUMBER]/BDU,EDB/XINRT,45
SYM,U PRINTS,,FD04PR
@ASG,A CINDAY2.
@USE 11,CINDAY2.
@ASG,A EOB*UNAMAP.
@XQT EOB*UNAMAP.RAMABS
SAMPLE TEST USING 1964 CINCINNATI-DAYTON DATA. D. BRUCE TURNER
EMISSIONS: TEST CITY, 1973
SFC MET DATA: TEST CITY 1973; UPPER AIR: TEST CITY 1973
64,001,01,366,24,3,1,5,10,6,1.609344,2.,0.,14400.
100411110011311100900000000000000000171111114567890
10.,0.,0.,0.,0.,0.,0.
PLANT 1 579.50 4406.75 232.365 13.335 82.9 513.1 3.5 13.7
PLANT 2 575.25 4405.25 150.465 57.005 76.2 464.3 3.2 12.5
PLANT 3 571.25 4407.00 19.005 3.255 25.9 477.6 1.0 15.8
PLANT 4 571.75 4402.25 81.060 28.350 40.8 499.8 2.8 17.6
PLANT 5 579.50 4403.25 26.145 5.145 18.3 533.2 0.6 14.7
PLANT 6 567.14 4400.89 2.56 0. 26.5 505. 1.04 3.81
PLANT 7 564.70 4407.50 36.43 0. 48.8 464. 3.05 18.6
PLANT 8 577.45 4401.35 33.64 0. 26.5 428. 1.68 5.02
PLANT 9 576.75 4400.70 38.8 0. 6. 654. .79 24.89
PLANT 10 580.10 4412.00 299.5 0. 93. 405. 4.88 12.59
PLANT 11 583.0 4400.90 16.74 0. 18.1 506. 1.37 4.23
PLANT 12 574.0 4398.00 226.2 0. 93.6 483. 4.88 12.59
ENDP
AONE 570. 4400. 4. 1.25 0.0 10.
ATWO 574. 4400. 2. 3.05 0.0 10.
ATHREE 576. 4400. 2. 6.25 0.0 12.
AFOUR 578. 4400. 2. 8.85 0.0 15.
AFIVE 578. 4402. 2. 3.15 0.0 10.
ASIX 574. 4402. 4. 0.00 0.0 0.
ASEVEN 570. 4404. 4. 4.25 0.0 15.
AEIGHT 574. 4406. 2. 2.60 0.0 10.
ANINE 578. 4406. 2. 3.10 0.0 12.
ATEN 580. 4406. 2. 2.76 0.0 20.
AELEVEN 582. 4406. 2. .83 0.0 20.
ATWELVE 580. 4404. 2. 1.66 0.0 20.
ATHIRTEEN 582. 4404. 2. 1.90 0.0 20.
AFOURTEEN 580. 4402. 2. .51 0.0 20.
AFIFTEEN 582. 4402. 2. 1.48 0.0 20.
ENDA
.75, 25., 3, 11.,15.,20.
13., 17.
93814,64,93815,64
RECEP 1 566.00 4405.0
RECEP 2 564.00 4401.5
3 572. 4400.866
4 574. 4400.866
5 576. 4400.866
6 578. 4400.866
7 580. 4400.866
8 571. 4402.598
9 573. 4402.598
10 575. 4402.598
11 577. 4402.598
12 579. 4402.598
13 572. 4404.330
14 574. 4404.330
15 576. 4404.330
16 578. 4404.330
17 580. 4404.330
18 571. 4406.062
19 573. 4406.062
20 575. 4406.062
21 577. 4406.062
22 579. 4406.062
23 572. 4407.794
24 574. 4407.794
25 576. 4407.794
26 578. 4407.794
27 580. 4407.794
ENDR
@FIN
@@
@@
@@

```

OUTPUT FROM URBAN RAM (VERSION 85364)
 AN AIR QUALITY DISPERSION MODEL IN
 SECTION 1. GUIDELINE MODELS
 IN UNAMAP (VERSION 6) DEC 86
 SOURCE: UNAMAP FILE ON EPA'S UNIVAC 1110, RTP. NC.

SAMPLE TEST USING 1964 CINCINNATI-DAYTON DATA. D. BRUCE TURNER
 EMISSIONS: TEST CITY, 1973
 SFC MET DATA: TEST CITY 1973; UPPER AIR: TEST CITY 1973

GENERAL INPUT INFORMATION

THIS IS THE URBAN VERSION(81352) OF RAM FOR THE POLLUTANT SO2 FOR 366 24-HOUR PERIODS.
 CONCENTRATION ESTIMATES BEGIN ON HOUR- 1, JULIAN DAY- 1, YEAR-1964.
 UNITS - THERE ARE 2.0000000 USER UNITS(INPUT UNITS) PER SMALLEST AREA SOURCE SQUARE SIDE LENGTH(INTERNAL UNIT)
 CONONE - THERE ARE 1.6093440 KILOMETERS PER USER UNIT
 CONTO - IT IS CALCULATED THAT THERE ARE 3.2186880 KILOMETERS PER SMALLEST AREA SOURCE SQUARE SIDE LENGTH(INTERNAL UNIT)
 RECEPTOR HEIGHT IS .0000000 METERS

A HALF-LIFE OF 14400.00 (SECONDS) HAS BEEN ASSUMED BY THE USER.
 HIGH-FIVE SUMMARY CONCENTRATION TABLES WILL BE OUTPUT FOR 4 AVERAGING PERIODS.
 AVG TIMES OF 1,3,8, AND 24 HOURS ARE AUTOMATICALLY DISPLAYED.

OPTION OPTION LIST OPTION SPECIFICATION : 0= IGNORE OPTION
 1= USE OPTION

TECHNICAL OPTIONS

1 NO STACK DOWNWASH 0
 2 NO GRADUAL PLUME RISE. 1
 3 USE BOUTANCY INDUCED DISPERSION 1
 4 NOT USED THIS VERSION 4

INPUT OPTIONS

5 WILL YOU INPUT POINT SOURCES? 1
 6 WILL YOU INPUT AREA SOURCES? 1
 7 WILL YOU USE EMISSIONS FROM PREVIOUS RUN? (UNIT 9) 0
 8 MET.DATA ON CARDS? (FROM UNIT 11 OTHERWISE) 0
 9 READ HOURLY PT. SOURCE' EMISSIONS (UNIT 15). 0
 10 READ HOURLY AREA SOURCE EMISSIONS (UNIT 16). 0
 11 SPECIFY SIGNIF PT. SOURCES. 0
 12 SPECIFY SIGNIF. AREA SOURCES. 0
 13 NOT USED THIS VERSION 3

RECEPTOR OPTIONS

14 WILL YOU ENTER RECEPTORS BY SPECIFYING COORDINATES? 1
 15 DO YOU WANT RAM TO GENERATE RECEPTORS DOWNWIND OF SIGNIF. PT. SOURCES? (WILL DO SO BY AVG-PERIOD) 0
 16 DO YOU WANT RAM TO GENERATE RECEPTORS DOWNWIND OF SIGNIF. AREA SOURCES?(WILL DO SO BY AVG-PERIOD) 0
 17 DO YOU WANT RAM TO GENERATE A HONEYCOMB ARRAY OF RECEPTORS TO COVER A SPECIFIC AREA? 0
 18 WILL YOU INPUT RADIAL DISTANCES(UP TO 5) TO GENERATE A POLAR COORDINATE RECEPTOR ARRAY (36 RECEPTORS FOR EACH DISTANCE) 0
 19 NOT USED THIS VERSION 9

PRINTED OUTPUT OPTIONS

20 DELETE POINT SOURCE LIST 0

21	DELETE AREA SOURCE LIST AND MAP	0
22	DELETE EMISSIONS WITH HEIGHT TABLE	0
23	DELETE RESULANT MET. DATA SUMMARY FOR AVERAGING PERIOD	1
24	DELETE ALL HOURLY OUTPUT (PT., AREA, & SUMMARIES)	1
25	DELETE HOURLY POINT CONTRIBUTIONS	1
26	DELETE MET. DATA ON HR. PT. CONTRIB.	1
27	DELETE PLUME HT. AND DIST. TO FINAL RISE ON HR. PT. CONTRIB.	1
28	DELETE HOURLY AREA CONTRIBUTIONS	1
29	DELETE MET. DATA ON HR. AREA CONTRIB.	1
30	DELETE HOURLY SUMMARY.	1
31	DELETE MET. DATA ON HOURLY SUMMARY.	1
32	DELETE ALL AVG-PERIOD OUTPUT.	1
33	DELETE POINT AVG-PERIOD CONTRIBUTIONS.	1
34	DELETE AREA AVG-PERIOD CONTRIBUTIONS.	1
35	DELETE AVG-PERIOD SUMMARY.	1
36	DELETE AVERAGE CONCENTRATIONS & HI-FIVE TABLE.	0
37	NOT USED THIS VERSION.	7
	DEFAULT OPTION.	
38	SET DEFAULT OPTION.	1

OTHER CONTROL AND OUTPUT OPTIONS:

39	RUN IS PART OF A SEGMENTED RUN.	0
40	WRITE PARTIAL CONC. TO DISK OR TAPE (UNIT 10).	0
41	WRITE HOURLY CONC. TO DISK OR TAPE (UNIT 12).	0
42	WRITE AVG-PERIOD CONC. TO DISK OR TAPE (UNIT 13).	0
43	PUNCH AVERAGING-PERIOD CONC. ON CARDS (UNIT 1).	0
44	NOT USED THIS VERSION.	4
45	NOT USED THIS VERSION.	5
46	NOT USED THIS VERSION.	6
47	NOT USED THIS VERSION.	7
48	NOT USED THIS VERSION.	8
49	NOT USED THIS VERSION.	9
50	NOT USED THIS VERSION.	0

POINT SOURCE INFORMATION											
SOURCE	EAST COORD	NORTH COORD	S02(G/SEC) EMISSIONS	PART(G/SEC) EMISSIONS	HT(M)	STACK TEMP(K)	STACK DIAM(M)	STACK VEL(IN/SEC)	POTEN. IMPACT (MICRO G/MM*3)	EFF HT(M)	BUOY FLUX F MM*4/S**3
1 PLANT 1	579.500	4406.750	232.365	13.335	82.90	513.10	3.50	13.70	155.805	370.460	176.487
2 PLANT 2	575.250	4405.250	150.465	57.005	76.20	464.30	3.20	12.50	144.901	299.488	115.773
3 PLANT 3	571.250	4407.000	19.005	3.255	25.90	477.60	1.00	15.80	199.064	80.256	14.971
4 PLANT 4	571.750	4402.250	81.060	28.350	40.80	499.80	2.80	17.60	82.104	291.015	139.965
5 PLANT 5	579.500	4403.250	26.145	5.145	18.30	533.20	.60	14.70	818.139	45.144	5.844
6 PLANT 6	567.140	4400.890	2.560	.000	26.50	505.00	1.04	3.81	72.298	47.606	4.241
7 PLANT 7	564.700	4407.500	36.430	.000	48.80	464.00	3.05	18.60	31.988	316.174	156.325
8 PLANT 8	577.450	4401.350	33.640	.000	26.50	428.00	1.68	5.02	461.534	69.507	10.956
9 PLANT 9	576.750	4400.700	38.800	.000	6.00	654.00	.79	24.89	448.911	76.111	21.021
10 PLANT 10	580.100	4412.000	299.500	.000	93.00	405.00	4.88	12.59	171.832	405.998	203.266
11 PLANT 11	583.000	4400.900	16.740	.000	18.10	586.00	1.37	4.23	389.308	52.685	8.193
12 PLANT 12	574.000	4398.000	226.200	.000	93.60	483.00	4.88	12.59	97.496	480.294	289.141

SIGNIFICANT S02 POINT SOURCES

RANK CHI-MAX SOURCE NO.
(MICROGRAMS/MM*3)

SOURCE	EAST COORD	NORTH COORD	SQ2 EMISSIONS (GRAMS/H**2/SEC)	PART EMISSIONS (GRAMS/H**2/SEC)	SIDE LENGTH (USER UNITS)	EFFECTIVE HEIGHT (G/M/SEC)
1	818.14	5				
2	461.53	8				
3	448.91	9				
4	389.31	11				
5	199.06	3				
6	171.83	10				
7	155.81	1				
8	144.90	2				
9	97.50	12				
10	82.10	4				
11	72.30	6				
12	31.99	7				

AREA SOURCE INFORMATION

SOURCE	EAST COORD	NORTH COORD	SQ2 EMISSIONS (GRAMS/H**2/SEC)	PART EMISSIONS (GRAMS/H**2/SEC)	SIDE LENGTH (USER UNITS)	EFFECTIVE HEIGHT (G/M/SEC)
1 ADNE	570.000	4400.000	3.0164-008	.0000	4.000	10.000
2 ATWO	574.000	4400.000	2.9440-007	.0000	2.000	10.000
3 ATHREE	576.000	4400.000	6.0328-007	.0000	2.000	12.000
4 AFOUR	578.000	4400.000	8.5425-007	.0000	2.000	15.000
5 AFIVE	578.000	4402.000	3.0406-007	.0000	2.000	10.000
6 ASIX	574.000	4402.000	.0000	.0000	4.000	.0000
7 ASEVEN	570.000	4404.000	1.0256-007	.0000	4.000	15.000
8 AEIGHT	574.000	4406.000	2.5097-007	.0000	2.000	10.000
9 ANINE	578.000	4406.000	2.9923-007	.0000	2.000	12.000
10 ATEN	580.000	4406.000	2.6641-007	.0000	2.000	20.000
11 AELEVEN	582.000	4406.000	8.0116-008	.0000	2.000	20.000
12 ATWELVE	580.000	4404.000	1.6023-007	.0000	2.000	20.000
13 ATHIRTEEN	582.000	4404.000	1.8340-007	.0000	2.000	20.000
14 AFOURTEEN	580.000	4402.000	4.9228-008	.0000	2.000	20.000
15 AFIFTEEN	582.000	4402.000	1.4286-007	.0000	2.000	20.000

AREA SOURCE MAP ARRAY (IA)

4	7	7	8	0	9	10	11
3	7	7	6	0	12	13	
2	1	1	6	6	5	14	15
1	1	1	2	3	4	0	0
1	2	3	4	5	6	7	

THE ORIGIN IN INTERNAL UNITS IS (284.00, 2199.00)
 THE SIZE OF THE AREA SOURCE ARRAY IS (7, 4)
 RMINE= 285.00 RMAX= 292.00 SHIN= 2200.00 SHAX= 2204.00 (IN INTERNAL UNITS)

TOTAL SQ2 EMISSION AND CUMULATIVE FRACTION ACCORDING TO HEIGHT

HEIGHT(M)	EMISSIONS(G/S)	CUMULATIVE FRACTION	TOTAL AREA EMISSIONS(G/S)	CUMULATIVE FRACTION
0 - 5	.00	.000	.00	.000
6 - 10	38.80	.033	10.05	.241
11 - 15	.00	.033	22.45	.780

16 - 20	42.88	.070	9.14	1.000
21 - 25	.00	.070	.00	1.000
26 - 30	55.20	.118	.00	1.000
31 - 35	.00	.118	.00	1.000
36 - 40	.00	.118	.00	1.000
41 - 45	81.06	.107	.00	1.000
46 - 50	36.43	.219	.00	1.000
51 - 55	.00	.219	.00	1.000
56 - 60	.00	.219	.00	1.000
61 - 65	.00	.219	.00	1.000
66 - 70	.00	.219	.00	1.000
71 - 75	.00	.219	.00	1.000
76 - 80	150.47	.348	.00	1.000
81 - 85	232.36	.548	.00	1.000
86 - 90	.00	.548	.00	1.000
91 - 95	525.70	1.000	.00	1.000
96 - 100	.00	1.000	.00	1.000
TOTAL	.00	.00		

ADDITIONAL INFORMATION ON SOURCES.
POINT SOURCE INFORMATION

EMISSION INFORMATION FOR 12 (NPT) POINT SOURCES HAS BEEN INPUT
0 SIGNIFICANT POINT SOURCES (NSIGP) ARE TO BE USED FOR THIS RUN

AREA SOURCE INFORMATION

EMISSION INFORMATION FOR 15 (NAS) AREA SOURCES HAVE BEEN DETERMINED BY RAM
0 SIGNIFICANT AREA SOURCES (NSIGA) ARE TO BE USED FOR THIS RUN
NUMBER OF AREA HEIGHT CLASSES (NHTS)= 3
REPRESENTATIVE AREA SOURCE HEIGHTS FOR EACH HEIGHT CLASS (HINT) IN METERS = 11.00 15.00 20.00
BREAK POINT HEIGHT BETWEEN THE AREA HEIGHT CLASSES (BPH) IN METERS = 13.00 17.00
FRACTION OF AREA SOURCE HEIGHT WHICH IS PHYSICAL HEIGHT (FH) = .750
LIMIT OF DISTANCE FOR AREA SOURCE INTEGRATION TABLES (XLIM) IN USER UNITS = 25.000
BOUNDARIES OF THE AREA SOURCE GRID IN USER UNITS:
RMIN= 570.000 RMAX= 584.000 SHIN= 4400.000 SMAX= 4408.000
SIZE(IRSIZEX I) OF AREA SOURCE MAP ARRAY(IA) IN INTERNAL UNITS = 7 EAST-WEST 'BY 4 NORTH-SOUTH

SURFACE MET DATA FROM STATION(ISFCD) 93814, YEAR(ISFCYR) 1964
MIXING HEIGHT DATA FROM STATION(IMXD) 93815, YEAR(IMXYR) 1964

RECEPTOR INFORMATION

RECEPTOR	IDENTIFICATION	EAST COORD	NORTH COORD
1 I	RECEP 1	566.000	4405.000
2 I	RECEP 2	564.000	4401.500
3 I	3	572.000	4400.866
4 I	4	574.000	4400.866
5 I	5	576.000	4400.866
6 I	6	578.000	4400.866
7 I	7	580.000	4400.866
8 I	8	571.000	4402.598
9 I	9	573.000	4402.598

10 I	575.000	4402.598
11 I	577.000	4402.598
12 I	579.000	4402.598
13 I	572.000	4404.330
14 I	574.000	4404.330
15 I	576.000	4404.330
16 I	578.000	4404.330
17 I	580.000	4404.330
18 I	571.000	4406.062
19 I	573.000	4406.062
20 I	575.000	4406.062
21 I	577.000	4406.062
22 I	579.000	4406.062
23 I	572.000	4407.794
24 I	574.000	4407.794
25 I	576.000	4407.794
26 I	578.000	4407.794
27 I	580.000	4407.794

SAMPLE TEST USING 1964 CINCINNATI-DAYTON DATA. D. BRUCE TURNER
EMISSIONS: TEST CITY, 1973
SFC MET DATA: TEST CITY 1973; UPPER AIR: TEST CITY 1973

CALMS FOR PERIOD: 714

RECEPTORS

RECEPTOR	IDENTIFICATION	EAST COORD	NORTH COORD
(USER UNITS)			
1 I 0	RECEP 1	566.00	4405.00
2 I 0	RECEP 2	564.00	4401.50
3 I 0	3	572.00	4400.87
4 I 0	4	574.00	4400.87
5 I 0	5	576.00	4400.87
6 I 0	6	578.00	4400.87
7 I 0	7	580.00	4400.87
8 I 0	8	571.00	4402.60
9 I 0	9	573.00	4402.60
10 I 0	10	575.00	4402.60
11 I 0	11	577.00	4402.60
12 I 0	12	579.00	4402.60
13 I 0	13	572.00	4404.33
14 I 0	14	574.00	4404.33
15 I 0	15	576.00	4404.33
16 I 0	16	578.00	4404.33
17 I 0	17	580.00	4404.33
18 I 0	18	571.00	4406.06
19 I 0	19	573.00	4406.06
20 I 0	20	575.00	4406.06
21 I 0	21	577.00	4406.06
22 I 0	22	579.00	4406.06
23 I 0	23	572.00	4407.79
24 I 0	24	574.00	4407.79
25 I 0	25	576.00	4407.79
26 I 0	26	578.00	4407.79
27 I 0	27	580.00	4407.79

DAY 1.HR 1. TO DAY366.HR24.
(MICROGRAMS/H*3)

2.79
2.23
6.99
9.86
19.52
17.77
8.21
7.90
9.06
10.55
16.46
15.38
9.14
10.01
11.99
13.37
16.48
7.46
9.57
11.77
11.76
13.87
8.34
9.09
12.57
11.29
* 21.17

FIVE HIGHEST 1-HOUR S02 CONCENTRATIONS((ENDING ON JULIAN DAY, HOUR)
(MICROGRAMS/H*H3)

RECEPTOR	1	2	3	4	5
1(566.00,4405.00)	100.14 (179, 4)	98.00 (247,22)	96.11 (186,24)	95.71 (254,20)	94.95 (163,24)
2(564.00,4401.50)	122.26 (138,21)	122.20 (187, 4)	119.62 (164, 4)	101.19 (306, 3)	101.18 (306, 6)
3(572.00,4400.87)	235.41 (35, 1)	204.90 (237, 6)	195.26 (300, 6)	192.58 (34,19)	190.33 (354, 1)
4(574.00,4400.87)	256.45 (78,20)	251.78 (214, 4)	247.02 (169, 2)	234.39 (257,20)	232.83 (192,22)
5(576.00,4400.87) *	850.35 (46, 2)	842.20 (177,24)	814.30 (296,23)	814.27 (223,21)	810.23 (253,22)
6(578.00,4400.87)	544.43 (14, 1)	540.13 (191, 4)	468.30 (14, 2)	466.61 (10,19)	446.52 (335,21)
7(580.00,4400.87)	265.72 (291, 3)	249.00 (75, 6)	215.84 (297, 2)	207.32 (200,20)	192.70 (318, 6)
8(571.00,4402.60)	185.21 (163,24)	184.93 (186,24)	182.44 (247,22)	182.35 (179, 4)	176.37 (254,20)
9(573.00,4402.60)	278.76 (300, 6)	252.90 (35, 1)	225.15 (293, 4)	203.96 (159,22)	203.96 (244, 1)
10(575.00,4402.60)	217.13 (341,23)	207.09 (45,20)	204.31 (147, 1)	203.74 (181, 3)	203.74 (346,22)
11(577.00,4402.60)	340.83 (209, 6)	340.80 (242, 1)	327.57 (183,24)	311.81 (246,23)	311.36 (260,24)
12(579.00,4402.60)	559.53 (35, 1)	559.12 (300, 6)	449.94 (289, 6)	396.90 (34,19)	390.39 (271,21)
13(572.00,4404.33)	339.07 (164, 4)	302.47 (206,24)	290.65 (138,21)	290.18 (187, 4)	275.05 (319, 5)
14(574.00,4404.33)	237.85 (206, 5)	196.64 (153,23)	192.26 (177, 1)	189.29 (34,20)	184.77 (58,24)
15(576.00,4404.33)	254.94 (206, 5)	224.84 (58,24)	199.26 (245, 3)	197.08 (153,23)	179.39 (185, 4)
16(578.00,4404.33)	299.77 (46, 3)	262.03 (209, 1)	254.26 (269, 6)	241.97 (11, 4)	234.18 (329, 4)
17(580.00,4404.33)	404.52 (187,24)	393.52 (259,22)	390.45 (230,24)	384.75 (299, 3)	291.99 (287,23)
18(571.00,4406.06)	223.36 (290, 4)	196.18 (223,21)	193.14 (290, 3)	190.85 (218, 4)	190.32 (263,24)
19(573.00,4406.06)	259.07 (47,22)	238.70 (208,22)	213.72 (191,23)	207.32 (111,23)	194.16 (153,24)
20(575.00,4406.06)	267.97 (345,12)	246.23 (231,24)	232.25 (157, 4)	220.59 (206, 4)	213.11 (24, 6)
21(577.00,4406.06)	310.08 (206,24)	295.92 (178, 3)	295.74 (179, 6)	249.53 (164, 4)	248.20 (188, 2)
22(579.00,4406.06)	229.33 (297, 1)	199.47 (330,12)	193.14 (219, 6)	183.37 (293, 4)	178.98 (296,21)
23(572.00,4407.79)	213.94 (187, 3)	209.33 (106, 6)	200.93 (300, 3)	178.27 (269, 7)	175.43 (209, 1)
24(574.00,4407.79)	293.46 (206,23)	257.91 (307,22)	246.55 (30,19)	233.21 (207,24)	222.89 (223,21)
25(576.00,4407.79)	280.75 (264, 1)	275.70 (184, 3)	263.19 (257,21)	261.57 (154, 3)	260.40 (220, 3)
26(578.00,4407.79)	292.61 (209, 1)	291.10 (11, 4)	272.88 (286, 1)	271.80 (208, 4)	251.34 (232,23)
27(580.00,4407.79)	264.71 (230,24)	264.29 (187,24)	253.06 (259,22)	251.38 (292, 8)	250.58 (299, 3)

FIVE HIGHEST 3-HOUR S02 CONCENTRATIONS((ENDING ON JULIAN DAY, HOUR)
(MICROGRAMS/M**3)
C-FLAG IDENTIFIES CONCENTRATIONS AFFECTED BY CALM HOURS

RECEPTOR

	1	2	3	4	5
1(566.00,4405.00)	54.32 (163,24)	46.00 (213,24)	45.95 (169, 3)	43.95 (284,24)	41.05 (153,24)
2(564.00,4401.50)	77.26 (164, 6)	53.77 (153,24)	53.45 (58,24)	52.29 (250, 6)	51.58 (306, 3)
3(572.00,4400.87)	98.15 (34,21)	94.18 (122, 3)	91.43 (312,24)	91.17 (354, 3)	83.88 (29, 6)
4(574.00,4400.87)	170.56 (78,21)	135.10 (169, 3)	124.05 (214, 6)	109.73 (214, 3)	108.61 (257,21)
5(576.00,4400.87)	426.77 (344,21) *	374.25 (243, 6)	358.46 (46, 3)	351.71 (345, 6)	349.64 (214, 6)
6(578.00,4400.87)	385.75 (14, 3)	277.54 (310,21)	251.49 (104,24)	203.15 (279,21)	201.63 (89, 3)
7(580.00,4400.87)	110.90 (141, 3)	106.48 (297, 3)	103.40 (293, 3)	97.34 (14, 3)	93.86 (75, 6)
8(571.00,4402.60)	134.37 (164, 3)	120.49 (242,24)	113.82 (18,21)	109.05 (163,24)	105.05 (181,24)
9(573.00,4402.60)	112.85 (293, 6)	95.23 (58,24)	93.24C (309, 3)	92.92C (300, 6)	84.30C (35, 3)
10(575.00,4402.60)	103.49 (241, 3)	99.59 (14, 3)	98.64 (233, 3)	96.94 (354, 3)	94.58 (265, 3)
11(577.00,4402.60)	199.01 (197, 4)	189.42C (298,21)	185.59 (347,21)	179.91 (54, 3)	158.84 (60, 3)
12(579.00,4402.60)	196.33 (34,24)	191.41 (304, 3)	186.51C (35, 3)	186.37C (300, 6)	181.52 (91,24)
13(572.00,4404.33)	171.85 (164, 6)	150.39 (188, 3)	120.24 (246, 6)	117.94 (178, 6)	115.65C (298,21)
14(574.00,4404.33)	109.79 (116, 6)	105.77 (11, 6)	99.47 (58,24)	88.13 (304,24)	87.86 (354, 3)
15(576.00,4404.33)	114.46 (58,24)	92.49 (50, 6)	85.85C (206, 6)	85.33 (160, 6)	82.31C (205, 3)
16(578.00,4404.33)	125.23 (312, 6)	121.83 (198, 6)	114.47 (290, 3)	111.90 (65,24)	110.47 (34,24)
17(530.00,4404.33)	232.18 (299, 3)	203.16 (156, 6)	197.77 (155,24)	197.73 (65,24)	189.85C (280,24)
18(571.00,4406.06)	117.63 (288, 6)	105.99 (58,24)	104.25 (312,24)	101.56 (303,24)	93.05 (290, 6)
19(573.00,4406.06)	142.52 (164, 3)	122.23 (153,24)	111.84 (47,24)	101.37 (228,24)	99.96 (242,24)
20(575.00,4406.06)	127.74 (19,15)	120.34 (307, 9)	120.28 (104, 3)	117.76 (159,24)	116.62 (332,24)
21(577.00,4406.06)	153.83 (188, 3)	129.89 (178, 6)	126.35 (164, 6)	112.68C (260,21)	104.13C (206,24)
22(579.00,4406.06)	137.20 (153, 6)	135.62 (148,24)	131.38 (13, 3)	131.04 (94,21)	129.55 (330,12)
23(572.00,4407.79)	103.87C (106, 6)	102.79C (201,24)	89.19 (344,21)	72.58 (11, 6)	71.31C (187, 3)
24(574.00,4407.79)	153.00 (30,21)	114.49 (48, 6)	112.42C (200,24)	112.36 (49, 6)	109.66 (174,24)
25(576.00,4407.79)	154.54 (241, 3)	145.82 (160, 6)	143.79 (197,24)	140.79 (198, 6)	139.18 (137, 3)
26(578.00,4407.79)	144.29 (227,24)	131.11C (29, 3)	121.42 (48, 3)	102.33C (209, 3)	99.20 (289,21)
27(500.00,4407.79)	194.91 (299, 3)	191.71 (156, 6)	187.85 (338, 3)	171.47 (196,24)	169.05 (105, 6)

FIVE HIGHEST 8-HOUR SO2 CONCENTRATIONS((ENDING ON JULIAN DAY, HOUR)
(MICROGRAMS/H*3)
C-FLAG IDENTIFIES CONCENTRATIONS AFFECTED BY CALM HOURS

RECEPTOR	1	2	3	4	5
1(566.00,4405.00)	35.04 (11, 8)	32.54 (169, 8)	30.82 (46, 8)	28.99 (214, 8)	28.58C (304,24)
2(564.00,4401.50)	46.96C (306, 8)	46.42 (164, 8)	35.21C (250, 8)	32.25C (50,24)	30.53 (246, 8)
3(572.00,4400.87)	68.85 (34,24)	60.92 (297, 8)	58.10 (291, 8)	55.42C (249, 8)	48.98C (312,24)
4(574.00,4400.87)	95.44C (78,24)	88.73 (214, 8)	83.07C (247, 8)	81.07C (329, 8)	77.65 (169, 8)
5(576.00,4400.87) *	265.05C (306, 8) *	217.53 (344,24)	200.36C (260, 8)	199.43C (285,24)	190.36C (243, 8)
6(578.00,4400.87)	205.04C (14, 8)	160.47C (191, 8)	139.93 (310,24)	137.89C (33, 8)	136.81C (279,24)
7(580.00,4400.87)	76.74C (14, 8)	72.40C (293, 8)	68.62 (297, 8)	64.39 (291, 8)	62.05C (191, 8)
8(571.00,4402.60)	91.04C (285,24)	82.26C (181,24)	78.58C (251, 8)	67.65 (11, 8)	63.14 (163,24)
9(573.00,4402.60)	64.69C (58,24)	61.75 (33,24)	58.82C (300, 8)	58.34C (254,24)	55.67C (274, 8)
10(575.00,4402.60)	71.55 (354, 8)	61.59C (66, 8)	59.90C (261,24)	59.44C (311, 8)	58.41C (48,24)
11(577.00,4402.60)	172.25C (320, 8)	153.99C (66, 8)	129.28 (265, 8)	128.93C (298,24)	117.87 (347,24)
12(579.00,4402.60)	166.76C (304, 8)	155.27C (289, 8)	144.29 (34,24)	118.27 (33,24)	109.72 (271,24)
13(572.00,4404.33)	101.85C (178, 8)	89.28C (66, 8)	78.77C (320, 8)	77.41C (189, 8)	70.34C (306, 8)
14(574.00,4404.33)	68.18 (116, 8)	64.40C (206, 8)	62.06C (300, 8)	60.34C (304,24)	59.55 (11, 8)
15(576.00,4404.33)	68.18 (284, 8)	57.90 (45, 8)	54.88C (184, 8)	52.33 (50,16)	51.88C (206, 8)
16(570.00,4404.33)	79.12C (198, 8)	76.14 (54, 8)	74.15C (266,24)	71.03C (208, 8)	68.77C (127, 8)
17(590.00,4404.33)	152.51 (299, 8)	147.91C (220, 8)	139.71C (231, 8)	138.71C (266, 8)	138.44 (105, 8)
18(571.00,4406.06)	80.88C (288, 8)	72.70 (290, 8)	66.28C (58,24)	51.87C (312,24)	51.47C (78,24)
19(573.00,4406.06)	79.88C (285,24)	74.73C (264, 8)	60.12 (153,24)	60.03C (208,24)	58.94 (164, 8)
20(575.00,4406.06)	91.56 (104, 8)	86.83C (320, 8)	81.90 (275,24)	81.25 (19,16)	75.63C (360,16)
21(577.00,4406.06)	116.15C (178, 8)	78.06C (188, 8)	61.69C (319, 8)	58.25C (260,24)	58.01 (285, 8)
22(579.00,4406.06)	88.43 (12,24)	84.17 (149, 8)	77.57 (153, 8)	77.54 (13, 8)	76.41C (289, 8)
23(572.00,4407.79)	56.19C (106, 8)	55.63C (187, 8)	54.90C (260, 8)	53.65C (248, 8)	52.36C (243, 8)
24(574.00,4407.79)	89.44C (30,24)	66.78 (306,24)	63.48 (307, 8)	60.53C (200,24)	59.41C (174,24)
25(576.00,4407.79)	96.61C (66, 8)	90.43C (266,24)	89.98C (127, 8)	89.00 (137, 8)	87.44C (264, 8)
26(578.00,4407.79)	76.74C (227, 8)	72.12C (29, 8)	65.22C (209, 8)	59.78 (117,24)	57.91 (227,24)
27(580.00,4407.79)	143.31 (299, 8)	125.94 (105, 8)	125.21C (301, 8)	124.26C (220, 8)	122.90 (156, 8)

FIVE HIGHEST 24-HOUR S02 CONCENTRATIONS (ENDING ON JULIAN DAY, HOUR)
(MICROGRAMS/H**3)
C-FLAG IDENTIFIES CONCENTRATIONS AFFECTED BY CALM HOURS

RECEPTOR	1	2	3	4	5
1(566.00,4405.00)	15.40C (180,24)	15.35C (169,24)	14.97 (11,24)	14.69C (319,24)	13.52C (285,24)
2(564.00,4401.50)	17.48C (285,24)	16.65C (206,24)	15.49 (305,24)	15.49 (164,24)	14.73 (228,24)
3(572.00,4400.87)	36.69 (34,24)	35.98C (297,24)	30.98 (340,24)	30.87C (249,24)	28.53C (307,24)
4(574.00,4400.87)	40.82 (214,24)	39.01C (359,24)	34.56C (78,24)	33.36C (247,24)	32.75C (206,24)
5(576.00,4400.87) *	108.50C (285,24) *	94.57 (228,24)	85.71C (306,24)	84.27C (344,24)	83.84C (260,24)
6(578.00,4400.87)	80.43C (310,24)	74.82C (341,24)	74.79C (191,24)	70.98C (53,24)	59.30C (14,24)
7(580.00,4400.87)	32.71C (297,24)	31.86C (291,24)	31.62C (593,24)	30.65 (326,24)	28.77C (341,24)
8(571.00,4402.60)	47.17C (181,24)	45.66C (285,24)	39.52C (251,24)	37.56C (124,24)	36.46C (180,24)
9(573.00,4402.60)	39.14 (34,24)	32.16C (35,24)	28.94C (58,24)	27.15C (33,24)	26.93C (48,24)
10(575.00,4402.60)	31.96C (48,24)	30.22C (264,24)	29.62C (313,24)	29.53C (237,24)	29.32 (345,24)
11(577.00,4402.60)	63.27C (66,24)	62.15C (237,24)	59.93C (320,24)	56.93C (265,24)	56.77C (298,24)
12(579.00,4402.60)	89.80 (34,24)	67.68C (304,24)	66.59C (313,24)	53.72C (297,24)	53.50C (289,24)
13(572.00,4404.33)	38.19C (178,24)	36.55C (66,24)	32.48C (298,24)	31.73C (142,24)	31.62 (305,24)
14(574.00,4404.33)	47.00 (34,24)	44.46 (272,24)	39.47C (274,24)	38.34 (116,24)	34.44C (300,24)
15(576.00,4404.33)	41.64 (50,24)	37.77C (45,24)	34.77 (330,24)	34.22C (208,24)	29.64C (310,24)
16(578.00,4404.33)	40.18C (266,24)	38.40C (35,24)	36.20 (34,24)	35.86C (287,24)	35.00C (198,24)
17(500.00,4404.33)	79.67C (299,24)	73.97C (220,24)	63.92 (327,24)	60.57C (301,24)	60.21C (287,24)
18(571.00,4406.06)	32.33C (288,24)	30.98 (590,24)	30.14C (312,24)	27.62C (206,24)	27.32C (59,24)
19(573.00,4406.06)	35.53C (264,24)	34.65C (285,24)	30.84C (181,24)	29.99C (319,24)	27.46C (247,24)
20(575.00,4406.06)	49.34 (19,24)	44.09 (43,24)	43.87C (307,24)	42.45 (332,24)	41.80C (125,24)
21(577.00,4406.06)	41.83C (178,24)	35.03 (305,24)	35.03C (206,24)	33.21C (142,24)	30.51C (188,24)
22(579.00,4406.06)	57.40 (256,24)	51.15 (153,24)	46.69 (149,24)	45.88 (115,24)	45.14C (273,24)
23(572.00,4407.79)	30.08 (345,24)	26.08C (247,24)	26.06 (354,24)	24.84C (48,24)	24.03C (300,24)
24(574.00,4407.79)	49.33C (307,24)	38.79 (345,24)	37.47C (30,24)	34.93C (306,24)	31.41 (262,24)
25(576.00,4407.79)	45.46C (266,24)	44.45 (315,24)	43.31 (197,24)	42.72C (184,24)	42.69C (237,24)
26(578.00,4407.79)	47.36C (227,24)	37.70C (48,24)	35.02 (8,24)	35.02 (354,24)	34.67 (282,24)
27(580.00,4407.79)	89.69C (299,24)	79.41 (327,24)	78.90 (5,24)	71.06 (302,24)	70.29C (220,24)

THIS RUN HAS TERMINATED NORMALLY.

SECTION 11

ERROR MESSAGES AND REMEDIAL ACTION

RAM can generate up to 22 error messages, some of which cause program termination. Table 3 lists each message along with error description and suggested corrective action.

TABLE 3. ERROR MESSAGES AND CORRECTIVE ACTION

MESSAGE:	NSIGP (THE NUMBER OF SIGNIFICANT POINT SOURCES) WAS FOUND TO EXCEED THE LIMIT (25). USER TRIED TO INPUT x SOURCES. ***** EXECUTION TERMINATED *****
DESCRIPTION:	The maximum number of significant point sources allowed by the program is 25.
ACTION:	Modify the value input in record type 9 to be 25.
MESSAGE:	NSIGA (THE NUMBER OF SIGNIFICANT AREA SOURCES) WAS FOUND TO EXCEED THE LIMIT (10). USER TRIED TO INPUT x SOURCES. ****EXECUTION TERMINATED ****
DESCRIPTION:	The maximum number of significant area sources allowed by the program is 10.
ACTION:	Modify the input value to be 10.
MESSAGE:	USER TRIED TO INPUT MORE THAN x POINT SOURCES. THIS GOES BEYOND THE CURRENT PROGRAM DIMENSIONS.
DESCRIPTION:	The maximum number of point sources is 250.
ACTION:	Reduce the number of point sources to comply with the maximum of 250.

MESSAGE: USER TRIED TO INPUT MORE THAN x AREA SOURCES. THIS GOES BEYOND THE CURRENT PROGRAM DIMENSIONS.

DESCRIPTION: The maximum number of area sources is 100.

ACTION: Reduce the number of area sources to comply with the maximum of 100.

MESSAGE: DIMENSIONS TOO SMALL TO HOLD ARRAY x BY y.

DESCRIPTION: The internal dimensions of the area source array are (25,25) for internal units.

ACTION: Recompile with dimensions larger than (25,25).

MESSAGE: AREA SOURCES, UNITS OR SIDE LENGTHS SPECIFIED INCORRECTLY ERROR ON EAST MAXIMUM BOUNDARY.

DESCRIPTION: The area source east boundary extends beyond the east boundary of the modeling region.

ACTION: Reduce the area source size, increase the size of the modeling region, or recompile the program with larger dimensions.

MESSAGE: AREA SOURCES, UNITS OR SIDE LENGTHS SPECIFIED INCORRECTLY ERROR ON NORTH MAXIMUM BOUNDARY.

DESCRIPTION: The area source north boundary extends beyond the north boundary of the modeling region.

ACTION: Reduce the area source size, increase the size of the modeling region, or recompile the program with larger dimensions.

MESSAGE: SOURCE, x, IS ALREADY LOCATED AT POSITION (,x,). CHECK SOURCE x.

DESCRIPTION: Two sources are collocated.

ACTION: Verify the input stream and separate or combine the collocated sources.

MESSAGE: AREA ARRAY IS TOO WIDE FOR PAGE SIZE, THEREFORE WILL NOT BE PRINTED.

DESCRIPTION: The area source array cannot be printed due to its size.

ACTION: If a printout is needed, reduce the size of the area source region.

MESSAGE: ***ERROR---USER TRIED TO SPECIFY, x, SIGNIFICANT SOURCES BUT IS ONLY ALLOWING, y, TOTAL SIGNIFICANT SOURCES IN THIS RUN. RUN TERMINATED-CHECK INPUT DATA.

DESCRIPTION: The number of significant sources exceeds the total significant sources specified.

ACTION: Verify consistency of significant sources in the input stream.

MESSAGE: (MPS) THE INPUT SIGNIFICANT SOURCE NUMBER WAS FOUND TO EQUAL ZERO - USER CHECK INPUT DATA.

DESCRIPTION: The number of significant sources exceeds the total significant sources specified.

ACTION: Verify consistency of significant sources in the input stream.

MESSAGE: THE INPUT LIMIT OF MAXIMUM DISTANCE FOR AREA INTEGRATION, x, CONVERTS TO y KM WHICH EXCEEDS STORAGE LIMITATIONS. UP TO 116 KM DISTANCES ARE ALLOWED.

DESCRIPTION: The maximum distance for area source integration was exceeded.

ACTION: Modify the limit such that the distance does not exceed 116 km.

MESSAGE: ERROR IN SPECIFYING SIGNIFICANT POINT SOURCES.

DESCRIPTION: The significant point sources were not input properly.

ACTION: Verify the input stream and correct as needed.

MESSAGE: DISAGREEMENT OF IDENTIFIERS- SURFACE DATA FROM CARD:
STATION = x, YEAR = x. FROM MET FILE: STATION = y, YEAR
= y. MIXING HEIGHT DATA FROM CARD: STATION = x, YEAR = x.
FROM MET FILE: STATION = y, YEAR = y.

DESCRIPTION: Header information in the meteorological file is not in
agreement with that specified in the input stream.

ACTION: Modify the input stream or replace the meteorological
data set to effect a match.

MESSAGE: ****USER EITHER TRIED TO INPUT MORE THAN 180 RECEPTORS OR
ENDR WAS NOT PLACED AFTER THE LAST RECEPTOR CARD.
*****EXECUTION TERMINATED*****

DESCRIPTION: The maximum number of user-specified receptors is 180,
and a record with ENDR in columns 1-4 is required to
signify the end of receptor input.

ACTION: Modify the input as needed.

MESSAGE: NO RECEPTORS HAVE BEEN CHOSEN.

DESCRIPTION: Either user-input or program-generated receptors are
required. Neither type was specified.

ACTION: Correct the input stream to specify receptors.

MESSAGE: DAYS DO NOT MATCH, IDAY = x, IDAYS = Y.

DESCRIPTION: If the run is part of a segmented run, the starting day
must match the day in the prior run.

ACTION: Modify the input stream to effect a match.

MESSAGE: RUN TERMINATED. CAN NOT WRITE FILES (OPTIONS 41 OR 42)
WHEN HAVING RAM GENERATE RECEPTORS FOR EACH AVERAGING
PERIOD, (OPTIONS 15,16,17).

DESCRIPTION: Options 41 or 42 are not compatible with options 15,
16, 17.

ACTION: Modify the input stream to ensure compatibility.

MESSAGE: DATE ON MET TAPE, x, DOES NOT MATCH INTERNAL DATE, y.

DESCRIPTION: The Julian date calculated by RAM does not match the date
in the input meteorological tape.

ACTION: Verify the proper data sequence in the input meteorology.

MESSAGE: HOUR, x, IS NOT PERMITTED. HOURS MUST BE DEFINED BETWEEN
1 AND 24.

DESCRIPTION: The hour specified is other than 1-24.

ACTION: Modify the input to conform to the hour stipulation
required by RAM.

MESSAGE: DATE BEING PROCESSED IS = x. DATE OF HOURLY POINT
EMISSION RECORD IS y. ***PLEASE CHECK EMISSION RECORDS.

DESCRIPTION: In the point emission record in process, the date does
not match the internal date calculated by RAM.

ACTION: Verify data sequence in the hourly area source emission
file.

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APPENDIX A

FORTTRAN SOURCE CODE FOR RAM

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C          RAMMET (VERSION 84136)                                RME00010
C          A MET PREPROCESSOR FOR RAM IN                          RME00020
C          SECTION 1. GUIDELINE MODELS                            RME00030
C          IN UNAMAP (VERSION 6) JULY 86                          RME00040
C          SOURCE: UNAMAP FILE ON EPA'S UNIVAC 1110, RTP, NC    RME00050
C***RAMMET-PREPROCESSOR- WRITTEN BY JOAN HRENKO NOVAK           RME00060
C*** BASED ON METHODS SUGGESTED BY TURNER , ZIMMERMAN, AND IRWIN. RME00070
C***RAMMET ASSUMES THERE IS NO MISSING DATA ON THE MET. TAPE.  RME00080
C***IF MISSING DATA IS DETECTED, THE LOCATION OF THE MISSING DATA IS RME00090
C***PRINTED. MISSING DATA MUST BE FILLED IN BEFORE PROCEEDING . RME00100
C          COMMON SEED,IRN,IRNP                                  RME00110
C          DIMENSION LSTAB(12,7), IDFAC(12,2), ANGL(3), ICEIL(3), IDG(3), IDIRME00120
C          1G(11)                                                RME00130
C          DIMENSION KST(24), SPEED(24), TEMP(24), AFV(24), FVR(24), HLH(2,24)RME00140
C          1)                                                    RME00150
C          DIMENSION IRAND(8784),IRND(24,366)                    RME00160
C          EQUIVALENCE (IRAND,IRND)                              RME00170
C          DATA IDIG /'0','1','2','3','4','5','6','7','8','9','-'/' RME00180
C          DATA IREC /1/,IMO /1/,ANGL /60.,35.,15./,CONST /57.29578/ RME00190
C          DATA IDFAC /0,31,59,90,120,151,181,212,243,273,304,334,0,31,60,91, RME00200
C          1121,152,182,213,244,274,305,335/                      RME00210
C          DATA LSTAB /7,7,7,6,6,6,5,5,5,5,4,4,6,6,6,5,5,5,4,4,4,4,4,4,4,4, RME00220
C          14,4,4,4,4,4,4,3,3,3,4,4,4,4,4,4,4,4,2,2,2,3,3,3,3,3,4,4,4, RME00230
C          21,2,2,2,2,2,2,3,3,3,3,4,1,1,1,1,1,2,2,2,2,2,3,3,3/ RME00240
C***      UNIT 8 = SURFACE DATA                                  RME00250
C***      UNIT 9 = OUTPUT FILE                                    RME00260
C***      UNIT 5 = UPPER AIR DATA IN CARD FORMAT               RME00270
C***      UNIT 12 = RANDOM NUMBERS                               RME00280
C          CALL WSTCLK
C          WRITE (6,5432)
C          5432 FORMAT ('1',21X,'RAMMET (VERSION 84136)'/
C          1 22X,'A MET PREPROCESSOR FOR RAM IN'/
C          2 22X,'SECTION 1. GUIDELINE MODELS '/
C          3 22X,'IN UNAMAP (VERSION 6) JULY 86'/
C          4 22X,'SOURCE: UNAMAP FILE ON EPA'S UNIVAC 1110, RTP, NC.')
```

IN=5
IO=6
IFLAG=0
READ (5,395) IRN,IRNP,ISK
395 FORMAT (312)

OPTIONAL FEATURES:

IRN - CONTROL FOR RANDOM NUMBERS.
0 READ PREVIOUSLY PREPARED RANDOM NUMBERS FROM FILE 12.
1 GENERATE A SET OF RANDOM NUMBERS USING THE UNIVAC LIBRARY
SUBROUTINE RANDU.
2 GENERATE A SET OF RANDOM NUMBERS USING THE IMSL LIBRARY
SUBROUTINE GGUBS.
3 GENERATE A SET OF RANDOM NUMBERS USING A USER PROVIDED
ROUTINE ACCESSED BY USER WRITTEN CODE AT STATEMENT 170
IN SUBROUTINE RNDM.

IRNP - CONTROL FOR RANDOM NUMBER LISTING AND ANALYSIS.
0 PROVIDE AND PRINT ANALYSIS.
1 DON'T.

ISK - CONTROL FOR USING OPAQUE OR TOTAL SKY COVER.
OPAQUE IS PREFERRED.
0 USE OPAQUE (COL79).
1 USE TOTAL (COL 56).

WRITE (6,397) IRN,IRNP,ISK
397 FORMAT ('0IRN = ',12,' CONTROL FOR RANDOM NUMBERS.'/

1 '0 - READ FROM FILE 12.'/ 1 - GENERATE USING UNIVAC RANDU.'/ RME00620
2 '2 - GENERATE USING IMSL GGUBS.'/ 3 - GENERATE USING USER'S RME00630
3ROUTINE.'/ 0IRNP = ',12,' CONTROL FOR RANDOM NUMBER LISTING AND ANRME00640
4ALYSIS.'/ 0 - PROVIDE AND PRINT ANALYSIS.'/ 1 - DON'T.'/ RME00650
5 '0ISK = ',12,' CONTROL FOR SKY COVER.'/ RME00660
6 '0 - USE OPAQUE (COL 79).'/ 1 - USE TOTAL (COL 56).'/ RME00670
C***READ CARD TO INITIALIZE MET TAPE ID, YEAR, LATITUDE, LONGITUDE, RME00680
C*** TIME ZONE ,NO. OF DAYS IN YEAR, INITIAL RANDOM NUMBER. RME00690


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****RAND(24) IS THE INITIAL RANDOM NO. USED TO GENERATE THE SEQUENCE OF RME00700
****NUMBERS FOR THE RANDOMIZED FLOW VECTOR. IF THE SAME NO. IS USED IN RME00710
****DIFFERENT EXECUTIONS OF THE PREPROCESSOR, THE SAME SET OF RANDOM NOS RME00720
****WILL BE GENERATED. ANY ODD NUMBER GREATER THAN 3 DIGITS CAN BE USED RME00730
****AS THE SEED. THIS SEED IS MULTIPLIED BY 10,000 INTERNALLY. RME00740
****ZONE IS GMT-LST. RME00750
      READ (IN,400) IDC,IYRC,ALAT,ALONG,ZONE,NDAYS,SEED RME00760
      WRITE (IO,410) IDC,IYRC,ALAT,ALONG,ZONE,NDAYS,SEED RME00770
C      IDC STATION IDENTIFICATION FOR SURFACE OBSERVATION TAPE RME00780
C      IYRC YEAR OF METEOROLOGICAL DATA RME00790
C      ALAT LATITUDE OF SITE RME00800
C      ALONG LONGITUDE OF SITE RME00810
C      ZONE TIME ZONE OF SITE RME00820
C      NDAYS NUMBER OF DAYS TO BE PROCESSED RME00830
C      SEED NUMBER USED AS SEED FOR RANDOM NUMBER GENERATION RME00840
C RME00850
      CALL RNDM(IRAND) RME00860
      DUM=ALAT/CONST RME00870
      SINLAT=SIN(DUM) RME00880
      COSLAT=COS(DUM) RME00890
      DUM=ALONG/15.-ZONE RME00900
      TEMPZ=15.*ZONE-ALONG RME00910
****RESET SUBSCRIPT IF LEAP YEAR RME00920
      LYS=1 RME00930
      IF (NDAYS.EQ.366) LYS=2 RME00940
****READ MET DATA RME00950
****THIS READ ASSUMES AN INPUT TAPE WITH HOURLY DATA FROM THE RME00960
****NATIONAL CLIMATIC CENTER, ASHVILLE, NC. IN THEIR STANDARD RME00970
****HOURLY CARD FORMAT. RME00980
****SKIP 00 HOUR OF MET DATA. RME00990
      READ (8,420) ID,IYEAR,IMONTH,IDAY,IHOUR,ICEIL,IDIR,ISPEED,ITEMP,ITRME01000
      LOAMT,ICOVER RME01010
      LWD=IDIR RME01020
****BEGIN PROCESSING WITH HOUR 01 RME01030
      READ (8,420) ID,IYEAR,IMONTH,IDAY,IHOUR,ICEIL,IDIR,ISPEED,ITEMP,ITRME01040
      LOAMT,ICOVER RME01050
****MIXING HEIGHT VALUES ARE DETERMINED TWICE A DAY FROM RADIOSONDE DATA RME01060
****USING THE PROCEDURES OF HOLZWORTH. RME01070
****READ PRIOR DAYS MIXING HEIGHT VALUES RME01080
      READ (IN,430) XMNML,XAFML RME01090
****PRESENT DAY RME01100
      READ (IN,440) IDM,IYM,XMN,XAF RME01110
****WRITE IDENTIFYING INFORMATION ON OUTPUT FILE RME01120
      WRITE (9) ID,IYEAR,IDM,IYM RME01130
      WRITE (IO,450) IYEAR,ID,IYM,IDM RME01140
**** READ NEXT DAY'S MIXING HEIGHT VALUES RME01150
      READ (IN,430) XMNPL,XAFPL RME01160
****START DAY LOOP. RME01170
      DO 380 IDY=1,NDAYS RME01180
****CALCULATE THE DAY NO AND THE TIME OF SUNRISE AND SUNSET RME01190
      DAY1=IDAY+IDFAC(IMONTH,LYS) RME01200
****CONSTANT 0.0172028=360./365.242*57.29578 RME01210
****DETERMINE THE ANGULAR(RADIANS) FRACTION OF A YEAR FOR THIS DATE. RME01220
      DAYNO=(DAY1-1.0)*0.0172028 RME01230
      TDAYNO=2.*DAYNO RME01240
      SIND=SIN(DAYNO) RME01250
      COSD=COS(DAYNO) RME01260
      SINTD=SIN(TDAYNO) RME01270
      COSTD=COS(TDAYNO) RME01280
****ACCOUNT FOR ELLIPTICITY OF EARTH'S ORBIT. RME01290
      SIGMA=279.9348+(DAYNO*CONST)+1.914827*SIND-0.079525*COSD+0.019938* RME01300
      ISINTD=0.00162*COSTD RME01310
****CONSTANT 0.39785=SIN(.4091720193=23.44383/57.29578) RME01320
****FIND THE SINE OF THE SOLAR DECLINATION. RME01330
      DSIN=0.39785*SIN(SIGMA/CONST) RME01340
      DCOS=SQRT(1.0-DSIN*DSIN) RME01350
****DETERMINE TIME(HRS) OF MERIDIAN PASSAGE RME01360
      AMM=12.0+0.12357*SIND-0.004289*COSD+0.153809*SINTD+0.060783*COSTD RME01370
      HCOS=(-SINLAT*DSIN)/(COSLAT*DCOS) RME01380
      RME01390

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C***DETERMINE SOLAR HOUR ANGLE OF SUNRISE-SUNSET.	RME01400
H2=(ATAN2(SQRT(1.-HCOS*HCOS),HCOS)/15.0)*CONST	RME01410
C***TIME OF SUNRISE(TSR) AND TIME OF SUNSET(TSS) ARE EXPRESSED IN	RME01420
C***LOCAL STANDARD TIME SINCE THE ZONE CORRECTION HAS ALREADY BEEN MADE.	RME01430
C***OTHERWISE THEY WOULD BE IN GREENWICH MEAN TIME.	RME01440
TSR=AMM-H2+DUM	RME01450
TSS=AMM+H2+DUM	RME01460
C***START HOUR LOOP	RME01470
DO 370 KHR=1,24	RME01480
KHRC=KHR	RME01490
C***INITIALIZE STABILITY BEFORE IT IS CALCULATED	RME01500
KST(KHR)=0	RME01510
IF (KHR.EQ.24) GO TO 70	RME01520
C***CHECK DATA FOR CORRECTNESS & CONTINUITY	RME01530
C***CHECK STATION NUMBER.	RME01540
IF (ID.EQ.IDC) GO TO 10	RME01550
WRITE (IO,460) IREC,ID,IDC	RME01560
WRITE (IO,510)	RME01570
CALL WAUDIT	
STOP	RME01580
C***CHECK YEAR.	RME01590
10 IF (IYEAR.EQ.IYRC) GO TO 20	RME01600
WRITE (IO,470) IYEAR,IYRC,IREC	RME01610
WRITE (IO,510)	RME01620
CALL WAUDIT	
STOP	RME01630
C***CHECK MONTH	RME01640
20 IF (IMONTH.EQ.IMO) GO TO 40	RME01650
IF (IMONTH.EQ.(IMO+1)) GO TO 30	RME01660
WRITE (IO,480) IMONTH,IMO,IREC	RME01670
C***	RME01680
WRITE (IO,510)	RME01690
CALL WAUDIT	
STOP	RME01700
30 IMO=IMONTH	RME01710
C***CHECK DAY	RME01720
40 IF (IFIX(DAY1).EQ.IDY) GO TO 50	RME01730
WRITE (IO,490) DAY1,IDY,IREC	RME01740
WRITE (IO,510)	RME01750
CALL WAUDIT	
STOP	RME01760
C***CHECK HOUR	RME01770
50 IF (IHOURL.EQ.KHRC) GO TO 80	RME01780
WRITE (IO,500) IHOURL,KHR,IREC	RME01790
WRITE (IO,510)	RME01800
GO TO 370	RME01810
60 WRITE (IO,520) KHR,IREC,IHOURL	RME01820
CALL WAUDIT	
STOP	RME01830
70 IF (IHOURL.NE.0) GO TO 60	RME01840
KHRC=IHOURL	RME01850
C***UPDATE MIXING HEIGHTS- STARTING NEW DAY.	RME01860
XNMN1=XMN	RME01870
XAFM1=XAF	RME01880
XMN=XMNP1	RME01890
XAF=XAFP1	RME01900
C***READ NEXT DAYS MIXING HEIGHTS.	RME01910
READ (IN,430,END=80) XMNP1,XAFP1	RME01920
80 ICDAMT=ICOVER	RME01930
IF (ISK.EQ.1) ICDAMT=ITOAMT	RME01940
JK=0	RME01950
90 JK=JK+1	RME01960
IF (ICDAMT.NE.IDIG(JK)) GO TO 90	RME01970
ISKY=JK-1	RME01980
IF (ICEIL(1).NE.IDIG(11)) GO TO 110	RME01990
IDG(1)=9	RME02000
IDG(2)=9	RME02010
IDG(3)=8	RME02020
GO TO 150	RME02030
110 DO 140 J1=1,3	RME02040

DO 120 JK=1,10	RME02050
IF (ICEIL(JI).EQ.IDIG(JK)) GO TO 130	RME02060
120 CONTINUE	RME02070
130 IDG(JI)=JK-1	RME02080
140 CONTINUE	RME02090
150 IROOF=IDG(1)*100+IDG(2)*10+IDG(3)	RME02100
C***IROOF IS CEILING HEIGHT IN HUNDREDS OF FEET.	RME02110
C***CONVERT TEMP FROM FAHRENHEIT TO KELVIN	RME02120
TEMP(KHR)=0.5556*(ITEMP-32.)+273.15	RME02130
C***CONVERT WIND SPEED FROM KNOTS TO METERS/SEC	RME02140
S=ISPEED*0.51444	RME02150
C***WIND SPEED IS SET TO 1 METER/SEC	RME02160
IF (S.LT.1.0) S=1.0	RME02170
SPEED(KHR)=S	RME02180
C***CHECK FOR CALMS	RME02190
IF (IDIR.EQ.0) GO TO 160	RME02200
C***WIND DIRECTION IS ASSUMED TO BE THE SAME AS FOR THE LAST HOUR	RME02210
C***IF THE WIND DIRECTION IS REPORTED AS "CALM".	RME02220
LWD=IDIR	RME02230
GO TO 170	RME02240
160 IDIR=LWD	RME02250
170 XDIR=IDIR*10.	RME02260
C***CALCULATE FLOW VECTOR AND RANDOM FLOW VECTOR	RME02270
IF (XDIR.GT.180.) GO TO 180	RME02280
FV=XDIR+180.	RME02290
GO TO 190	RME02300
180 FV=XDIR-180.	RME02310
190 AFV(KHR)=FV	RME02320
XRN=IRND(KHR,IDY)	RME02330
FVR(KHR)=FV+XRN-4.	RME02340
IF (FVR(KHR).GT.360.) FVR(KHR)=FVR(KHR)-360.	RME02350
C***DETERMINE RADIATION INDEX.	RME02360
IF (ISKY.EQ.10.AND.IROOF.LT.70) GO TO 200	RME02370
IF (IHOURLT.TSR.AND.IHOURLT.TSS) GO TO 210	RME02380
IRADX=2	RME02390
IF (ISKY.LE.4) IRADX=1	RME02400
GO TO 280	RME02410
200 IRADX=3	RME02420
GO TO 280	RME02430
C***DETERMINE THE ANGLE OF ELEVATION	RME02440
C***DETERMINE SOLAR HOUR ANGLE(RADIANS)	RME02450
210 HI=(15.*(KHRC-AMM)+TEMPZ)/CONST	RME02460
ALFSN=SINLAT*DSIN+DCOS*COSLAT*COS(HI)	RME02470
C***DETERMINE SOLAR ELEVATION ANGLE(DEG).	RME02480
ALF=ATAN2(ALFSN,SQRT(1.-ALFSN*ALFSN))*CONST	RME02490
DO 220 I=1,3	RME02500
220 IF (ALF.GT.ANGL(I)) GO TO 230	RME02510
I=4	RME02520
230 ICN=5-I	RME02530
IF (ISKY.GT.5) GO TO 240	RME02540
IRADX=ICN+3	RME02550
GO TO 280	RME02560
240 IRADX=ICN-1	RME02570
IF (IROOF.LT.70) GO TO 250	RME02580
IF (IROOF.LT.160) GO TO 260	RME02590
IF (ISKY.EQ.10) GO TO 270	RME02600
IRADX=ICN	RME02610
GO TO 270	RME02620
250 IRADX=ICN-2	RME02630
GO TO 270	RME02640
260 IF (ISKY.EQ.10) IRADX=IRADX-1	RME02650
270 IF (IRADX.LT.1) IRADX=1	RME02660
IRADX=IRADX+3	RME02670
280 IND=ISPEED	RME02680
IF (ISPEED.GT.12) IND=12	RME02690
IF (ISPEED.LE.1) IND=1	RME02700
C***DETERMINE STABILITY.	RME02710
KST(KHR)=LSTAB(IND,IRADX)	RME02720
C***DO NOT ALLOW STABILITY TO VARY RAPIDLY	RME02730
IF (IDY.EQ.1.AND.KHR.EQ.1) LST=KST(KHR)	RME02740

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      IF ((KST(KHR)-LST).GT.1) KST(KHR)=LST+1
      IF ((LST-KST(KHR)).GT.1) KST(KHR)=LST-1
      LST=KST(KHR)
      IF (KST(KHR).LT.1) WRITE (IO,540) KST(KHR),IND,IRADX,IREC
C***CALCULATE MIXING HEIGHT
      IHR=KHRC
      XHR=IHR
      IF (IHR.GT.14.AND.XHR.LE.TSS) GO TO 300
      IND=2
      IF (XHR.LE.TSS) GO TO 310
      IF (KST(KHR).EQ.4) GO TO 290
      HLH(2,KHR)=XAF+(XMNP1-XAF)*((XHR-TSS)/(24.-TSS))
      IND=1
290    HLH(IND,KHR)=XAF+(XAFP1-XAF)*((XHR-TSS)/(38.-TSS))
      IF (IND.EQ.2) HLH(1,KHR)=HLH(2,KHR)
      GO TO 360
300    HLH(1,KHR)=XAF
      HLH(2,KHR)=XAF
      GO TO 360
310    IF (XHR.GT.TSR) GO TO 330
      KSTSP=KST(KHR)
      IF (KST(KHR).EQ.4) GO TO 320
      HLH(2,KHR)=XMN
      IND=1
320    HLH(IND,KHR)=XAFM1+(XAF-XAFM1)*((24.-TSS+XHR)/(24.-TSS+14.))
      IF (IND.EQ.2) HLH(1,KHR)=HLH(2,KHR)
      GO TO 360
330    IF (KSTSP.EQ.4) GO TO 350
      HLH(2,KHR)=XMN+(XAF-XMN)*((XHR-TSR)/(14.-TSR))
      HLH(1,KHR)=XAF*(XHR-TSR)/(14.-TSR)
      GO TO 360
340    IFLAG=1
      IHOURL=0
      GO TO 370
350    HLH(1,KHR)=XAFM1+(XAF-XAFM1)*((24.-TSS+XHR)/(24.-TSS+14.))
      HLH(2,KHR)=HLH(1,KHR)
C***READ NEXT HOUR'S MET DATA
360    IF (IFLAG.EQ.1) GO TO 390
C***STORE CORRECT MONTH AND DAY FOR DAILY PRINTOUT, SINCE 24TH HOUR LABER
      IF(KHR.NE.23) GO TO 365
      LMON=IMONTH
      LDAY=IDAY
365    READ (8,420,END=340) ID,IYEAR,IMONTH,IDAY,IHOURL,ICEIL,IDIR,ISPEED,
      ITEMP,ITOAMT,ICOVER
      IREC=IREC+1
C***END OF HOUR LOOP.
370    CONTINUE
C***WRITE DAYS CALCULATION ON TO FILE
C***EACH ARRAY CONTAINS THE COMPLETE INFORMATION FOR ONE DAY ORDERED
C***SEQUENTIALLY FROM HOUR 01 THRU 24
      WRITE (9) IYEAR,LMON,DAY1,KST,SPEED,TEMP,AFV,FVR,HLH
      WRITE (IO,550) IYEAR,LMON,LDAY,DAY1,TSR,TSS
      WRITE (IO,560) KST
      WRITE (IO,570) SPEED,TEMP,AFV,FVR,((HLH(I,J),J=1,24),I=1,2)
C***END OF DAY LOOP.
380    CONTINUE
390    WRITE (9) IYEAR,LMON,DAY1,KST,SPEED,TEMP,AFV,FVR,HLH
      WRITE (IO,550) IYEAR,LMON,LDAY,DAY1,TSR,TSS
      WRITE (IO,560) KST
      WRITE (IO,570) SPEED,TEMP,AFV,FVR,((HLH(I,J),J=1,24),I=1,2)
      WRITE (IO,580)
      CALL WAUDIT
      STOP
C
400    FORMAT (I5,I2,1X,2F10.1,F2.0,I4,F10.0)
410    FORMAT('0',RAMMET - VERSION 84136',/1X,
      *' STATION NUMBER=',I5,5X,'YEAR OF DATA=',I2/1X,
      *' LATITUDE=',F10.1,' LONGITUDE=',F10.1,' ZONE=',F4.0/1X,
      *' NUMBER OF DAYS IN YEAR=',I3,' RANDOM SEED=',F10.0)
420    FORMAT (I5,4I2,3A1,22X,2I2,4X,I3,6X,A1,22X,A1)

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RME02750
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430 FORMAT (12X,F5.0,13X,F5.0) RME03440
440 FORMAT (15,12,5X,F5.0,13X,F5.0) RME03450
450 FORMAT (1X,'19',12,' SURFACE DATA AT STATION ',15,10X,'19',12,' MIRM RME03460
1XING HEIGHT DATA AT STATION ',15) RME03470
460 FORMAT (' ID DOES NOT MATCH IN RECORD ',14,' ID ON TAPE IS ',15,RME03480
*, ' ID REQUESTED IS ',15) RME03490
470 FORMAT (' YEAR IS',13,' INSTEAD OF ',12,' IREC=',14) RME03500
480 FORMAT (' MONTH ',12,' DOES NOT AGREE WITH LOOP ',12,' IREC=',14) RME03510
490 FORMAT (' DAY ',F4.0,' DOES NOT AGREE WITH LOOP ',12,' IREC=',14) RME03520
500 FORMAT (' HOUR ',12,' DOES NOT AGREE WITH LOOP ',12,' IREC=',14) RME03530
510 FORMAT (' *****DATA IS MISSING. PLEASE CORRECT INPUT FILE*****') RME03540
520 FORMAT (' ERROR: MISSING HOUR LOOP VALUE=',13,' WHILE VALUE ',15,RME03550
1 RECORD ',17,' IS = ',13) RME03560
530 FORMAT (' THE CHARACTER ',A1,' IS NOT ALLOWABLE.', ' CLOUD COVER DER RME03570
1FAULTS TO 10.') RME03580
540 FORMAT (' STABILITY=',4I4) RME03590
550 FORMAT (' IYEAR=',12,' IMONTH=',12,' DAY=',12,' JULIAN DAY=', RME03600
*F5.0,' SUNRISE=',F7.3,' SUNSET=',F7.3) RME03610
560 FORMAT (' KST=',24(I1,4X)) RME03620
570 FORMAT (' SPEED=',24(F4.1,1X))/' TEMP=',24(F4.0,1X))/' AFV=',24(F RME03630
14.0,1X))/' FVR=',24(F4.0,1X))/' HLH1=',12(F5.0,1X)/6X,12(F5.0,1X)/' RME03640
2HLH2=',12(F5.0,1X)/6X,12(F5.0,1X)) RME03650
580 FORMAT (' ALL RECORDS HAVE BEEN PROCESSED') RME03660
C RME03670
END RME03680
C
SUBROUTINE RNDM(IRAND) RME03690
COMMON SEED,IRN,IRNP RME03700
DIMENSION RAND(8784),IRAND(8784),IDUM(24) RME03710
DIMENSION KS(10),K2(10),K3(10),K4(10),K5(10),K6(10),KG(10) RME03720
DOUBLE PRECISION DSEED RME03730
DATA DLH,TLH,QLH,FLH,SLH/0.,0.,0.,0.,0./ RME03740
IF (IRN.GT.0) GO TO 120 RME03750
DO 8 JA = 1,366 RME03760
READ (12,1020) J,IDUM RME03770
1020 FORMAT (18,3X,24I1) RME03780
C CHECK TO SEE IF J CORRECT. RME03790
IF(J.EQ.JA) GO TO 4 RME03800
WRITE (6,1030) J,JA RME03810
1030 FORMAT(' INPUT RECORD:',14,' DOESN'T MATCH EXPECTED RECORD:',14) RME03820
4 IE = JA * 24 RME03830
IB = IE - 24 RME03840
DO 6 I = 1,24 RME03850
IS = IB + I RME03860
6 IRAND(IS) = IDUM(I) RME03870
8 CONTINUE RME03880
GO TO 150 RME03890
120 IF(IRN.GT.1) GO TO 160 RME03900
WRITE (6,1050) SEED RME03910
1050 FORMAT (' SEED USED FOR THIS RUN =',F10.0//) RME03920
C USE RANDU FROM UNIVAC LIBRARY. RME03930
RAND(1) = SEED RME03940
CALL RANDU (RAND,8784) RME03950
GO TO 190 RME03960
160 IF(IRN.GT.2) GO TO 170 RME03970
WRITE (6,1050) SEED RME03980
C USE GGUBS FROM IMSL LIBRARY. RME03990
DSEED = SEED RME04000
CALL GGUBS(DSEED,8784,RAND) RME04010
GO TO 190 RME04020
C USER SHOULD REMOVE THIS STOP AND PLACE CODE THAT WILL USE RME04030
C HIS/HER OWN ROUTINE TO GENERATE 8784 RANDOM NUMBERS AND PLACE RME04040
C THEM IN THE ARRAY RAND. RME04050
170 WRITE (6,2200) RME04060
2200 FORMAT (' NORMALLY EXECUTION WILL CONTINUE USING THE USER'S ', RME04070
1 'RANDOM NUMBER ROUTINE. CURRENTLY THERE IS A STOP CODE AT THAT ' RME04080
2 'POINT!!!') RME04090
CALL WAUDIT
STOP
190 DO 100 I = 1,8784

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100	IRAND(I) = RAND(I) * 10.	RME04120
150	IF (IRNP.EQ.1) RETURN	RME04130
	L = 1	RME04140
	IS = 1	RME04150
200	IL = 120 * L	RME04160
	M = L * 5	RME04170
	IF (IL.GT.8784) GO TO 300	RME04180
	WRITE (6,1100) M,(IRAND(I), I = IS,IL)	RME04190
	IS = IL + 1	RME04200
	L = L + 1	RME04210
	GO TO 200	RME04220
300	M = ((8784 - IS + 1)/24) + (L - 1) * 5	RME04230
	WRITE (6,1100) M,(IRAND(I), I = IS,8784)	RME04240
1100	FORMAT (14,5(1X,2411))	RME04250
	L = IRAND(1) + 1	RME04260
	DO 90 I = 1,8784	RME04270
	N = IRAND(I)	RME04280
C	L IS DIGIT FOR LAST HOUR.	RME04290
C	N IS DIGIT FOR THIS HOUR.	RME04300
	NA = N	RME04310
	IF (NA.EQ.0) NA = 10	RME04320
	KS(NA) = KS(NA) + 1	RME04330
	IF (N.NE.L) GO TO 60	RME04340
C	N = L, THEREFORE HAVE A DOUBLE THIS HOUR.	RME04350
	K2(NA) = K2(NA) + 1	RME04360
C	IF (DLH.EQ.0.) GO TO 50	RME04370
	THEREFORE HAVE A TRIPLE THIS HOUR.	RME04380
	K3(NA) = K3(NA) + 1	RME04390
	IF (TLH.EQ.0.) GO TO 40	RME04400
C	THEREFORE HAVE A QUAD THIS HOUR.	RME04410
	K4(NA) = K4(NA) + 1	RME04420
	IF (QLH.EQ.0.) GO TO 30	RME04430
C	THEREFORE HAVE FIVE-IN-A-ROW THIS HOUR.	RME04440
	K5(NA) = K5(NA) + 1	RME04450
	IF (FLH.EQ.0.) GO TO 20	RME04460
C	THEREFORE HAVE SIX-IN-A-ROW THIS HOUR.	RME04470
	K6(NA) = K6(NA) + 1	RME04480
	IF (SLH.EQ.0.) GO TO 10	RME04490
C	THEREFORE HAVE SEVEN-OR-MORE-IN-A-ROW THIS HOUR.	RME04500
	KG(NA) = KG(NA) + 1	RME04510
10	SLH = 1.	RME04520
20	FLH = 1.	RME04530
30	QLH = 1.	RME04540
40	TLH = 1.	RME04550
50	DLH = 1.	RME04560
	GO TO 70	RME04570
60	DLH = 0.	RME04580
	TLH = 0.	RME04590
	QLH = 0.	RME04600
	FLH = 0.	RME04610
	SLH = 0.	RME04620
70	L = N	RME04630
90	CONTINUE	RME04640
	WRITE (6,1200) (J,J = 1,9)	RME04650
1200	FORMAT ('0DIGIT',10I5,7X,'SUM')	RME04660
	DO 95 J = 1,10	RME04670
	ISUM = ISUM + KS(J)	RME04680
	WRITE (6,1300) KS(10),(KS(J), J = 1,9),ISUM	RME04690
1300	FORMAT ('0SINGLE',10I5,110)	RME04700
	CHISQ = 0.	RME04710
	DO 400 J = 1,10	RME04720
	S = KS(J)	RME04730
	SA = S - 878.4	RME04740
400	CHISQ = CHISQ + SA * SA/878.4	RME04750
	WRITE (6,1400) CHISQ	RME04760
1400	FORMAT ('0CHI SQUARE =',F10.2)	RME04770
	ISUM = 0	RME04780
	DO 450 J = 1,10	RME04790
450	ISUM = ISUM + K2(J)	RME04800
	WRITE (6,1500) K2(10),(K2(J), J = 1,9),ISUM	RME04810

1500	FORMAT ('ODOUBLE',10I5,I10)	RME04820
	CHISQ = 0.	RME04830
	DO 500 J = 1,10	RME04840
	S = K2(J)	RME04850
	SA = S - 87.83	RME04860
500	CHISQ = CHISQ + SA * SA/87.83	RME04870
	WRITE (6,1400) CHISQ	RME04880
	ISUM = 0	RME04890
	DO 550 J = 1,10	RME04900
550	ISUM = ISUM + K3(J)	RME04910
	WRITE (6,1600) K3(10), (K3(J), J = 1,9), ISUM	RME04920
1600	FORMAT ('OTRIPLE',10I5,I10)	RME04930
	CHISQ = 0.	RME04940
	DO 600 J = 1,10	RME04950
	S = K3(J)	RME04960
	SA = S - 8.782	RME04970
600	CHISQ = CHISQ + SA * SA/8.782	RME04980
	WRITE (6,1400) CHISQ	RME04990
	ISUM = 0	RME05000
	DO 650 J = 1,10	RME05010
650	ISUM = ISUM + K4(J)	RME05020
	WRITE (6,1700) K4(10), (K4(J), J = 1,9), ISUM	RME05030
1700	FORMAT ('04 IN ROW',10I5,I10)	RME05040
	CHISQ = 0.	RME05050
	DO 700 J = 1,10	RME05060
	S = K4(J)	RME05070
	SA = S - 0.8781	RME05080
700	CHISQ = CHISQ + SA * SA/0.8781	RME05090
	WRITE (6,1400) CHISQ	RME05100
	ISUM = 0	RME05110
	DO 800 J = 1,10	RME05120
800	ISUM = ISUM + K5(J)	RME05130
	WRITE (6,1800) K5(10), (K5(J), J = 1,9), ISUM	RME05140
1800	FORMAT ('05 IN ROW',10I5,I10)	RME05150
	ISUM = 0	RME05160
	DO 900 J = 1,10	RME05170
900	ISUM = ISUM + K6(J)	RME05180
	WRITE (6,1900) K6(10), (K6(J), J = 1,9), ISUM	RME05190
1900	FORMAT ('06 IN ROW',10I5,I10)	RME05200
	ISUM = 0	RME05210
	DO 950 J = 1,10	RME05220
950	ISUM = ISUM + K6(J)	RME05230
	WRITE (6,2000) K6(10), (K6(J), J = 1,9), ISUM	RME05240
2000	FORMAT ('07 IN ROW',10I5,I10)	RME05250
	WRITE (6,2100)	RME05260
2100	FORMAT ('0 WITH 9 DEGREES OF FREEDOM, THE PROBABILITY',	RME05270
	1' THAT A VALUE OF CHISQ WILL EXCEED:',	RME05280
	2' 23.59 IS 0.005', 21.67 IS 0.01',	RME05290
	3' 19.02 IS 0.025', 16.92 IS 0.05',	RME05300
	4' 14.68 IS 0.10')	RME05310
	RETURN	RME05320
	END	RME05330

C	RAM (VERSION 85364)	RAM00010
C	AN AIR QUALITY DISPERSION MODEL IN	RAM00020
C	SECTION 1. GUIDELINE MODELS	RAM00030
C	IN UNAMAP (VERSION 6) JUL 86	RAM00040
C	SOURCE: UNAMAP FILE ON EPA'S UNIVAC 1110, RTP. NC.	RAM00050
C		RAM00060
C	THIS MAIN PROGRAM IS REFERRED TO AS A IN COMMON STATEMENTS	RAM00070
C		RAM00080
C		RAM00090
C	C-->-->--> OUTLINE OF PROGRAM SECTIONS	RAM00100
C	SECTION A - GENERAL REMARKS	RAM00110
C	SECTION B - DATA INPUT LISTS.	RAM00120
C	SECTION C - INPUT FILE DESCRIPTIONS	RAM00130
C	SECTION D - OUTPUT PUNCHED CARD DESCRIPTION	RAM00140
C	SECTION E - OUTPUT FILE DESCRIPTIONS	RAM00150
C	SECTION F - TEMPORARY FILE DESCRIPTION	RAM00160
C	SECTION G - COMMON, DIMENSION, AND DATA STATEMENTS .	RAM00170
C	SECTION H - FLOW DIAGRAM.	RAM00180
C	SECTION I - RUN SET-UP AND READ FIRST 6 INPUT CARDS.	RAM00190
C	SECTION J - INPUT AND PROCESS EMISSION INFORMATION.	RAM00200
C	SECTION K - EXECUTE FOR INPUT OF SIGNIFICANT SOURCE NUMBERS.	RAM00210
C	SECTION L - CHECK MET. DATA IF FROM FILE OF ONE YEARS'S DATA.	RAM00220
C	SECTION M - GENERATE POLAR COORDINATE RECEPTORS.	RAM00230
C	SECTION N - READ AND PROCESS RECEPTOR INFORMATION.	RAM00240
C	SECTION O - POSITION FILES AS REQUIRED.	RAM00250
C	SECTION P - START LOOPS FOR DAY AND AVERAGING TIME; READ	RAM00260
C	MET. DATA.	RAM00270
C	SECTION Q - CALCULATE AND WRITE MET. SUMMARY INFORMATION.	RAM00280
C	SECTION R - DETERMINE ADDITIONAL RECEPTORS FOR THIS AVG-PER	RAM00290
C	(OPTIONAL)	RAM00300
C	SECTION S - INITIALIZE FOR HOURLY LOOP.	RAM00310
C	SECTION T - BEGIN HOURLY LOOP.	RAM00320
C	SECTION U - CALCULATE AND STORE FOR HIGH-FIVE TABLE.	RAM00330
C	SECTION V - END HOURLY, AVERAGING TIME, AND DAILY LOOPS.	RAM00340
C	SECTION W - WRITE AVERAGE CONC. AND HIGH-FIVE TABLES.	RAM00350
C	SECTION X - CLOSE OUT FILES.	RAM00360
C	SECTION Y - FORMAT STATEMENTS.	RAM00370
C		RAM00380
C	C-->-->--> SECTION A - GENERAL REMARKS.	RAM00390
C		RAM00400
C		RAM00410
C	C*****	RAM00420
C	NOTE: THE CARD INPUT FOR RAM (85364) DIFFERS FROM	RAM00430
C	PREVIOUS VERSIONS.	RAM00440
C	THIS VERSION OF RAM IS COMPILED WITH THE UNIVAC	RAM00450
C	ASCII FORTRAN COMPILER. THIS VERSION OF THE MODEL	RAM00460
C	DIFFERS SLIGHTLY FROM EARLIER VERSIONS IN THE AREAS	RAM00470
C	OF FORMAT STATEMENTS AND CONDITION STATEMENTS.	RAM00480
C	C*****	RAM00490
C	RAM PROGRAM ABSTRACT.	RAM00500
C	RAM IS AN EFFICIENT GAUSSIAN-PLUME MULTIPLE-SOURCE	RAM00510
C	AIR QUALITY ALGORITHM. RAM IS DESCRIBED IN: NOVAK, J.H., AND	RAM00520
C	TURNER, D.B., 1976: AIR POLLUTION CONTROL ASSOC. J., VOL. 26, NO. 6,	RAM00530
C	PAGES 570-575 (JUNE 1976). RAM'S PRINCIPAL USE IS TO DETERMINE	RAM00540
C	SHORT TERM (ONE-HOUR TO ONE-DAY) CONCENTRATIONS FROM POINT AND	RAM00550
C	AREA SOURCES IN URBAN AREAS.	RAM00560
C		RAM00570
C		RAM00580
C	EXECUTION OF RAM IS LIMITED TO A MAXIMUM OF 250 POINT	RAM00590
C	SOURCES, 100 AREA SOURCES, AND 180 RECEPTORS. SIMULATION	RAM00600
C	IS DONE HOUR-BY-HOUR AND HOURLY METEOROLOGICAL DATA	RAM00610
C	ARE REQUIRED AS INPUT. LENGTH OF SIMULATED TIME CAN	RAM00620
C	VARY FROM 1 HOUR TO 1 YEAR.	RAM00630
C		RAM00640
C	RAM AUTHORS:	RAM00650
C	D. BRUCE TURNER* AND JOAN HRENKO NOVAK*	RAM00660
C	METEOROLOGY AND ASSESSMENT DISISION, ESRL	RAM00670
C	ENVIRONMENTAL PROTECTION AGENCY	RAM00680
C		RAM00690
C	* ON ASSIGNMENT FROM NATIONAL OCEANIC AND ATMOSPHERIC ADMIN.,	RAM00700

DEPARTMENT OF COMMERCE.

C***

MODIFIED FOR DEFAULT OPTION BY:

JEROME B. MERSCH
SOURCE RECEPTOR ANALYSIS BRANCH
MONITORING AND DATA ANALYSIS DIVISION
ENVIRONMENTAL PROTECTION AGENCY

RAM SUPPORTED BY:

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MAIL DROP 80, EPA
RESRCH TRI PK, NC 27711

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BACKGROUND--

1. THE ORIGINAL RAM BY JOAN HRENKO NOVAK AND D.BRUCE TURNER WAS MADE AVAILABLE IN FOUR VERSIONS:
RAM SHORT TERM URBAN
RAMR SHORT TERM RURAL
RAMF LONG TERM URBAN
RAMFR LONG TERM RURAL
ON UNAMAP(VERSION 3) IN MARCH 1978.
2. USING THE POINT SOURCE PORTIONS OF RAMR AS A BASIS, THOMAS E. PIERCE AND D.BRUCE TURNER DEVELOPED THE MODEL MPTR. THIS MODEL CONTAINS MANY OPTIONS SO THAT IT IS QUITE VERSATILE PRIMARILY DUE TO ITS MANY USER SELECTED OPTIONS.
3. IN BEGINNING THE TASK OF REVISING RAM FOR GUIDELINE MODEL CONSISTENCY, IT WAS FELT THAT ADDITIONAL OPTIONS COULD BE EMPLOYED, SIMILAR TO MPTR, IN ORDER TO MAKE THE MODEL MORE VERSATILE. THE APPROACH USED HERE WAS TO BEGIN WITH MPTR, REMOVE ITS OPTIONAL TERRAIN FEATURES AND ADD BACK IN THE AREA SOURCE COMPUTATIONS AND RECEPTOR LOCATION FEATURES.

CURRENT MODEL - USERS WILL FIND THAT THERE ARE NO LONGER FOUR VERSIONS OF RAM BUT ONLY ONE. USE OF URBAN OR RURAL DISPERSION PARAMETERS ARE CONTROLLED BY THE INPUT VALUE FOR THE VARIABLE MUOR ("1" FOR URBAN, "2" FOR RURAL). THE LENGTH OF THE MODEL RUN IS DETERMINED BY THE NUMBER OF AVERAGING PERIODS, NPER, TO BE RUN AND THE LENGTH OF THE AVERAGING PERIOD, NAVG. FOR LONG-TERM RUNS (SUCH AS USING A YEAR'S DATA), THE OPTION TO CALCULATE AND PRINT THE HI-FIVE TABLE IS NORMALLY EMPLOYED SO THAT THE HIGHEST AND SECOND HIGHEST CONCENTRATION FOR EACH AVERAGING-TIME CAN BE EASILY DETERMINED.

THIS VERSION OF RAM WAS ASSEMBLED BY CURTIS A. SMITH (JUN -AUG 1980) AND ALFREIDA D. RANKINS (AUG 1980 -PRESENT) UNDER THE GUIDANCE OF D. BRUCE TURNER.

NOTE TO USERS:

ALTHOUGH THE ORIGINAL VERSION OF RAM CONTAINED SUBROUTINES TO LOCATE RECEPTORS DOWNWIND FROM SIGNIFICANT SOURCES FOR EACH AVERAGING PERIOD, THIS OPTION WAS DELETED FROM THE LONG-TERM VERSION (THE VERY SITUATION WHERE IT WOULD HAVE BEEN MOST USEFUL). THIS ACTION WAS TAKEN BECAUSE IT WAS FELT IT WOULD CREATE CONFUSION FOR THE USER TO GENERATE RECEPTORS WITH GIVEN RECEPTOR NUMBERS WHOSE LOCATIONS SHIFT WITH EACH NEW AVERAGING PERIOD.

DETERMINATION OF MAXIMUM CONCENTRATIONS FROM MULTIPLE SOURCES IS A DIFFICUT AND TIME CONSUMING TASK. WITH THIS VERSION OF RAM THE FOLLOWING PROCEDURES CAN BE APPLIED TO ASSIST LOCATING MAXIMUM CONCENTRATIONS THAT CAN BE COMPARED WITH AIR QUALITY STANDARDS:

RAM00710
RAM00720
RAM00730
RAM00740
RAM00750
RAM00760
RAM00770
RAM00780
RAM00790
RAM00800
RAM00810
RAM00820
RAM00830
RAM00840
RAM00850
RAM00860
RAM00870
RAM00880
RAM00890
RAM00900
RAM00910
RAM00920
RAM00930
RAM00940
RAM00950
RAM00960
RAM00970
RAM00980
RAM00990
RAM01000
RAM01010
RAM01020
RAM01030
RAM01040
RAM01050
RAM01060
RAM01070
RAM01080
RAM01090
RAM01100
RAM01110
RAM01120
RAM01130
RAM01140
RAM01150
RAM01160
RAM01170
RAM01180
RAM01190
RAM01200
RAM01210
RAM01220
RAM01230
RAM01240
RAM01250
RAM01260
RAM01270
RAM01280
RAM01290
RAM01300
RAM01310
RAM01320
RAM01330
RAM01340
RAM01350
RAM01360
RAM01370
RAM01380
RAM01390
RAM01400

1. EXECUTE FOR A LONG PERIOD OF RECORD (FOR EXAMPLE, A YEAR) FOR EXISTING MONITOR LOCATIONS AND EMPLOYING THE OPTION TO GENERATE RECEPTORS DOWNWIND OF SIGNIFICANT SOURCES (DIFFERENT RECEPTOR LOCATIONS ARE GENERATED FOR EACH AVERAGING PERIOD). YOU MAY WANT TO ADD SPECIFIED OR GENERATED RECEPTORS TO GET REASONABLE AREA COVERAGE. (MOST OUTPUT WOULD BE SUPPRESSED BY USE OF OPTIONS TO AVOID EXCESS PRINTED OUTPUT.) THE HI-FIVE TABLE WOULD BE NEEDED HOWEVER.

2. USING THE HI -FIVE TABLE SELECT DATES AND TIMES (AND NOTE RECEPTOR NUMBERS) PRODUCING HIGH VALUES (HIGHEST, SECOND HIGHEST, AND POSSIBLY , THIRD HIGHEST).

3. MAKE SHORT-TERM RUNS FOR THE ABOVE IDENTIFIED PERIODS USING THE SAME RECEPTORS, RECEPTOR OPTIONS AND AVERAGING PERIOD AS IN THE INITIAL RUN. BE SURE TO GET PRINTOUT FOR THE AVERAGING PERIOD. THIS ALLOWS DETERMINATION OF THE COORDINATES OF EACH RECEPTOR IDENTIFIED IN STEP 2 ABOVE.

4. MAKE A LONG TERM RUN USING INPUT RECEPTORS ONLY (SO GIVEN SOURCE NUMBER WILL BE AT SAME LOCATION THROUGHOUT RUN). ALL RECEPTORS IDENTIFIED AS PRODUCING HIGH CONCENTRATIONS IN STEPS 2 AND 3 SHOULD BE USED. THIS RUN IS PROBABLY FOR A ONE-YEAR PERIOD AND THE ONLY OUTPUT NEEDED IS THE HIGH-FIVE TABLE FOR DETERMINATION OF ANNUAL CONCENTRATIONS AND HIGHEST AND SECOND HIGHEST CONCENTRATIONS FOR EACH AVERAGING TIME. (THESE WILL BE AVAILABLE FOR EACH RECEPTOR)

ALTHOUGH THIS METHOD WILL STILL BE RELATIVELY EXPENSIVE (ESPECIALLY IF MANY RECEPTORS ARE USED), IT PROVIDES A SYSTEMATIC METHODOLOGY FOR LOOKING FOR MAXIMUM CONCENTRATIONS.

DEFAULT OPTION DESCRIPTION

SELECTION OF THE DEFAULT OPTION CAUSES THE FOLLOWING FEATURES TO BE SET:

 - FINAL PLUME RISE IS USED; GRADUAL (TRANSITIONAL) RISE IS NOT PERMITTED.
 - MOMENTUM PLUME RISE IS ALWAYS ACCOUNTED FOR.
 - BUOYANCY INDUCED DISPERSION IS USED
 - THE POWER LAW WIND PROFILE EXPONENTS HAVE BEEN PRESET TO .15, .15, .20, .25 .30 AND .30 FOR THE URBAN OPTION FOR STABILITY A THROUGH F RESPECTIVELY; MUOR HAS BEEN PRESET TO 1 , URBAN OPTION.
 - STACK TIP DOWNWASH WILL ALWAYS BE CALCULATED WHEN APPROPRIATE. BRIGGS STACK TIP DOWNWASH IS USED.
 - EXPONENTIAL DECAY (HALF-LIFE) IS SET TO 4 HOURS FOR URBAN SO2 APPLICATIONS, OTHER SITUATIONS USE NO DECAY. THIS IS CONSISTENT WITH REGULATORY GUIDANCE.
 - CONCENTRATIONS FOR CALM HOURS ARE SET TO 0.
 - FOR MULTI-HOUR AVERAGING PERIODS THE THE CONCENTRATIONS RESULTING FROM THE CONSIDERATION OF CALM WIND CONDITIONS ARE TREATED AS DESCRIBED IN SECTION U OF THIS PROGRAM.
 - IN ORDER TO FACILITATE THE HANDLING OF CALM WIND CONDITIONS, THE START HOUR AND THE AVERAGING PERIOD HAVE BEEN

C	IOPT(34) - DELETE AREA AVG-PERIOD CONTRIBUTIONS.	RAM03510
C	IOPT(35) - DELETE AVG-PERIOD SUMMARY.	RAM03520
C	IOPT(36) - DELETE AVERAGE CONCENTRATIONS & HI-FIVE TABLE.	RAM03530
C	IOPT(37) - NOT USED THIS VERSION.	RAM03540
C		RAM03550
C	DEFAULT OPTION	RAM03560
C	IOPT(38) - SET DEFAULT OPTION	RAM03570
C		RAM03580
C	OTHER CONTROL AND OUTPUT OPTIONS:	RAM03590
C	IOPT(39) - RUN IS PART OF A SEGMENTED RUN.	RAM03600
C	* * * * * SEE CAUTION BELOW * * * * *	RAM03610
C	IOPT(40) - WRITE PARTIAL CONC. TO DISK OR TAPE.(UNIT 10)	RAM03620
C	* * * * * SEE NOTE BELOW * * * * *	RAM03630
C	IOPT(41) - WRITE HOURLY CONC. TO DISK OR TAPE.(UNIT 12)	RAM03640
C	* * * * * SEE NOTE BELOW * * * * *	RAM03650
C	IOPT(42) - WRITE AVG-PERIOD CONC. TO DISK OR TAPE.(UNIT 13)	RAM03660
C	IOPT(43) - PUNCH AVG-PERIOD CONCENTRATIONS ON CARDS.(UNIT 1)	RAM03670
C	IOPT(44) - NOT USED THIS VERSION.	RAM03680
C	IOPT(45) - NOT USED THIS VERSION.	RAM03690
C	IOPT(46) - NOT USED THIS VERSION.	RAM03700
C	IOPT(47) - NOT USED THIS VERSION.	RAM03710
C	IOPT(48) - NOT USED THIS VERSION.	RAM03720
C	IOPT(49) - NOT USED THIS VERSION.	RAM03730
C	IOPT(50) - NOT USED THIS VERSION.	RAM03740
C		RAM03750
C	* * * * * CAUTION ON USING OPTION 40. * * * * *	RAM03760
C		RAM03770
C	A TREMENDOUS FILE OF MANY RECORDS CAN	RAM03780
C	CAN BE GENERATED BY EMPLOYING OPTION 40.	RAM03790
C	THE USER WILL NEED TO WRITE THE SOFTWARE	RAM03800
C	TO PROCESS THIS FILE ALSO. BE SURE YOU	RAM03810
C	PLAN AHEAD BEFORE USING THIS OPTION.	RAM03820
C	ALTHOUGH THE AUTHORS FEEL IT IS UNLIKELY	RAM03830
C	TO EMPLOY OPTIONS 39 AND 40 ON THE SAME RUN,	RAM03840
C	IT IS POSSIBLE TO DO SO. HOWEVER, NOTE THAT	RAM03850
C	THE SECOND AND SUBSEQUENT SEGMENTS WILL NOT	RAM03860
C	SKIP OVER PREVIOUSLY GENERATED PARTIAL CONC.	RAM03870
C	FILES. THEREFORE UNLESS THE EXECUTIVE CONTROL	RAM03880
C	LANGUAGE HAS BEEN CHANGED SO THAT UNIT 10	RAM03890
C	ACCESSES A DIFFERENT FILE ON EACH SEGMENT,	RAM03900
C	ANY PREVIOUSLY GENERATED PARTIAL CONCENTRATION	RAM03910
C	FILES WILL BE DESTROYED BY WRITING OVER THESE	RAM03920
C	FILES.	RAM03930
C		RAM03940
C		RAM03950
C	* * * * * NOTE ON OUTPUT FILES * * * * *	RAM03960
C		RAM03970
C	THE AUTHORS FEEL THAT THE OUTPUT FILES	RAM03980
C	GENERATED BY OPTIONS 41 AND 42 ARE USEFUL	RAM03990
C	ONLY WHEN THE RECEPTORS ARE SET FOR THE RUN	RAM04000
C	AND NOT VARYING FROM ONE AVG-PER TO ANOTHER.	RAM04010
C	THEREFORE THESE OPTIONS CAN BE USED WITH OPTIONS	RAM04020
C	14 AND 18, BUT A PROGRAM TERMINATION WILL	RAM04030
C	OCCUR IF TRYING TO USE OPTIONS 41 OR 42 IN	RAM04040
C	COMBINATION WITH ANY OF OPTIONS 15, 16, OR 17.	RAM04050
C		RAM04060
C		RAM04070
C	CARD 6. WIND. FORMAT(FREE)	RAM04080
C	(THIS CARD IS REQUIRED)	RAM04090
C		RAM04100
C	HANE - ANEMOMETER HEIGHT (METERS)	RAM04110
C	PL(I), I=1,6 - WIND SPEED POWER LAW PROFILE EXPONENTS FOR EACH	RAM04120
C	STABILITY.	RAM04130
C		RAM04140
C	*****DEFAULT OPTION NOTE*****	RAM04150
C		RAM04160
C	SELECTION OF THE DEFAULT OPTION CAUSES PL	RAM04170
C	TO BE SET TO THE VALUES DESCRIBED ABOVE UNDER	RAM04180
C	DEFAULT OPTION DESCRIPTION. UNDER THIS OPTION,	RAM04190
C	CARD 6 IS STILL REQUIRED TO INPUT HANE.	RAM04200

ALL OTHER DATA ON THE CARD WILL BE IGNORED.

CARD TYPE 7. POINT SOURCE CARD. FORMAT(3A4,8F8.2)

(USED IF OPTION 5 = 1 AND OPTION 7 = 0)
(UP TO 250 POINT SOURCE CARDS ARE ALLOWED.)

PNAME(I,NPT) I=1,3 - 12 CHARACTER POINT SOURCE IDENTIFICATION.
SOURCE(1,NPT) - EAST COORDINATE OF POINT SOURCE (USER UNITS)
SOURCE(2,NPT) - NORTH COORDINATE OF POINT SOURCE (USER UNITS)
SOURCE(3,NPT) - SULFUR DIOXIDE EMISSION RATE (G/SEC).
SOURCE(4,NPT) - PARTICULATE EMISSION RATE (G/SEC).
SOURCE(5,NPT) - PHYSICAL STACK HEIGHT (METERS).
SOURCE(6,NPT) - STACK GAS TEMPERATURE (KELVIN).
SOURCE(7,NPT) - STACK INSIDE DIAMETER (METERS).
SOURCE(8,NPT) - STACK GAS EXIT VELOCITY (M/SEC).

CARD WITH 'ENDP' IN COLS 1-4 IS USED TO SIGNIFY THE
END OF THE POINT SOURCES.

CARD TYPE 8. AREA SOURCE CARD. FORMAT(3A4,6F10.2)

(USED IF OPTION 6 = 1 AND OPTION 7 = 0)
(ONE CARD FOR EACH AREA SOURCE, UP TO
100 AREA SOURCE CARDS ALLOWED.)

ANAME(J,NAS), J=1,3 - 12 CHAR. AREA SOURCE IDENT.
ASORC(1,NAS) - EAST COORD. OF SW CORNER OF AREA SOURCE
(USER UNITS).
ASORC(2,NAS) - NORTH COORD. OF SW CORNER OF AREA SOURCE
(USER UNITS).
ASORC(5,NAS) - SIDE LENGTH OF AREA SOURCE (USER UNITS).
ASORC(3,NAS) - SULFUR DIOXIDE EMISSION RATE FOR ENTIRE
AREA (G/SEC).
ASORC(4,NAS) - PARTICULATE EMISSION RATE FOR ENTIRE
AREA (G/SEC).
ASORC(6,NAS) - AREA SOURCE HEIGHT (METERS).

(NOTE THAT ASORC(5,NAS) - SIDE LENGTH IS READ OUT OF ORDER
TO CONFORM WITH THE EXISTING ORDER OF IPP EMISSIONS DATA.)

CARD WITH 'ENDA' IN COLS 1 -4 IS USED
TO SIGNIFY THE END OF THE AREA SOURCES.

CARD TYPE 9. SPECIFIED SIGNIFICANT PT. SOURCES. FORMAT(26I3)

(USED IF OPTION 11 = 1; NSIGP MUST BE NON-ZERO.)
INPT - NUMBER OF USER SPECIFIED SIGNIFICANT SOURCES.
MPS(I), I=1,NPT - POINT SOURCE NUMBERS USER WANTS CONSIDERED
SIGNIFICANT.

CARD TYPE 10. INFO. ASSOCIATED WITH AREA SOURCES. FORMAT(FREE)
(THIS CARD IS REQUIRED ONLY IF IOPT(6)=1)

FH - FRACTION OF AREA SOURCE HEIGHT WHICH IS PHYSICAL
HEIGHT.
XLIM - DISTANCE LIMIT ON INTEGRATION FOR AREA SOURCE (USER
UNITS). XLIM CANNOT EXCEED 116 KM.
NHTS - INTEGER NUMBER OF HEIGHTS TO BE USED FOR AREA
SOURCES (MIN=1, MAX=3).
HINT - HEIGHT(S) (METERS) FOR AREA SOURCE INTEGRATIONS.
THIS IS AN ARRAY OF FROM ONE TO THREE ELEMENTS.

CARD TYPE 11. BREAKPOINT HEIGHTS. FORMAT(FREE)

(THIS CARD IS REQUIRED ONLY WHEN CARD TYPE 10 IS USED.)

BPH -BREAKPOINT HEIGHTS (METERS) BETWEEN AREA SOURCE HEIGHTS.
THESE VALUES DEFINE THE BOUNDS OF HEIGHTS CLASSES.

RAM04210
RAM04220
RAM04230
RAM04240
RAM04250
RAM04260
RAM04270
RAM04280
RAM04290
RAM04300
RAM04310
RAM04320
RAM04330
RAM04340
RAM04350
RAM04360
RAM04370
RAM04380
RAM04390
RAM04400
RAM04410
RAM04420
RAM04430
RAM04440
RAM04450
RAM04460
RAM04470
RAM04480
RAM04490
RAM04500
RAM04510
RAM04520
RAM04530
RAM04540
RAM04550
RAM04560
RAM04570
RAM04580
RAM04590
RAM04600
RAM04610
RAM04620
RAM04630
RAM04640
RAM04650
RAM04660
RAM04670
RAM04680
RAM04690
RAM04700
RAM04710
RAM04720
RAM04730
RAM04740
RAM04750
RAM04760
RAM04770
RAM04780
RAM04790
RAM04800
RAM04810
RAM04820
RAM04830
RAM04840
RAM04850
RAM04860
RAM04870
RAM04880
RAM04890
RAM04900

BPH IS AN ARRAY OF TWO ELEMENTS. ONE VALUE WILL BE READ RAM04910
 IF NHTS ON PREVIOUS CARD IS 1 OR 2. TWO VALUES READ FOR RAM04920
 NHTS=3. IF NHTS IS 1, THE VALUE OF BPH MUST BE LARGER RAM04930
 THAN ANY AREA HEIGHT IN THE DATA SET FOR THE RUN. RAM04940
 RAM04950

CARD TYPE 12. SPECIFY SIGNIF. AREA SOURCES. FORMAT(26I3)
 (USED IF IOPT(12)=1; NSIGA MUST BE NON-ZERO.)
 INAS - NUMBER OF USER SPECIFIED SIGNIFICANT AREA SOURCES
 (MAX=10). RAM04960
 MAS - AREA SOURCE NUMBERS USER WANTS TO CONSIDER SIGNIF. RAM04970
 RAM04980
 RAM04990

CARD TYPE 13. MET. DATA IDENTIFIERS. FORMAT(FREE)
 (USED IF OPTION 8 = 0)
 ISFCD - SFC MET STATION IDENTIFIER (5 DIGITS) RAM05000
 ISFCYR - YEAR OF SFC MET DATA (2 DIGITS) RAM05010
 IMXD - UPPER-AIR STATION IDENTIFIER (5 DIGITS) RAM05020
 IMXYR - YEAR OF MIXING HEIGHT DATA (2 DIGITS) RAM05030
 RAM05040
 RAM05050
 RAM05060
 RAM05070
 RAM05080
 RAM05090
 RAM05100
 RAM05110
 RAM05120

CARD TYPE 14. POLAR COORDINATE RECEPTORS. FORMAT(FREE)
 (USED IF OPTION 18 = 1)
 RADIL(I), I= 1,5 - ONE TO FIVE RADIAL DISTANCES (REST OF FIVE
 ARE ZEROS) EACH OF WHICH GENERATES 36
 RECEPTORS AROUND POINT CENTX, CENTY ON
 AZIMUTHS 10 TO 360 DEGREES. (USER UNITS) RAM05130
 CENTX - EAST COORDINATE ABOUT WHICH RADIALS ARE CENTERED.
 (USER UNITS) RAM05140
 CENTY - NORTH COORDINATE ABOUT WHICH RADIALS ARE CENTERED.
 (USER UNITS) RAM05150
 RAM05160
 RAM05170
 RAM05180
 RAM05190
 RAM05200
 RAM05210
 RAM05220
 RAM05230
 RAM05240
 RAM05250
 RAM05260
 RAM05270
 RAM05280
 RAM05290
 RAM05300

CARD TYPE 15. RECEPTOR. FORMAT(2A4,2F10.3,F10.0)
 (USED IF OPTION 14 = 1)
 (REMEMBER, 180 IS TOTAL NUMBER OF RECEPTORS ALLOWED IN RAM)
 RNAME(I), I=1,2 - 8 DIGIT ALPHANUMERIC STATION IDENTIFICATION.
 RREC - EAST COORDINATE OF RECEPTOR (USER UNITS) RAM05310
 SREC - NORTH COORDINATE OF RECEPTOR (USER UNITS) RAM05320
 RAM05330
 RAM05340
 RAM05350
 RAM05360
 RAM05370
 RAM05380
 RAM05390
 RAM05400

CARD WITH 'ENDR' IN COLS 1-4 IS USED TO SIGNIFY THE END OF
 THE RECEPTOR CARDS. (NEEDED ONLY IF IOPT(14)=1.)

CARD TYPE 16. HONEYCOMB BOUNDARIES. FORMAT(FREE)
 (USED IF OPTION 17 = 1)
 (HONEYCOMB RECEPTORS WILL ONLY BE GENERATED FOR THE AREA
 DEFINED BY THESE BOUNDS)
 NOTE, IF BOUNDARY VARIABLES ARE INPUT AS ZERO, BOUNDARIES
 WILL BE THE SAME AS THE AREA SOURCE REGION. HOWEVER, IF
 NO AREA SOURCES ARE INPUT AND IF HONEYCOMB RECEPTORS ARE
 TO BE GENERATED, THIS CARD MUST HAVE BOUNDARIES INCLUDED
 TO PROVIDE THE BOUNDS FOR RECEPTOR GENERATION.
 RAM05410
 RAM05420
 RAM05430
 RAM05440
 RAM05450
 RAM05460
 RAM05470
 RAM05480
 RAM05490
 RAM05500
 RAM05510
 RAM05520
 RAM05530
 RAM05540
 RAM05550
 RAM05560
 RAM05570

GRIDSPACE - GRID SPACING (DISTANCE BETWEEN) FOR HONEYCOMB
 RECEPTORS (USER UNITS).
 HRMIN - MINIMUM EAST COORDINATE (USER UNITS).
 HRMAX - MAXIMUM EAST COORDINATE (USER UNITS).
 HSMIN - MINIMUM NORTH COORDINATE (USER UNITS).
 HSMAX - MAXIMUM NORTH COORDINATE (USER UNITS).
 RAM05580
 RAM05590
 RAM05600

CARD TYPE 17. SEGMENTED RUN. FORMAT(FREE)
 (USED IF OPTION 39=1)

C	IDAY	-	NUMBER OF DAYS PREVIOUSLY PROCESSED.	RAM05610
C	LDRUN	-	LAST DAY TO BE PROCESSED IN THIS RUN.	RAM05620
C	CARD TYPE 18.		METEOROLOGY. FORMAT(FREE)	RAM05630
C			(USED IF OPTION 5 = 1)	RAM05640
C			(ONE CARD FOR EACH HOUR OF THE SIMULATION.)	RAM05650
C	JYR	-	YEAR OF MET DATA. (2 DIGITS)	RAM05660
C	DAY1	-	JULIAN DAY OF MET DATA.	RAM05670
C	JHR	-	HOURLY OF MET DATA.	RAM05680
C	IKST	-	STABILITY CLASS FOR THIS HOUR.	RAM05690
C	QU	-	WIND SPEED FOR THIS HOUR (M/SEC).	RAM05700
C	QTEMP	-	AMBIENT AIR TEMPERATURE FOR THIS HOUR (KELVIN).	RAM05710
C	QTHETA	-	WIND DIRECTION FOR THIS HOUR (DEGREES AZIMUTH FROM	RAM05720
C			WHICH THE WIND BLOWS).	RAM05730
C	QHL	-	MIXING HEIGHT FOR THIS HOUR (METERS).	RAM05740
C				RAM05750
C	C-->-->-->		SECTION C - INPUT FILE DESCRIPTIONS.	RAM05760
C			INPUT FILE (UNIT 11) METEOROLOGICAL DATA (USED IF IOPT(8)=0)	RAM05770
C	RECORD 1			RAM05780
C	ID		SFC STATION IDENTIFIER, 5 DIGITS	RAM05790
C	IYEAR		YEAR OF SURFACE DATA, 2 DIGITS	RAM05800
C	IDM		MIX HT STATION IDENTIFIER, 5 DIGITS	RAM05810
C	IYR		YEAR OF MIX HT DATA, 2 DIGITS	RAM05820
C	RECORD TYPE 2 (ONE FOR EACH DAY OF YEAR)			RAM05830
C	JYR		YEAR	RAM05840
C	IMO		MONTH	RAM05850
C	DAY1		JULIAN DAY	RAM05860
C	IKST(24)		STABILITY CLASS	RAM05870
C	QU(24)		WIND SPEED, METERS PER SECOND	RAM05880
C	QTEMP(24)		AMBIENT AIR TEMPERATURE, KELVIN	RAM05890
C	DUMR(24)		FLOW VECTOR TO 10 DEG, DEGREES AZIMUTH	RAM05900
C	QTHETA(24)		RANDOMIZED FLOW VECTOR, DEGREES AZIMUTH	RAM05910
C	HLH(2,24)		MIXING HEIGHT, METERS	RAM05920
C	INPUT FILE(UNIT 15)		POINT SOURCE HOURLY EMISSION DATA	RAM05930
C			(USED IF IOPT(9)=1)	RAM05940
C	RECORD TYPE 1 (ONE FOR EACH HOUR OF SIMULATION)			RAM05950
C	IDATA		DATE-TIME INDICATOR CONSISTING OF YEAR,	RAM05960
C			JULIAN DAY, AND HOUR: YYDDH.	RAM05970
C	SOURCE(IPOL,I),I=1,NPT		EMISSION RATE FOR THE POLLUTANT IPOL	RAM05980
C			FOR EACH SOURCE, GRAMS PER SECOND.	RAM05990
C	INPUT FILE(UNIT 16)		AREA SOURCE HOURLY EMISSION DATA	RAM06000
C			(USED IF IOPT(10) = 1)	RAM06010
C	RECORD TYPE 1 (ONE FOR EACH HOUR OF SIMULATION)			RAM06020
C	IDATA		DATE-TIME INDICATOR CONSISTING OF YEAR,	RAM06030
C			JULIAN DAY, AND HOURS YYDDH.	RAM06040
C	ASORC(IPOL,I),I=1,NAS		EMISSION RATE FOR THE POLLUTANT IPOL	RAM06050
C			FOR EACH SOURCE, GRAMS PER SECOND FOR EACH AREA	RAM06060
C	C-->-->-->		SECTION D - OUTPUT PUNCHED CARD DESCRIPTION	RAM06070
C	OUTPUT PUNCHED CARDS (UNIT 1)		AVERAGE CONCENTRATIONS	RAM06080
C			(PUNCHED IF IOPT(43)=1)	RAM06090
C	CARD TYPE 1 (ONE FOR EACH RECEPTOR FOR EACH AVERAGING TIME)			RAM06100
C	CC:1-4		WORD'CNTRL' PUNCHED	RAM06110
C	CC:5		BLANK	RAM06120
C				RAM06130
C				RAM06140
C				RAM06150
C				RAM06160
C				RAM06170
C				RAM06180
C				RAM06190
C				RAM06200
C				RAM06210
C				RAM06220
C				RAM06230
C				RAM06240
C				RAM06250
C				RAM06260
C				RAM06270
C				RAM06280
C				RAM06290
C				RAM06300

C	CC:6-15	RREC	EAST COORDINATE OF RECEPTOR, USER UNITS	RAM06310
C	CC:16-25	SREC	NORTH COORDINATE OF RECEPTOR, USER UNITS	RAM06320
C	CC:26-35	GWU	CONCENTRATION FOR AVERAGING TIME, MICROG/M**3	RAM06330
C	CC:36-45	ACHI(K)	CONC. FROM AREAS, MICROG/M**3	RAM06340
C	CC:46-55	PCHI(K)	CONC. FROM POINTS, MICROG/M**3	RAM06350
C	CC:56-60	K	RECEPTOR NUMBER	RAM06360
C	CC:61-65	IDATE(1)	YEAR	RAM06370
C	CC:66-70	IDATE(2)	JULIAN DAY	RAM06380
C	CC:71-75	NE	ENDING HOUR FOR AVG-PER.	RAM06390
C	CC:76-80	NAVG	NUMBER OF HOURS IN AVG-PER.	RAM06400
C				RAM06410
C	->->->-> SECTION E - OUTPUT FILE DESCRIPTIONS			RAM06420
C	OUTPUT FILE (UNIT 10) PARTIAL CONCENTRATIONS (USED IF IOPT(40)=1)			RAM06430
C	RECORD TYPE 1			RAM06440
C	NPER	NUMBER OF PERIODS		RAM06450
C	NAVG	NUMBER OF HOURS IN AVERAGING PERIOD.		RAM06460
C	LINE1(14)	80 ALPHANUMERIC CHARACTERS FOR TITLE.		RAM06470
C	LINE2(14)	80 ALPHANUMERIC CHARACTERS FOR TITLE.		RAM06480
C	LINE3(14)	80 ALPHANUMERIC CHARACTERS FOR TITLE.		RAM06490
C	RECORD TYPE 2 (FROM RAM) (ONE FOR EACH AVERAGING PERIOD)			RAM06500
C	NRECEP	NUMBER OF RECEPTORS		RAM06510
C	NPT	NUMBER OF POINT SOURCES		RAM06520
C	NAS	NUMBER OF AREA SOURCES		RAM06530
C	RREC(I), I=1, NRECEP	EAST COORDINATE OF RECEPTOR, USER UNITS		RAM06540
C	SREC(I), I=1, NRECEP	NORTH COORDINATE OF RECEPTOR, USER UNITS		RAM06550
C	FOR EACH SIMULATION HOUR, NRECEP RECORDS OF TYPE 3			RAM06560
C	ARE GENERATED FOLLOWED BY NRECEP RECORDS OF TYPE 4.			RAM06570
C	RECORD TYPE 3 (ONE FOR EACH RECEPTOR FOR EACH SIMULATED HOUR, FROM PT)			RAM06580
C	IDATE	YEAR AND JULIAN DAY		RAM06590
C	LH	HOUR		RAM06600
C	K	RECEPTOR NUMBER		RAM06610
C	PARTC(J), J=1, NPT	CONCENTRATION AT RECEPTOR K FROM POINT SOURCE J, G/M**3.		RAM06620
C	RECORD TYPE 4 (ONE FOR EACH RECEPTOR FOR EACH SIMULATED HOUR, FROM JMHARE)			RAM06630
C	IDATE	YEAR AND JULIAN DAY		RAM06640
C	LH	HOUR		RAM06650
C	KREC	RECEPTOR NUMBER		RAM06660
C	PARTC(J), J=1, NAS	CONCENTRATION AT RECEPTOR KREC FROM AREA SOURCE J, G/M**3		RAM06670
C	OUTPUT FILE (UNIT 12) HOURLY CONCENTRATIONS (USED IF IOPT(41)=1)			RAM06680
C	RECORD 1			RAM06690
C	NPER	NUMBER OF PERIODS		RAM06700
C	NAVG	NUMBER OF HOURS IN AVERAGING PERIOD.		RAM06710
C	LINE1(14)	80 ALPHANUMERIC CHARACTERS FOR TITLE.		RAM06720
C	LINE2(14)	80 ALPHANUMERIC CHARACTERS FOR TITLE.		RAM06730
C	LINE3(14)	80 ALPHANUMERIC CHARACTERS FOR TITLE.		RAM06740
C	RECORD 2			RAM06750
C	NRECEP	NUMBER OF RECEPTORS.		RAM06760
C	RREC(I), I=1, NRECEP	EAST COORDINATE OF RECEPTOR, USER UNITS		RAM06770
C	SREC(I), I=1, NRECEP	NORTH COORDINATE OF RECEPTOR, USER UNITS		RAM06780
C	RECORD TYPE 3 (ONE FOR EACH SIMULATED HOUR)			RAM06790
C				RAM06800
C				RAM06810
C				RAM06820
C				RAM06830
C				RAM06840
C				RAM06850
C				RAM06860
C				RAM06870
C				RAM06880
C				RAM06890
C				RAM06900
C				RAM06910
C				RAM06920
C				RAM06930
C				RAM06940
C				RAM06950
C				RAM06960
C				RAM06970
C				RAM06980
C				RAM06990
C				RAM07000

C	IDATE(2)	JULIAN DAY	RAM07010
C	LH	HOURLY	RAM07020
C	PHCHI(I), I=1, NRECEP	HOURLY CONCENTRATION FOR EACH RECEPTOR,	RAM07030
C		G/M**3.	RAM07040
C	OUTPUT FILE (UNIT 13)	AVERAGING-PERIOD CONCENTRATIONS (USED IF	RAM07050
C		IOPT(42)=1)	RAM07060
C	RECORD 1		RAM07070
C			RAM07080
C	NPER	NUMBER OF PERIODS	RAM07090
C	NAVG	NUMBER OF HOURS IN AVERAGING PERIOD.	RAM07100
C	LINE1(14)	80 ALPHANUMERIC CHARACTERS FOR TITLE.	RAM07110
C	LINE2(14)	80 ALPHANUMERIC CHARACTERS FOR TITLE.	RAM07120
C	LINE3(14)	80 ALPHANUMERIC CHARACTERS FOR TITLE.	RAM07130
C			RAM07140
C			RAM07150
C	RECORD 2		RAM07160
C			RAM07170
C	NRECEP	NUMBER OF RECEPTORS.	RAM07180
C	RREC(I), I=1, NRECEP	EAST COORDINATE OF RECEPTOR, USER UNITS	RAM07190
C	SREC(I), I=1, NRECEP	NORTH COORDINATE OF RECEPTOR, USER UNITS	RAM07200
C	RECORD TYPE 3 (ONE FOR EACH SIMULATED AVERAGING PERIOD)		RAM07210
C			RAM07220
C	IDATE(2)	JULIAN DAY	RAM07230
C	NE	ENDING HOUR OF PERIOD	RAM07240
C	PCHI(K), K=1, NRECEP	AVERAGING PERIOD CONCENTRATION FOR EACH	RAM07250
C		RECEPTOR, G/M**3.	RAM07260
C	C-->-->--> SECTION F - TEMPORARY FILE DESCRIPTIONS		RAM07270
C			RAM07280
C	TEMPORARY FILE (UNIT 9) EMISSION DATA		RAM07290
C	(ALWAYS WRITTEN; READ IF IOPT (7)= 1)		RAM07300
C	RECORD 1		RAM07310
C			RAM07320
C	NPT	NUMBER OF POINT SOURCES	RAM07330
C	NAS	NUMBER OF AREA SOURCES	RAM07340
C	RECORD 2		RAM07350
C			RAM07360
C	IMPS(I), I=1, 25	NUMBER OF POINT SOURCE SIGNIF.	RAM07370
C	SOURCE(I, J),	POINT SOURCE INFO.	RAM07380
C	I=1, 9		RAM07390
C	J=1, NPT		RAM07400
C	RECORD 3		RAM07410
C			RAM07420
C	IMAS(I), I=1, 10	ORDER OF AREA SOURCE SIGNIF.	RAM07430
C	RMIN	WEST BOUNDARY OF AREA SOURCES	RAM07440
C	RMAX	EAST BOUNDARY OF AREA SOURCES	RAM07450
C	SMIN	SOUTH BOUNDARY OF AREA SOURCES	RAM07460
C	SMAX	NORTH BOUNDARY OF AREA SOURCES	RAM07470
C	IRSIZE	FIRST DIMENSION OF IA ARRAY	RAM07480
C	ISSIZE	SECOND DIMENSION OF IA ARRAY	RAM07490
C	ASORC(I, J)	AREA SOURCE INFO.	RAM07500
C	I=1, 6		RAM07510
C	J=1, NAS		RAM07520
C	IA(I, J)	AREA SOURCE MAP ARRAY.	RAM07530
C	I=1, IRSIZE		RAM07540
C	J=1, ISSIZE		RAM07550
C	TEMPORARY FILE (UNIT 14) VALUES FOR HIGH-FIVE TABLES (USED IF		RAM07560
C		IOPT(39)=1)	RAM07570
C	ONLY RECORD		RAM07580
C			RAM07590
C	IDAY(ON WRITE)	NUMBER OF DAYS PROCESSED	RAM07600
C	IDAYS(ON READ)	NUMBER OF DAYS PREVIOUSLY PROCESSED	RAM07610
C	SUM(180)	CUMULATION OF LONG-TERM CONCENTRATION, (G/M**3)	RAM07620
C			RAM07630
C			RAM07640
C			RAM07650
C			RAM07660
C			RAM07670
C			RAM07680
C			RAM07690
C			RAM07700

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C      NHR      NUMBER OF HOURS PROCESSED      RAM07710
C      DAY1A    JULIAN D/Y OF START OF LENGTH OF RECORD.      RAM07720
C      HRL      START HOJR OF LENGTH OF RECORD      RAM07730
C      HMAXA(3,5,180,5) HIGHEST FIVE CONCENTRATIONS (G/M**3), AND      RAM07740
C      ASSOCIATED DAY AND HOUR, FOR EACH RECEPTOR,      RAM07750
C      FOR FI/E DIFFERENT AVERAGING TIMES.      RAM07760
C      RAM07770
C->->-> SECTION G - COMMON, DIMENSION, AND DATA STATEMENTS.      RAM07780
C      RAM07790
COMMON /AB/ DELM,DELN      RAM07800
COMMON /AMOST/ DELH,FH,HINT(3),H,HL,IO,IOPT(50),KST,MUOR,NHTS,RC,RRAM07810
1CZ,SY,SZ,TEMP,TLOS,UPL,X,Y,Z      RAM07820
COMMON /AE/ HCL(10),PXUCOR(6,9),PXUEXR(6,9),PXCOR(6,9),PXEXR(6,9),      RAM07830
1PXUCOF(6,9),PXUEXP(6,9),PXJOF(6,9),PXEXP(6,9),AXCOR(6,9),AXEXR(6,9)RAM07840
2),AXCOF(6,9),AXEXP(6,9)      RAM07850
COMMON /AEFM/ ITYPE(180),CODE(180),UNITS,RREU(180),SREU(180)      RAM07860
COMMON /AEFGKM/ NRECEP,RRIC(180),SRIC(180),IDATE(2),LH,NPT      RAM07870
COMMON /AEG/ SOURCE(9,250)      RAM07880
COMMON /AEGIKM/ IPOL,CON'WO,SINT,COST,U,HANE,PL(6)      RAM07890
COMMON /AEK/ ASORC(6,100)      RAM07900
COMMON /AEM/ NSIGP,MPS(25),NSIGA,MAS(10)      RAM07910
COMMON /AF/ GRIDSP,HRMIN,HRMAX,HSMIN,HSMAX      RAM07920
COMMON /AGK/ PARTC(250)      RAM07930
COMMON /AGM/ PSAV(250),HSAV(250),DH(250),DSAV(250),UPH(250),HPR(25)RAM07940
10),FP(250),PCHI(180),PHCHI(180),PSIGS(180,26),PHSIGS(180,26),IPSIGRAM07950
2S(250),GRANDT(180)      RAM07960
COMMON /AIL/ CIN(3,200),XLIM      RAM07970
COMMON /AIM/ HARE(3)      RAM07980
COMMON /AK/ BPH(2),RMIN,SMIN,RMAX,SMAX,NAS,IRSIZE,ISSIZE,IA(25,25)RAM07990
1,IWD,IASIGS(100),NBP      RAM08000
COMMON /AKL/ IH,NS,KREC      RAM08010
COMMON /AKM/ BPHM(2),ACHI(180),AHCHI(180),ASIGS(180,11),AHSIGS(180)RAM08020
1,11)      RAM08030
COMMON /AM/ LINE1(20),LINE2(20),LINE3(20),IPOLU,QTHETA(24),QU(24),      RAM08040
1QHL(24),QTEMP(24),IKST(24),NAVG,NB,RNAME(2,180)      RAM08050
COMMON /AN/ HMAXA(5,180,5),NDAY(5,180,5),IHR(5,180,5),CONC(180,5),      RAM08060
1JDAY      RAM08070
C      DIMENSION MODEL(2,2),DEG(3)      RAM08080
C      DIMENSION PNAME(3,250),ANAME(3,100),IFREQ(7),DUMR(24),HLH(2,24)RAM08100
1),IMPS(25),TITLE(2),TABLE(4,21),RADIL(5)      RAM08110
C      DIMENSION IDUMR(24)      RAM08120
C      DIMENSION SUM(180),NTIME(5),ATIME(5),IPOLT(2),DNAME(36)      RAM08130
C      DIMENSION STAR(2,180),SIGNIF(250),IMAS(10)      RAM08140
C      DIMENSION PLL(6,2),CF(5)      RAM08150
C      EQUIVALENCE (PNAME(1,1),RNAME(1,1),ANAME(1,1))      RAM08160
C      EQUIVALENCE (UPH(1),SIGNIF(1))      RAM08170
C      EQUIVALENCE (DH(1),TABLE(1,1))      RAM08180
C      DATA IN /5/,IO /6/      RAM08190
C      DATA DEG /90.,180.,270./      RAM08200
C      DATA IFREQ /7*0/,BLNK /' ',BNK4 /' ' / ,IRIN /'I' / ,IRPC /'C'RAM08210
1/      RAM08220
C      DATA TITLE /'SO2 ','PART' / ,IRSIZE,ISSIZE /1,1/      RAM08230
C      DATA IRDIM /25/,ISDIM /25/      RAM08240
C      DATA MODEL /'URBA','N','RURA','L' /      RAM08250
C      DATA IPOLT /'SO2 ','PART' /      RAM08260
C      DATA RMIN /99999 / ,SMIN /99999 /      RAM08270
C      DATA ENDP /'ENDP' / ,ENDA /'ENDA' / ,ENDR /'ENDR' /      RAM08280
C      DATA MAXP /250/,MAXA /100/,STR /'*' / ,STAR /360*' /      RAM08290
C      MAXP EQUALS SECOND DIMENSION OF THE ARRAY NAMED: SOURCE.      RAM08300
C      MAXA EQUAL SECOND DIMENSION OF THE ARRAY NAMED: ASORC.      RAM08310
C      DATA DNAME /10,20,30,40,50,60,70,80,      RAM08320
1,90,100,110,120,130,140,150,160,170,180,      RAM08330
2180,190,200,210,220,230,240,250,260,270,      RAM08340
3,280,290,300,310,320,330,340,350,360, /      RAM08350
4      RAM08360
C      DATA NTIME /1,3,8,24,0 / ,ATIME /1.,3.,8.,24.,0. /      RAM08370
C      RAM08380
C      RAM08390
C      RAM08400

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DATA ITMIN1 /9999/ IDIV8 /0/ IDIV24 /0/ ICALM /0/
DATA C/'C'/, ICFL3/0/, ICFL8/0/, ICFL24/0/, CF/5*'/, /

DEFAULT POWER LAW EXPONENTS.

DATA PLL/.15,.15,.20,.25,.30,.30,.07,.07,.10,.15,.35,.55/

SECTION H - FLOW DIAGRAM

RELATION OF SUBROUTINES IN RAM

RAM

* BLOCK DATA

* READ DATA FROM CARDS

* INITIALIZE SGZ

* INITIALIZE SYSZ

* INITIALIZE JMHREC

* READ EMISSION DATA FROM
CARDS OR DISK

* READ RECEPTOR DATA

- LOOP FOR CALENDAR DAYS

- LOOP FOR AVERAGING TIME

* READ MET DATA

* ANGARC

* GREC (ENTRY TO JMHREC)

* JMHON

- LOOP ON HOURS

- (READ HOURLY EMISSIONS)

* * * * * PT

- LOOP ON RECEPTORS

- LOOP ON SOURCES

* * RCON

** SYZ(ENTRY TO SYSZ)

* * * * * JMH54

* * JMHCZ

* * SIGZ(ENTRY TO SGZ)

* * * * * JMHARE

- LOOP ON RECEPTORS

* * JMHPOL

RAM08410
RAM08420
RAM08430
RAM08440
RAM08450
RAM08460
RAM08470
RAM08480
RAM08490
RAM08500
RAM08510
RAM08520
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RAM08570
RAM08580
RAM08590
RAM08600
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RAM08670
RAM08680
RAM08690
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RAM08960
RAM08970
RAM08980
RAM08990
RAM09000
RAM09010
RAM09020
RAM09030
RAM09040
RAM09050
RAM09060
RAM09070
RAM09080
RAM09090
RAM09100

C	WRITE ERROR STATEMENT	RAM09790
	WRITE (IO,1860) NSIGP	RAM09800
	CALL WAUDIT	
	STOP	RAM09810
50	IF (NSIGA.LE.10) GO TO 60	RAM09820
C	WRITE ERROR STATEMENT	RAM09830
	WRITE (IO,1870) NSIGA	RAM09840
	CALL WAUDIT	
	STOP	RAM09850
60	IP=IPOL-2	RAM09860
	CONTWO=CONONE*UNITS	RAM09870
C		RAM09880
C	READ CARD TYPE 5 (SEE DESCRIPTION, SECTION B).	RAM09890
C		RAM09900
	READ (IN,1800) (IOPT(I),I=1,50)	RAM09910
C		RAM09920
	IF(IOPT(38).NE.1) GO TO 55	RAM09930
C		RAM09940
C	DEFAULT SELECTION RESULTS IN THE FOLLOWING: USE STACK DOWNWASH	RAM09950
C	(1); USE FINAL PLUME RISE (2); USE BUOYANCY-INDUCED DISPERSION	RAM09960
C	(3); WRITE HIGH-5 TABLES (36) BUT DELETE ALL OTHER OUTPUT (23,	RAM09970
C	24, 25, 26, 27, 28, 29, 30, 31, 32, 33, 34, AND 35).	RAM09980
C		RAM09990
C	EMISSIONS FROM PREVIOUS RUN ARE NOT ALLOWED.	RAM10000
C	MET DATA ON CARDS ARE NOT ALLOWED.	RAM10010
C	SPECIFICATION OF SIGNIFICANT POINT AND AREA	RAM10020
C	SOURCES IS NOT ALLOWED.	RAM10030
C		RAM10040
	IOPT(1)=0	RAM10050
	IOPT(2)=1	RAM10060
	IOPT(3)=1	RAM10070
	IOPT(7)=0	RAM10080
	IOPT(8)=0	RAM10090
	IOPT(11)=0	RAM10100
	IOPT(12)=0	RAM10110
	IOPT(15)=0	RAM10120
	IOPT(16)=0	RAM10130
	IOPT(23)=1	RAM10140
	IOPT(24)=1	RAM10150
	IOPT(25)=1	RAM10160
	IOPT(26)=1	RAM10170
	IOPT(27)=1	RAM10180
	IOPT(28)=1	RAM10190
	IOPT(29)=1	RAM10200
	IOPT(30)=1	RAM10210
	IOPT(31)=1	RAM10220
	IOPT(32)=1	RAM10230
	IOPT(33)=1	RAM10240
	IOPT(34)=1	RAM10250
	IOPT(35)=1	RAM10260
	IOPT(36)=0	RAM10270
	IOPT(39)=0	RAM10280
	IOPT(40)=0	RAM10290
	IOPT(41)=0	RAM10300
	IOPT(42)=0	RAM10310
	IOPT(43)=0	RAM10320
C		RAM10330
C	SET HALF-LIFE FOR DEFAULT OPTION	RAM10340
C		RAM10350
	IF(IPOL.EQ.3)HAFL=14400.	RAM10360
	IF(IPOL.NE.3)HAFL=0.	RAM10370
C		RAM10380
C		RAM10390
C	SET POWER LAW WIND PROFILE EXPONENTS;	RAM10400
C	SET START HOUR, AND AVERAGING PERIOD ;	RAM10410
C	SET THE NUMBER OF SIGNIFICANT POINT AND	RAM10420
C	AREA SOURCES.	RAM10430
C		RAM10440
	MUOR=1	RAM10450
	IHSTR=1	RAM10460

	NAVG=24	RAM10470
	NSIGP=0	RAM10480
	NSIGA=0	RAM10490
55	CONTINUE	RAM10500
C		RAM10510
C		RAM10520
C		RAM10530
C		RAM10540
C		RAM10550
C		RAM10560
C		RAM10570
	WRITE GENERAL INPUT INFORMATION	
	WRITE (IO,2120) (MODEL(K,MUOR),K=1,2),TITLE(IP),NPER,NAVG,IHSTRT,IR	RAM10580
	IDATE(2),IDATE(1),UNITS,CONONE,CONTWO,Z	RAM10590
	DAYIA=IDATE(2)	RAM10600
	HR1=IHSTRT	RAM10610
	IF (HAFL.GT.0.0) GO TO 70	RAM10620
	TLOS=0.	RAM10630
	WRITE (IO,2130)	RAM10640
	GO TO 80	RAM10650
70	WRITE (IO,2140) HAFL	RAM10660
	TLOS=693./HAFL	RAM10670
C	IF HI-5 TABLE,IOPT(36),SEE IF FIFTH AVG-TIME NECESSARY.	RAM10680
80	IF (IOPT(36).EQ.1) GO TO 90	RAM10690
	NAVT=5	RAM10700
C		RAM10710
C	FOR DEFAULT OPTION	RAM10720
C	ADDITIONAL AVERAGING PERIOD SET TO ZERO.	RAM10730
	IF (IOPT(38).EQ.1) NAV5=0	RAM10740
C		RAM10750
	IF (NAV5.EQ.1.OR.NAV5.EQ.3.OR.NAV5.EQ.8.OR.NAV5.EQ.24.OR.NAV5.EQ.0	RAM10760
1)	NAVT=4	RAM10770
	NTIME(5)=NAV5	RAM10780
	ATIME(5)=NAV5	RAM10790
	WRITE (IO,2150) NAVT	RAM10800
	IF (NAVT.EQ.5) WRITE (IO,2160) NAV5	RAM10810
C	IF NO SIGNIF. SOURCES TO BE CONSIDERED,ELIMINATE CONTRIB OUTPUT	RAM10820
90	IF (NSIGP.GT.0) GO TO 100	RAM10830
	IOPT(25)=1	RAM10840
	IOPT(33)=1	RAM10850
100	IF (NSIGA.GT.0) GO TO 110	RAM10860
	IOPT(28)=1	RAM10870
	IOPT(34)=1	RAM10880
110	WRITE (IO,2170) (I,IOPT(I),I=1,4)	RAM10890
	WRITE (IO,2180) (I,IOPT(I),I=5,13)	RAM10900
	WRITE (IO,2190) (I,IOPT(I),I=14,19)	RAM10910
	WRITE (IO,2200) (I,IOPT(I),I=20,31)	RAM10920
	WRITE (IO,2210) (I,IOPT(I),I=32,38)	RAM10930
	WRITE (IO,2220) (I,IOPT(I),I=39,50)	RAM10940
	ASSIGN 230 TO KTRL	RAM10950
	MIX=2	RAM10960
	IF (MUOR.EQ.1) GO TO 120	RAM10970
	ASSIGN 240 TO KTRL	RAM10980
	MIX=1	RAM10990
C	EXECUTE ASSIGN STATEMENTS FOR URBAN-RURAL SELECTIONS IN	RAM11000
C	SUBROUTINES.	RAM11010
120	CALL SGZ	RAM11020
	CALL SYSZ	RAM11030
	CALL JMHREC	RAM11040
C		RAM11050
C		RAM11060
C	READ CARD TYPE 6 (SEE DESCRIPTION, SECTION B).	RAM11070
C		RAM11080
C	SWITCH TO SELECT DEFAULT POWER LAW EXPONENTS,	RAM11090
C	TERRAIN ADJUSTMENT FACTORS.	RAM11100
C		RAM11110
	IF (IOPT(38).NE.0) READ (IN,*) HANE	RAM11120
	IF (IOPT(38).EQ.0) READ (IN,*) HANE,PL	RAM11130
	IF (IOPT(38).EQ.0) GO TO 105	RAM11140
	DO 104 I1=1,6	RAM11150
	PL(I1)=PL(I1,MUOR)	RAM11160

104	CONTINUE	RAM11170
105	CONTINUE	RAM11180
C		RAM11190
C	MUCH OF THE FOLLOWING PROGRAM SECTION IS BASED UPON	RAM11200
C	RAMQ IN THE PREV. RAM. THIS SECTION IS RESPONSIBLE	RAM11210
C	FOR MAKING THE NECESSARY DATA CONVERSIONS ON THE RAW	RAM11220
C	EMISSIONS DATA IN ORDER TO ESTABLISH A STANDARD	RAM11230
C	DATA BANK WHICH WILL BE ACCEPTABLE. A CONVERSION FACTOR	RAM11240
C	FROM USER UNITS TO KILOMETERS IS APPLIED WHEN NECESSARY.	RAM11250
C		RAM11260
C->->->->	SECTION J - INPUT AND PROCESS EMISSION INFORMATION.	RAM11270
C		RAM11280
C	IF NOT READING EMISSIONS FROM PREVIOUS RUN, SKIP	RAM11290
C		RAM11300
C	IF (IOPT(7).EQ.0) GO TO 140	RAM11310
C	READ (9) NPT,NAS	RAM11320
C		RAM11330
C	IF NOT USING POINT SOURCES, SKIP	RAM11340
C	IF (NPT.EQ.0) GO TO 130	RAM11350
C	READ RECORD OF POINT SOURCE INFORMATION	RAM11360
C	READ (9) (IMPS(I),I=1,25),((SOURCE(I,J),I=1,9),J=1,NPT)	RAM11370
C		RAM11380
C	IF NOT USING AREA SOURCES, SKIP	RAM11390
130	IF (NAS.EQ.0) GO TO 630	RAM11400
C	READ RECORD OF AREA SOURCE INFORMATION	RAM11410
C	READ (9) (IMAS(I),I=1,10),RMIN,RMAX,SMIN,SMAX,IRSIZE,ISSIZE,((ASORRAM11420	
C	1C(I,J),I=1,6),J=1,NAS),((IA(I,J),I=1,IRSIZE),J=1,ISSIZE)	RAM11430
C	GO TO 630	RAM11440
C		RAM11450
C	ARE THERE POINT SOURCES? IF NOT, SKIP TO AREA SECTION.	RAM11460
140	IF (IOPT(5).EQ.0) GO TO 310	RAM11470
C		RAM11480
C	IF (IOPT(20).EQ.1) GO TO 150	RAM11490
C	WRITE HEADING FOR POINT SOURCE INFO.	RAM11500
C	WRITE (10,2240)	RAM11510
150	NPT=0	RAM11520
C		RAM11530
C	BEGIN LOOP TO READ THE POINT SOURCE INFORMATION	RAM11540
160	NPT=NPT+1	RAM11550
C	IF (NPT.LE.MAXP) GO TO 170	RAM11560
C	READ (IN,1810) DUM	RAM11570
C	IF (DUM.EQ.ENDP) GO TO 270	RAM11580
C	WRITE ERROR STATEMENT	RAM11590
C	WRITE (10,1880) MAXP	RAM11600
C	CALL WAUDIT	
C	STOP	RAM11610
C		RAM11620
C	READ CARD TYPE 7 (SEE DESCRIPTION, SECTION B).	RAM11630
C		RAM11640
170	READ (IN,1820) (PNAME(I,NPT),I=1,3),(SOURCE(I,NPT),I=1,8)	RAM11650
C	CARD WITH 'ENDP' IN COL 1-4 IS USED TO SIGNIFY END OF	RAM11660
C	POINT SOURCES.	RAM11670
C	IF (PNAME(1,NPT).EQ.ENDP) GO TO 270	RAM11680
C	CALCULATE BUOYANCY FACTOR	RAM11690
C	D=SOURCE(7,NPT)	RAM11700
C	FOLLOWING VARIABLE IS BRIGGS' F WITHOUT TEMPERATURE FACTOR.	RAM11710
C	SOURCE(9,NPT)=2.45153*SOURCE(8,NPT)*D*D	RAM11720
C	2.45153 IS GRAVITY OVER FOUR.	RAM11730
C	TS=SOURCE(6,NPT)	RAM11740
C	IF (TS.GT.293.) GO TO 180	RAM11750
C	HF=SOURCE(5,NPT)	RAM11760
C	GO TO 200	RAM11770
180	F=SOURCE(9,NPT)*(TS-293.)/TS	RAM11780
C	IF (F.GE.55.) GO TO 190	RAM11790
C	ONLY BUOYANCY PLUME RISE IS CONSIDERED HERE.	RAM11800
C	HF=SOURCE(5,NPT)+21.425*F**0.75/3.	RAM11810
C	GO TO 200	RAM11820
190	HF=SOURCE(5,NPT)+38.71*F**0.6/3.	RAM11830
C	HSAV, DSAV, AND PSAV ARE USED FOR TEMPORARY STORAGE	RAM11840
200	HSAV(NPT)=HF	RAM11850

C	DETERMINE HEIGHT INDEX.	RAM11860
	DO 210 IH=2,9	RAM11870
	IF (HF.LT.(HCL(IH)-.01)) GO TO 220	RAM11880
210	CONTINUE	RAM11890
	IH=10	RAM11900
220	IS=IH-1	RAM11910
	GO TO KTRL, (230,240)	RAM11920
230	A=PXUCOF(2,IS)	RAM11930
	B=PXUEXP(2,IS)	RAM11940
	GO TO 250	RAM11950
240	A=PXUCOR(2,IS)	RAM11960
	B=PXUEXR(2,IS)	RAM11970
250	DSAV(NPT)=(A*HF**B)*SOURCE(IPOL,NPT)/3.	RAM11980
C	AN ESTIMATE OF THE POTENTIAL IMPACT OF EACH SOURCE IS	RAM11990
C	DETERMINED AND STORED IN DSAV. MAX CONCENTRATION IS	RAM12000
C	DETERMINED BY $CHI(MAX) = (A*H**B)*Q/U$ WHERE	RAM12010
C	A IS THE COEFFICIENT AND B IS THE EXPONENT, OF	RAM12020
C	MAXIMUM $CHI*U/Q$ VALUES PREDETERMINED FOR B STABILITY	RAM12030
C	AND A SPECIFIC EFFECTIVE HEIGHT RANGE. PLUME RISE	RAM12040
C	IS CALCULATED FOR B STABILITY AND 3 M/SEC WIND SPEED.	RAM12050
C		RAM12060
	IPSIGS(NPT)=0	RAM12070
	IF (IOPT(20).EQ.1) GO TO 260	RAM12080
C	LIST POINT SOURCE INFORMATION.	RAM12090
	WRITE (IO,2250) NPT,(PNAME(J,NPT),J=1,3),(SOURCE(K,NPT),K=1,8),DSAV(NPT)	RAM12100
	IV(NPT),HSAV(NPT),F	RAM12110
C	SOURCE COORDINATES ARE TRANSFORMED INTO INTERNAL UNITS.	RAM12120
260	SOURCE(1,NPT)=SOURCE(1,NPT)/UNITS	RAM12130
	SOURCE(2,NPT)=SOURCE(2,NPT)/UNITS	RAM12140
C		RAM12150
C	GO BACK AND READ DATA FOR ANOTHER POINT SOURCE.	RAM12160
	GO TO 160	RAM12170
C		RAM12180
270	NPT=NPT-1	RAM12190
C		RAM12200
C		RAM12210
C		RAM12220
	RANK 25 HIGHEST POINT SOURCES.	RAM12230
	NLIM=25	RAM12240
	IF (NPT.LT.25) NLIM=NPT	RAM12250
	DO 290 I=1,NLIM	RAM12260
	SIGMAX=-1.0	RAM12270
	DO 280 J=1,NPT	RAM12280
	IF (DSAV(J).LE.SIGMAX) GO TO 280	RAM12290
	SIGMAX=DSAV(J)	RAM12300
	LMAX=J	RAM12310
280	CONTINUE	RAM12320
C	IMPS IS THE SOURCE NUMBER IN ORDER OF SIGNIFICANCE.	RAM12330
	IMPS(I)=LMAX	RAM12340
C	PSAV IS THE CALC. CONC. IN ORDER OF SIGNIFICANCE.	RAM12350
	PSAV(I)=SIGMAX	RAM12360
290	DSAV(LMAX)=-1.0	RAM12370
C	OUTPUT TABLE OF RANKED SOURCES.	RAM12380
	WRITE (IO,2260) TITLE(IP)	RAM12390
	DO 300 I=1,NLIM	RAM12400
	WRITE (IO,2270) I,PSAV(I),IMPS(I)	RAM12410
300	CONTINUE	RAM12420
C	IF NOT EXPECTING AREA SOURCES, SKIP.	RAM12430
310	IF (IOPT(6).EQ.0) GO TO 550	RAM12440
	NAS=0	RAM12450
	IF (IOPT(21).EQ.1) GO TO 320	RAM12460
	WRITE (IO,2280)	RAM12470
C	BEGIN LOOP TO READ AREA SOURCES	RAM12480
320	NAS=NAS+1	RAM12490
	IF (NAS.LE.MAXA) GO TO 330	RAM12500
	READ (IN,1810) DUM	RAM12510
	IF (DUM.EQ.ENDA) GO TO 390	RAM12520
C	WRITE ERROR STATEMENT	RAM12530
	WRITE (IO,1890) MAXA	
	CALL WAUDIT	
	STOP	RAM12540

C		RAM12550
C	READ CARD TYPE 8 (SEE DESCRIPTION, SECTION B)	RAM12560
C		RAM12570
330	READ (IN,1830) (ANAME(J,NAS),J=1,3),ASORC(1,NAS),ASORC(2,NAS),ASORC(3,NAS),ASORC(4,NAS),ASORC(5,NAS),ASORC(6,NAS)	RAM12580
	IF (ANAME(1,NAS).EQ.ENDA) GO TO 390	RAM12590
	IF (IOPT(22).EQ.1) GO TO 370	RAM12600
C	STORE AREA EMISSIONS ACCORDING TO HEIGHT CLASS	RAM12610
	DO 340 I=1,20	RAM12620
	HC=I*5.	RAM12630
	IF (ASORC(6,NAS).LE.HC) GO TO 350	RAM12640
340	CONTINUE	RAM12650
	GO TO 360	RAM12660
C	ADD EMISSION RATE INTO TABLE AND TOTAL.	RAM12670
350	TABLE(3,I)=TABLE(3,I)+ASORC(IPOL,NAS)	RAM12680
360	TABLE(3,21)=TABLE(3,21)+ASORC(IPOL,NAS)	RAM12690
C	CALCULATE SIDE LENGTH IN INTERNAL UNITS	RAM12700
370	WA=ASORC(5,NAS)/UNITS	RAM12710
C	CONVERTS SIDE LENGTH IN INTERNAL UNITS TO METERS AND ADJUST	RAM12720
C	EMISSION RATE	RAM12730
	SF=WA*1000.*CONTWO	RAM12740
C	DETERMINE EMISSION RATE IN G/SEC-M**2.	RAM12750
	ASORC(3,NAS)=ASORC(3,NAS)/(SF*SF)	RAM12760
	ASORC(4,NAS)=ASORC(4,NAS)/(SF*SF)	RAM12770
C	FOR AREA SOURCES, SIGNIFICANCE IS DETERMINED BY SELECTING A	RAM12780
C	SPECIFIED NUMBER OF AREA SOURCES (N < OR = 10) WHICH HAVE	RAM12790
C	THE HIGHEST EMISSION RATE TIMES THE SIDE LENGTH OF THE AREA	RAM12800
C	SOURCE.	RAM12810
	SIGNIF(NAS)=SF*ASORC(IPOL,NAS)	RAM12820
	IF (IOPT(21).EQ.1) GO TO 380	RAM12830
	WRITE (IO,2290) NAS,(ANAME(J,NAS),J=1,3),(ASORC(K,NAS),K=1,6),SIGNIF(NAS)	RAM12840
	1IF(NAS)	RAM12850
C	CO-ORDINATES ARE TRANSLATED TO INTERNAL UNITS.	RAM12860
380	ASORC(1,NAS)=ASORC(1,NAS)/UNITS	RAM12870
	ASORC(2,NAS)=ASORC(2,NAS)/UNITS	RAM12880
	ASORC(5,NAS)=WA	RAM12890
C	READJUST AREA SOURCE REGION BOUNDARIES AS REQUIRED	RAM12900
C	(INTERNAL UNITS).	RAM12910
	RC=ASORC(1,NAS)	RAM12920
	SC=ASORC(2,NAS)	RAM12930
	IF (RC.LT.RMIN) RMIN=RC	RAM12940
	IF (SC.LT.SMIN) SMIN=SC	RAM12950
C	RC,SC, AND WA IN INTERNAL UNITS.	RAM12960
	A=RC+WA	RAM12970
	B=SC+WA	RAM12980
	IF (A.GT.RMAX) RMAX=A	RAM12990
	IF (B.GT.SMAX) SMAX=B	RAM13000
C	GO BACK AND READ DATA FOR ANOTHER AREA SOURCE.	RAM13010
	GO TO 320	RAM13020
C		RAM13030
390	NAS=NAS-1	RAM13040
C		RAM13050
C	DETERMINE SIZE OF AREA ARRAY	RAM13060
	A=RMAX-RMIN+.0005	RAM13070
	IRSIZE=A	RAM13080
	IF (A-FLOAT(IRSIZE).GT.0.001) GO TO 410	RAM13090
	B=SMAX-SMIN+.0005	RAM13100
	ISSIZE=B	RAM13110
	IF (B-FLOAT(ISSIZE).GT.0.001) GO TO 420	RAM13120
C	CHECK SIZE OF AREA SOURCE REGION WITH DIMENSIONS OF IA ARRAY.	RAM13130
	IF (IRSIZE.GT.IRDIM) GO TO 400	RAM13140
	IF (ISSIZE.LE.ISDIM) GO TO 430	RAM13150
C	WRITE ERROR STATEMENT	RAM13160
400	WRITE (IO,1900) IRSIZE,ISSIZE	RAM13170
	CALL WAUDIT	RAM13180
	STOP	
C	WRITE ERROR STATEMENT	RAM13190
410	WRITE (IO,1910)	RAM13200
	CALL WAUDIT	RAM13210
	STOP	RAM13220

C	WRITE ERROR STATEMENT	RAM13230
420	WRITE (IO,1920)	RAM13240
	CALL WAUDIT	
	STOP	
C	ZERO IA ARRAY(AREA SOURCE MAP ARRAY)	RAM13250
430	DO 440 I=1,IRSIZE	RAM13260
	DO 440 J=1,ISSIZE	RAM13270
440	IA(I,J)=0	RAM13280
C	LOOP THROUGH ALL AREA SOURCES AND STORE SOURCE NO'S IN IA.	RAM13290
C	THERE CAN BE NO OVERLAPPING OF AREA SOURCES. LOCATIONS ARE	RAM13300
C	DEFINED BY THE INTERNAL GRID SYSTEM.	RAM13310
	A=RMIN-1.	RAM13320
	B=SMIN-1.	RAM13330
	DO 460 NS=1,NAS	RAM13340
	IR=ASORC(1,NS)-A+.0005	RAM13350
	IS=ASORC(2,NS)-B+.0005	RAM13360
	IWA=ASORC(5,NS)+.0005-1.	RAM13370
	IQ=IS+IWA	RAM13380
	ID=IR+IWA	RAM13390
	DO 450 I=IR,ID	RAM13400
	DO 450 J=IS,IQ	RAM13410
C	CHECK TO SEE IF IA ALREADY HAS A SOURCE IN THE I,J TH POSITION	RAM13420
C	IF (IA(I,J).EQ.0) GO TO 450	RAM13430
	WRITE ERROR STATEMENT	RAM13440
	WRITE (IO,1930) IA(I,J),I,J,NS	RAM13450
	CALL WAUDIT	RAM13460
	STOP	
C	STORE SOURCE NO. IN APPROPRIATE POSITION	RAM13470
450	IA(I,J)=NS	RAM13480
460	CONTINUE	RAM13490
C	PRINT OUT AREA SOURCE MAP ARRAY(IA) IF NOT TOO LARGE TO FIT	RAM13500
C	ACROSS PAGE.	RAM13510
	IF (IRSIZE.GT.41) GO TO 480	RAM13520
	WRITE (IO,2300)	RAM13530
	ID=ISSIZE+1	RAM13540
	DO 470 IQ=1,ISSIZE	RAM13550
	J=ID-IQ	RAM13560
470	WRITE (IO,2310) J,(IA(I,J),I=1,IRSIZE)	RAM13570
	WRITE (IO,2320) (I,I=1,IRSIZE)	RAM13580
	GO TO 490	RAM13590
C	WRITE EXPLANATORY STATEMENT	RAM13600
480	WRITE (IO,1940)	RAM13610
C	PRINT OUT ORIGIN CO-ORDINATES AND BOUNDARIES IN INTERNAL UNITS	RAM13620
490	WRITE (IO,2330) A,B,IRSIZE,ISSIZE	RAM13630
	WRITE (IO,2340) RMIN,RMAX,SMIN,SMAX	RAM13640
C		RAM13650
C	RANK HIGHEST 10 AREA SOURCES	RAM13660
	NLIM=10	RAM13670
	IF (NAS.LT.10) NLIM=NAS	RAM13680
	DO 510 I=1,NLIM	RAM13690
	SIGMAX=-1.0	RAM13700
	DO 500 J=1,NAS	RAM13710
	IF (SIGNIF(J).LE.SIGMAX) GO TO 500	RAM13720
	SIGMAX=SIGNIF(J)	RAM13730
	IMAX=J	RAM13740
500	CONTINUE	RAM13750
	IMAS(I)=IMAX	RAM13760
	HPR(I)=SIGMAX	RAM13770
510	SIGNIF(IMAX)=-1.0	RAM13780
	IF (NSIGA.EQ.0) GO TO 530	RAM13790
	WRITE (IO,2350) TITLE(IP)	RAM13800
	DO 520 I=1,NLIM	RAM13810
	WRITE (IO,2360) I,HPR(I),IMAS(I)	RAM13820
520	CONTINUE	RAM13830
530	DO 540 I=1,NAS	RAM13840
	ASORC(5,I)=ASORC(5,I)*0.5	RAM13850
540	IASIGS(I)=0	RAM13860
550	IF (IOPT(22).EQ.1) GO TO 610	RAM13870
C		RAM13880
C	EMISSIONS WITH HEIGHT TABLE.	RAM13890
		RAM13900

C	DO 590 I=1,NPT	RAM13910
	DO 560 J=1,20	RAM13920
	HC=J*5.	RAM13930
	IF (SOURCE(5,I).LE.HC) GO TO 570	RAM13940
560	CONTINUE	RAM13950
C	POINT SOURCES WITH PHYSICAL HEIGHTS GT 100 METERS ARE LISTED	RAM13960
C	SEPARATELY.	RAM13970
	WRITE (IO,2370) I,SOURCE(5,I),SOURCE(IPOL,I)	RAM13980
	GO TO 580	RAM13990
C	ADD EMISSION RATE INTO TABLE AND TOTAL.	RAM14000
570	TABLE(1,J)=TABLE(1,J)+SOURCE(IPOL,I)	RAM14010
580	TABLE(1,21)=TABLE(1,21)+SOURCE(IPOL,I)	RAM14020
590	CONTINUE	RAM14030
C	OUTPUT SOURCE-STRENGTH-HEIGHT TABLE	RAM14040
C	THIS TABLE DISPLAYS THE TOTAL EMISSIONS FOR BOTH POINT AND	RAM14050
C	AREA SOURCES AND THE CUMULATIVE FREQUENCY ACCORDING TO	RAM14060
C	HEIGHT CLASS. REQUIRED INPUT TO RAM, SUCH AS HEIGHT CLASS	RAM14070
C	BOUNDARIES FOR AREA SOURCES AND REPRESENTATIVE HEIGHTS FOR	RAM14080
C	EACH HEIGHT CLASS, CAN BE DETERMINED FROM THESE TABLES.	RAM14090
	WRITE (IO,2380) TITLE(IP)	RAM14100
C	HEIGHT CLASS EMISSIONS ARE IN 1 AND 3.	RAM14110
C	DETERMINE CUMULATIVE PERCENT IN 2 AND 4.	RAM14120
	IF (TABLE(1,21).EQ.0.0) TABLE(1,21)=1.0	RAM14130
	IF (TABLE(3,21).EQ.0.0) TABLE(3,21)=1.0	RAM14140
	ID=0	RAM14150
	IQ=5	RAM14160
	TABLE(2,1)=TABLE(1,1)/TABLE(1,21)	RAM14170
	TABLE(4,1)=TABLE(3,1)/TABLE(3,21)	RAM14180
	WRITE (IO,2390) ID,IQ,(TABLE(J,1),J=1,4)	RAM14190
	DO 600 I=2,20	RAM14200
	IQ=I*5	RAM14210
	ID=IQ-4	RAM14220
	TABLE(2,I)=TABLE(1,I)/TABLE(1,21)+TABLE(2,I-1)	RAM14230
	TABLE(4,I)=TABLE(3,I)/TABLE(3,21)+TABLE(4,I-1)	RAM14240
	WRITE (IO,2390) ID,IQ,(TABLE(J,I),J=1,4)	RAM14250
600	CONTINUE	RAM14260
	IF (NSIGP.EQ.0) TABLE(1,21)=0.0	RAM14270
	IF (NSIGA.EQ.0) TABLE(3,21)=0.0	RAM14280
	WRITE (IO,2400) TABLE(1,21),TABLE(3,21)	RAM14290
C	WRITE FIRST EMISSION RECORD	RAM14300
610	WRITE (9) NPT,NAS	RAM14310
	IF (NPT.EQ.0) GO TO 620	RAM14320
C		RAM14330
C		RAM14340
C	WRITE RECORD OF POINT SOURCE INFORMATION	RAM14350
	WRITE (9) (IMPS(I),I=1,25),((SOURCE(I,J),I=1,9),J=1,NPT)	RAM14360
620	IF (NAS.EQ.0) GO TO 630	RAM14370
C	WRITE RECORD OF AREA SOURCE INFORMATION	RAM14380
	WRITE (9) (IMAS(I),I=1,10),RMIN,RMAX,SMIN,SMAX,IRSIZE,ISSIZE,((ASORAM14400	
	IRC(I,J),I=1,6),J=1,NAS),((IA(I,J),I=1,IRSIZE),J=1,ISSIZE)	RAM14410
C		RAM14420
C-->-->-->SECTION K - EXECUTE FOR INPUT OF SIGNIFICANT SOURCE NUMBERS.		RAM14430
C		RAM14440
630	WRITE (IO,2410) NPT,NSIGP	RAM14450
	IF (NSIGP.EQ.0) GO TO 700	RAM14460
	IF (NSIGP.GT.NPT) NSIGP=NPT	RAM14470
	IF (NSIGA.GT.NAS) NSIGA=NAS	RAM14480
	IF (IOPT(11).EQ.0) GO TO 660	RAM14490
C		RAM14500
C	READ CARD TYPE 9 (SEE DESCRIPTION, SECTION B).	RAM14510
C		RAM14520
	READ (IN,1840) INPT,(MPS(I),I=1,INPT)	RAM14530
	WRITE (IO,2420) INPT,(MPS(I),I=1,INPT)	RAM14540
	IF (INPT.LE.NSIGP) GO TO 640	RAM14550
C	WRITE ERROR STATEMENT	RAM14560
	WRITE (IO,1950) INPT,NSIGP	RAM14570
	CALL WAUDIT	
	STOP	
640	IF (INPT.EQ.0) GO TO 660	RAM14580
		RAM14590

C	IF LAST SPECIFIED SOURCE NUMBER IS ZERO WRITE WARNING STATEMENT	RAM14600
	IF (MPS(INPT).EQ.0) WRITE (IO,1960)	RAM14610
	J=INPT+1	RAM14620
	K=1	RAM14630
C	ADD SIGNIFICANT PT. SOURCES DETERMINED FROM RANKED SOURCE LIST	RAM14640
C	IF NSIGP GREATER THAN INPT.	RAM14650
	IF (J.GT.NSIGP) GO TO 680	RAM14660
	DO 650 I=J,NSIGP	RAM14670
	MPS(I)=IMPS(K)	RAM14680
650	K=K+1	RAM14690
	GO TO 680	RAM14700
660	DO 670 I=1,NSIGP	RAM14710
670	MPS(I)=IMPS(I)	RAM14720
680	WRITE (IO,2430) (MPS(I),I=1,NSIGP)	RAM14730
C	FILL IN SIGNIFICANT POINT SOURCE ARRAY	RAM14740
	DO 690 I=1,NSIGP	RAM14750
	J=MPS(I)	RAM14760
690	IPSIGS(J)=I	RAM14770
700	IF (IOPT(9).EQ.0) GO TO 720	RAM14780
C	SAVE AVERAGE EMISSION RATE	RAM14790
	DO 710 I=1,NPT	RAM14800
710	PSAV(I)=SOURCE(IPOL,I)	RAM14810
C		RAM14820
C	IOPT(6) CONTROL OPTION, AREA SOURCE INPUT? 0=NO, 1=YES.	RAM14830
C	IF NO AREA SOURCES, SKIP	RAM14840
720	IF (IOPT(6).EQ.0) GO TO 800	RAM14850
	WRITE (IO,2440) NAS,NSIGA	RAM14860
C		RAM14870
C	READ CARD TYPE 10	RAM1488C
C		RAM14890
	READ (IN,*) FH,XLIM,NHTS,(HINT(I),I=1,NHTS)	RAM14900
	NBP=NHTS-1	RAM14910
	WRITE (IO,2450) NHTS,(HINT(I),I=1,NHTS)	RAM14920
	IF (NBP.LE.0) NBP=1	RAM14930
C		RAM14940
C	READ CARD TYPE 11.	RAM14950
C		RAM14960
	READ (IN,*) (BPH(I),I=1,NBP)	RAM14970
	WRITE (IO,2460) (BPH(I),I=1,NBP)	RAM14980
C	CONVERT TO USER UNITS FOR PRINT OUT. XLIM IS CONVERTED TO KM.	RAM14990
	C1=RMIN*UNITS	RAM15000
	C2=RMAX*UNITS	RAM15010
	C3=SMIN*UNITS	RAM15020
	C4=SMAX*UNITS	RAM15030
	C5=XLIM	RAM15040
	XLIM=XLIM*CONONE	RAM15050
	WRITE (IO,2470) FH,C5,C1,C2,C3,C4,IRSIZE,ISSIZE	RAM15060
	IF (XLIM.LT.116.) GO TO 730	RAM15070
C	WRITE ERROR STATEMENT	RAM15080
	WRITE (IO,1970) XLIM	RAM15090
	CALL WAUDIT	
	STOP	RAM15100
730	IF (NSIGA.EQ.0) GO TO 810	RAM15110
C	IF NOT SPECIFYING SIGNIF. AREA SOURCES, SKIP	RAM15120
	IF (IOPT(12).EQ.0) GO TO 760	RAM15130
C		RAM15140
C	READ THE NUMBER OF SIGNIFICANT AREA SOURCES THAT USER	RAM15150
C	WANTS TO SPECIFY AND THE NUMBER DESIGNATIONS OF THOSE SOURCES	RAM15160
C	ON CARD TYPE 12.	RAM15170
C		RAM15180
	READ (IN,1840) INAS,(MAS(I),I=1,INAS)	RAM15190
	WRITE (IO,2480) INAS,(MAS(I),I=1,INAS)	RAM15200
	IF (INAS.LE.NSIGA) GO TO 740	RAM15210
C	WRITE ERROR STATEMENT	RAM15220
	WRITE (IO,1950) INAS,NSIGA	RAM15230
	CALL WAUDIT	
	STOP	RAM15240
740	IF (INAS.EQ.0) GO TO 760	RAM15250
C	IF LAST SPECIFIED SOURCE NUMBER IS ZERO WRITE WARNING STATEMENT	RAM15260
	IF (MAS(INAS).EQ.0) WRITE (IO,1980)	RAM15270

	J=INAS+1	RAM15280
	K=1	RAM15290
C	ADD SIGNIFICANT AREA SOURCES DETERMINED FROM RANKED SOURCE	RAM15300
C	LIST IF NSIGA GREATER THAN INAS.	RAM15310
	IF (J.GT.NSIGA) GO TO 780	RAM15320
	DO 750 I=J,NSIGA	RAM15330
	MAS(I)=IMAS(K)	RAM15340
750	K=K+1	RAM15350
	GO TO 780	RAM15360
C	TRANSFER SIGNIFICANT SOURCES DETERMINED FROM SIGNIFICANT SOURCE	RAM15370
C	LIST IF INAS EQUAL ZERO.	RAM15380
760	DO 770 I=1,NSIGA	RAM15390
770	MAS(I)=IMAS(I)	RAM15400
780	WRITE (IO,2490) (MAS(I),I=1,NSIGA)	RAM15410
C		RAM15420
C	FILL IN SIGNIFICANT AREA SOURCE MARKER ARRAY	RAM15430
	DO 790 I=1,NSIGA	RAM15440
	J=MAS(I)	RAM15450
790	IASIGS(J)=I	RAM15460
800	CONTINUE	RAM15470
C		RAM15480
C-->-->-->	SECTION L - CHECK MET DATA IF FROM FILE OF ONE YEAR'S DATA.	RAM15490
C		RAM15500
810	IF (IOPT(8).EQ.1) GO TO 840	RAM15510
C		RAM15520
C	READ CARD TYPE 13 (SEE DESCRIPTION, SECTION B).	RAM15530
C		RAM15540
	READ (IN,*) ISFCD,ISFCYR,IMXD,IMXYR	RAM15550
C	READ ID RECORD FROM PREPROCESSED MET DISK OR TAPE FILE.	RAM15560
	READ (11) ID,IYEAR,IDM,IYM	RAM15570
	IF (ISFCD.EQ.ID.AND.ISFCYR.EQ.IYEAR) GO TO 820	RAM15580
C	WRITE ERROR STATEMENT	RAM15590
	WRITE (IO,1990) ISFCD,ISFCYR,ID,IYEAR,IMXD,IMXYR,IDM,IYM	RAM15600
	CALL WAUDIT	
	STOP	RAM15610
820	IF (IMXD.EQ.IDM.AND.IMXYR.EQ.IYM) GO TO 830	RAM15620
C	WRITE ERROR STATEMENT	RAM15630
	WRITE (IO,1990) ISFCD,ISFCYR,ID,IYEAR,IMXD,IMXYR,IDM,IYM	RAM15640
	CALL WAUDIT	
	STOP	RAM15650
830	WRITE (IO,2500) ISFCD,ISFCYR,IMXD,IMXYR	RAM15660
C		RAM15670
C-->-->-->	SECTION M - GENERATE POLAR COORDINATE RECEPTORS.	RAM15680
C		RAM15690
840	NRECEP=0	RAM15700
	WRITE (IO,2510)	RAM15710
	DO 850 I=1,180	RAM15720
	DO 850 J=1,2	RAM15730
850	RNAME(J,I)=BNK4	RAM15740
	IF (IOPT(18).NE.1) GO TO 890	RAM15750
C		RAM15760
C	READ CARD TYPE 14 (SEE DESCRIPTION, SECTION B).	RAM15770
C		RAM15780
	READ (IN,*) RADIL,CENTX,CENTY	RAM15790
	JA=0	RAM15800
	DO 860 J=1,5	RAM15810
	IF (RADIL(J).EQ.0) GO TO 860	RAM15820
	JA=JA+1	RAM15830
860	CONTINUE	RAM15840
	WRITE (IO,2520) CENTX,CENTY,RADIL	RAM15850
	DO 880 I=1,36	RAM15860
C	CALCULATE THE ANGLE IN RADIANS	RAM15870
	A=FLOAT(I)*0.1745329	RAM15880
C	0.1745329 IS 2*PI/36	RAM15890
	SINT=SIN(A)	RAM15900
	COST=COS(A)	RAM15910
	DO 870 J=1,JA	RAM15920
	NRECEP=I+36*(J-1)	RAM15930
	RREU(NRECEP)=(RADIL(J)*SINT)+CENTX	RAM15940
C	CALCULATE THE EAST-COORDINATE	RAM15950

C	SREU(NRECEP)=(RADIL(J)*COST)+CENTY	RAM15960
	CALCULATE THE NORTH-COORDINATE	RAM15970
	ITYPE(NRECEP)=IRPC	RAM15980
	RNAME(1,NRECEP)=DNAME(I)	RAM15990
C	ALPHANUMERIC INFORMATION WHICH INDICATES DEGREES AZIMUTH	RAM16000
	ENCODE (4,2530,RNAME(2,NRECEP)) RADIL(J)	RAM16010
C	ENCODE THE FLOATING POINT VARIABLE OF RADIAL DISTANCE	RAM16020
C	TO ALPHANUMERIC REPRESENTATION SO INFO CAN BE PRINTED	RAM16030
870	CONTINUE	RAM16040
880	CONTINUE	RAM16050
	NRECEP=36*JA	RAM16060
C		RAM16070
C-->-->-->	SECTION N - READ AND PROCESS RECEPTOR INFORMATION.	RAM16080
C		RAM16090
C	NOW READ CARD TYPE 15 IF NECESSARY. MUST HAVE A CARD WITH	RAM16100
C	'ENDR' IN COLS 1-4 TO INDICATE END OF RECEPTOR CARDS.	RAM16110
C	NO MORE THAN 180 RECEPTORS CAN BE INPUT TO MPTER.	RAM16120
C		RAM16130
890	IF (IOPT(14).EQ.0) GO TO 940	RAM16140
C	START LOOP TO ENTER RECEPTORS.	RAM16150
	NRECEP=NRECEP+1	RAM16160
	IF (NRECEP.LE.180) GO TO 910	RAM16170
	READ (IN,1810,END=900) DUM	RAM16180
	IF (DUM.EQ.ENDR) GO TO 930	RAM16190
C	WRITE ERROR STATEMENT	RAM16200
900	WRITE (IO,2000)	RAM16210
	CALL WAUDIT	
	STOP	RAM16220
C		RAM16230
C	READ CARD TYPE 15 (SEE DESCRIPTION, SECTION B).	RAM16240
C		RAM16250
910	READ (IN,1850) (RNAME(J,NRECEP),J=1,2),RREU(NRECEP),SREU(NRECEP)	RAM16260
C	PLACE 'ENDR' IN COLS 1 TO 4 ON CARD FOLLOWING LAST RECEPTOR	RAM16270
C	TO END READING TYPE 15 CARDS.	RAM16280
	ITYPE(NRECEP)=IRIN	RAM16290
	IF (RNAME(1,NRECEP).EQ.ENDR) GO TO 920	RAM16300
	GO TO 890	RAM16310
920	RNAME(1,NRECEP)=BNK4	RAM16320
930	NRECEP=NRECEP-1	RAM16330
	IF (NRECEP.GT.0) GO TO 940	RAM16340
C	WRITE ERROR STATEMENT	RAM16350
	WRITE (IO,2010) NRECEP	RAM16360
	CALL WAUDIT	
	STOP	RAM16370
940	IF (NRECEP.EQ.0) GO TO 960	RAM16380
C	PRINT OUT TABLE OF RECEPTORS. (IN USER UNITS)	RAM16390
	WRITE (IO,2540)	RAM16400
	DO 950 K=1,NRECEP	RAM16410
	WRITE (IO,2550) K,ITYPE(K),(RNAME(J,K),J=1,2),RREU(K),SREU(K)	RAM16420
	RREC(K)=RREU(K)/UNITS	RAM16430
	SREC(K)=SREU(K)/UNITS	RAM16440
950	ICODE(K)=0	RAM16450
960	NPREC=NRECEP	RAM16460
	IF (IOPT(17).EQ.0) GO TO 990	RAM16470
C		RAM16480
C	READ CARD TYPE 16	RAM16490
C		RAM16500
	READ (IN,*) GRDSPU,HRMNU,HRMXU,HSMNU,HSMXU	RAM16510
	IF (HRMXU.EQ.0.0) GO TO 970	RAM16520
C	IF USER DOESN'T SPECIFY BOUNDARIES FOR HONEYCOMB SOURCES	RAM16530
C	USE AREA SOURCE BOUNDARIES.	RAM16540
C	CONVERT INPUT GRID BOUNDARIES(USER UNITS) TO INTERNAL UNITS	RAM16550
	HRMIN=HRMNU/UNITS	RAM16560
	HRMAX=HRMXU/UNITS	RAM16570
	HSMIN=HSMNU/UNITS	RAM16580
	HSMAX=HSMXU/UNITS	RAM16590
	GO TO 980	RAM16600
C	RMIN,RMAX,SMIN,SMAX ARE IN INTERNAL UNITS	RAM16610
970	HRMIN=HRMIN	RAM16620
	HRMAX=HRMAX	RAM16630

	HSMIN=SMIN	RAM16640
	HSMAX=SMA	RAM16650
C	CONVERT GRIDSP FROM USER UNITS TO INTERNAL UNITS.	RAM16660
980	GRIDSP=GRDSPU/UNITS	RAM16670
C		RAM16680
C->->->->	SECTION O - POSITION FILES AS REQUIRED.	RAM16690
C		RAM16700
990	IF (IOPT(39).EQ.0) GO TO 1000	RAM16710
C		RAM16720
C	READ CARD TYPE 17 (SEE DESCRIPTION, SECTION B).	RAM16730
C		RAM16740
	READ (IN,*) IDAY,LDRUN	RAM16750
	WRITE (IO,2560) IDAY,LDRUN	RAM16760
	IF (IDAY.EQ.0) GO TO 1000	RAM16770
C	READ INFO FOR HIGH-FIVE TABLE FROM LAST SEGMENT.	RAM16780
	READ (14) IDAYS,SUM,NHR,DAY1A,HR1,HMAXA,NDAY,IHR	RAM16790
	REWIND 14	RAM16800
	IF (IDAY.EQ.IDAYS) GO TO 1000	RAM16810
C	WRITE ERROR STATEMENT	RAM16820
	WRITE (IO,2020) IDAY,IDAYS	RAM16830
	CALL WAUDIT	
	STOP	RAM16840
1000	NP=IDAY*(24/NAVG)	RAM16850
C	IF OPTION 40 = 1, WRITE INITIAL INFO TO UNIT 10(PART. CONC.)	RAM16860
	IF (IOPT(40).EQ.1) WRITE (10) NPER,NAVG,LINE1,LINE2,LINE3	RAM16870
	IF (IOPT(41).EQ.0) GO TO 1040	RAM16880
	IF (IOPT(15).EQ.0.AND.IOPT(16).EQ.0.AND.IOPT(17).EQ.0) GO TO 1010	RAM16890
C	WRITE TERMINATION OF RUN STATEMENT	RAM16900
C	(WRONG COMBINATION OF OPTIONS).	RAM16910
	WRITE (IO,2030)	RAM16920
	CALL WAUDIT	
	STOP	RAM16930
1010	IF (IDAY.LE.0) GO TO 1030	RAM16940
C	SKIP PREVIOUSLY GENERATED HOURLY RECORDS.	RAM16950
	ISKIP=IDAY*24+2	RAM16960
	DO 1020 I=1,ISKIP	RAM16970
1020	READ (12)	RAM16980
	GO TO 1040	RAM16990
C	WRITE LEAD TWO RECORDS ON HOURLY FILE.	RAM17000
1030	WRITE (12) NPER,NAVG,LINE1,LINE2,LINE3	RAM17010
	WRITE (12) NRECEP,(RREU(I),I=1,NRECEP),(SREU(I),I=1,NRECEP)	RAM17020
1040	IF (IOPT(42).EQ.0) GO TO 1080	RAM17030
	IF (IOPT(15).EQ.0.AND.IOPT(16).EQ.0.AND.IOPT(17).EQ.0) GO TO 1050	RAM17040
C	WRITE TERMINATION OF RUN STATEMENT	RAM17050
C	(WRONG COMBINATION OF OPTIONS).	RAM17060
	WRITE (IO,2030)	RAM17070
	CALL WAUDIT	
	STOP	RAM17080
1050	IF (IDAY.LE.0) GO TO 1070	RAM17090
C	SKIP PREVIOUSLY GENERATED AVERAGING-PERIOD FILE.	RAM17100
	ISKIP=NP+2	RAM17110
	DO 1060 I=1,ISKIP	RAM17120
1060	READ (13)	RAM17130
	GO TO 1080	RAM17140
C	WRITE LEAD TWO RECORDS ON AVERAGING PERIOD FILE.	RAM17150
1070	WRITE (13) NPER,NAVG,LINE1,LINE2,LINE3	RAM17160
	WRITE (13) NRECEP,(RREU(I),I=1,NRECEP),(SREU(I),I=1,NRECEP)	RAM17170
	GO TO 1120	RAM17180
1080	IF (IOPT(9).EQ.0) GO TO 1100	RAM17190
	IF (IDAY.EQ.0) GO TO 1100	RAM17200
C	SKIP PREVIOUSLY USED HOURLY PT. EMISSIONS.	RAM17210
	ISKIP=IDAY*24	RAM17220
	DO 1090 I=1,ISKIP	RAM17230
1090	READ (15)	RAM17240
1100	IF (IOPT(10).EQ.0) GO TO 1120	RAM17250
	IF (IDAY.EQ.0) GO TO 1120	RAM17260
C	SKIP PREVIOUSLY USED HOURLY AREA EMISSIONS.	RAM17270
	ISKIP=IDAY*24	RAM17280
	DO 1110 I=1,ISKIP	RAM17290
1110	READ (16)	RAM17300

1120	IDAY=IDATE(2)-1	RAM17310
	IF (IDAY.LE.0.OR.IOPT(8).EQ.1) GO TO 1140	RAM17320
C	SKIP PREVIOUSLY USED HOURLY MET. RECORDS.	RAM17330
	DO 1130 I=1,IDAY	RAM17340
1130	READ (11)	RAM17350
1140	CONTINUE	RAM17360
C		RAM17370
C-->-->-->	SECTION P - START LOOPS FOR DAY AND AVG TIME; READ MET DATA.	RAM17380
C		RAM17390
1150	IDAY=IDAY+1	RAM17400
	D=IDAY	RAM17410
	NHRS=0	RAM17420
	IF (IOPT(8).EQ.1) GO TO 1190	RAM17430
C	IF OPTION 8 EQUALS ZERO, INPUT MET DATA OFF DISK (UNIT 11)	RAM17440
	READ (11) JYR,ID,DAY1,IKST,QU,QTEMP,DUMR,QTHETA,HLH	RAM17450
	DO 1151 JMI=1,24	RAM17460
	IDUMR(JMI)=DUMR(JMI)+0.5	RAM17470
1151	CONTINUE	RAM17480
	IF (JYR.NE.IDATE(1)) GO TO 1160	RAM17490
	IF (DAY1.EQ.D) GO TO 1170	RAM17500
C	DATE ON MET TAPE DOES NOT MATCH INTERNAL DATE	RAM17510
C	WRITE ERROR STATEMENT	RAM17520
1160	WRITE (10,2040) JYR,IDATE(2),IDATE(1),IDAY	RAM17530
	CALL WAUDIT	
	STOP	RAM17540
C	MODIFY WIND VECTOR BY 180 DEGREES. SINCE FLOW VECTORS WERE	RAM17550
C	OUTPUT FROM RAMMET. THIS CONVERTS BACK TO WIND DIRECTIONS.	RAM17560
1170	IDATE(2)=DAY1	RAM17570
	DO 1180 IQ=1,24	RAM17580
	IF (IKST(IQ).EQ.7) IKST(IQ)=6	RAM17590
	QTHETA(IQ)=QTHETA(IQ)+180.	RAM17600
	IF (QTHETA(IQ).GT.360.) QTHETA(IQ)=QTHETA(IQ)-360.	RAM17610
1180	QHL(IQ)=HLH(MIX,IQ)	RAM17620
1190	NB=IHSTRT	RAM17630
	NE=NB+NAVG-1	RAM17640
	IF (NB.GT.0) GO TO 1200	RAM17650
C	WRITE ERROR STATEMENT	RAM17660
	WRITE (10,2050) IHSTRT	RAM17670
	CALL WAUDIT	
	STOP	RAM17680
C	START LOOP FOR AVERAGING PERIOD.	RAM17690
1200	U=0.0	RAM17700
	TEMP=0.0	RAM17710
	DELN=0.0	RAM17720
	DELM=0.0	RAM17730
	DO 1210 I=1,7	RAM17740
1210	IFREQ(I)=0.0	RAM17750
	NRECEP=NPREC	RAM17760
	DO 1240 I=NB,NE	RAM17770
	JHR=I	RAM17780
	DAY2=IDATE(2)	RAM17790
	IF (IOPT(8).EQ.0) GO TO 1220	RAM17800
C		RAM17810
C	READ CARD TYPE 18 IF IOPT(8) =1. (HOURLY MET DATA)	RAM17820
C	(SEE DESCRIPTION, SECTION B).	RAM17830
C		RAM17840
	READ (IN,*) JYR,DAY1,JHR,IKST(JHR),QU(JHR),QTEMP(JHR),QTHETA(JHR),	RAM17850
	1QHL(JHR)	RAM17860
	IF (I.NE.NB) GO TO 1220	RAM17870
C	REDEFINE START HOURS AND DATES AT FIRST HOUR OF EACH	RAM17880
C	AVERAGING PERIOD IF READING HOURLY MET DATA.	RAM17890
C	THE PURPOSE OF THIS IS TO BE ABLE TO CALCULATE	RAM17900
C	FOR SEVERAL AVG-PERIODS THAT ARE NOT CONTINUOUS	RAM17910
C	IN TIME.	RAM17920
	IDATE(1)=JYR	RAM17930
	IHSTRT=JHR	RAM17940
	ISTDAY=DAY1	RAM17950
	IDATE(2)=ISTDAY	RAM17960
	DAY2=IDATE(2)	RAM17970
1220	IF (IKST(JHR).EQ.7) IKST(JHR)=6	RAM17980

	IF (IOPT(15).EQ.0.AND.IOPT(16).EQ.0.AND.IOPT(23).EQ.1) GO TO 1240	RAM17990
C		RAM18000
C-->-->-->	SECTION Q - CALCULATE AND WRITE MET. SUMMARY INFO.	RAM18010
C		RAM18020
	IF (IOPT(23).EQ.1) GO TO 1230	RAM18030
	IF (I.EQ.NB) WRITE (IO,2570) NAVG,IHSTRT,IDATE	RAM18040
	WRITE (IO,2580) JHR,QTHETA(JHR),QU(JHR),QHL(JHR),QTEMP(JHR),IKST(JHR)	RAM18050
	1HR)	RAM18060
1230	TRAD=QTHETA(JHR)*0.01745329	RAM18070
	SINT=SIN(TRAD)	RAM18080
	COST=COS(TRAD)	RAM18090
C	CALCULATE WIND COMPONENTS	RAM18100
	URES=QU(JHR)	RAM18110
	A=URES*SINT	RAM18120
	B=URES*COST	RAM18130
	DELM=DELM+A	RAM18140
	DELN=DELN+B	RAM18150
	TEMP=TEMP+QTEMP(JHR)	RAM18160
	U=U+URES	RAM18170
	KST=IKST(JHR)	RAM18180
	IFREQ(KST)=IFREQ(KST)+1	RAM18190
C	END LOOP TO READ ALL MET DATA FOR AVERAGING PERIOD.	RAM18200
1240	CONTINUE	RAM18210
	IF (IOPT(15).EQ.0.AND.IOPT(16).EQ.0.AND.IOPT(23).EQ.1) GO TO 1310	RAM18220
C	CALCULATE RESULTANT WIND DIRECTION THETA	RAM18230
	DELN=DELN/NAVG	RAM18240
	DELM=DELM/NAVG	RAM18250
	THETA=ANGARC(DELM,DELN)	RAM18260
C	CALCULATE AVERAGE AND RESULTANT SPEED AND PERSISTENCE.	RAM18270
	U=U/NAVG	RAM18280
	TEMP=TEMP/NAVG	RAM18290
	URES=SQRT(DELN*DELN+DELM*DELM)	RAM18300
	A=URES/U	RAM18310
C	DETERMINE MODAL AND AVERAGE STABILITY	RAM18320
	LSMAX=0	RAM18330
	DO 1250 I=1,7	RAM18340
	LST=IFREQ(I)	RAM18350
	IF (LST.LE.LSMAX) GO TO 1250	RAM18360
	LSMAX=LST	RAM18370
	LSTAB=I	RAM18380
1250	CONTINUE	RAM18390
	ID=LSTAB+1	RAM18400
	KST=LSTAB	RAM18410
	DO 1260 I=ID,7	RAM18420
	IF (LSMAX.EQ.IFREQ(I)) GO TO 1270	RAM18430
1260	CONTINUE	RAM18440
	GO TO 1290	RAM18450
C	IF TIE FOR MAX MODAL STABILITY, CALCULATE AVERAGE STABILITY	RAM18460
1270	IQ=0	RAM18470
	DO 1280 J=1,7	RAM18480
1280	IQ=IQ+IFREQ(J)*J	RAM18490
	KST=FLOAT(IQ)/FLOAT(NAVG)+0.5	RAM18500
C	PRINT RESULTANT MET DATA SUMMARY FOR AVERAGING PERIOD.	RAM18510
1290	IF (IOPT(23).EQ.1) GO TO 1300	RAM18520
	WRITE (IO,2590) THETA,URES,U,TEMP,A,KST	RAM18530
C		RAM18540
C-->-->-->	SECTION R - DETERMINE ADDITIONAL RECEPTORS FOR THIS AVG-PERIOD	RAM18550
C	(OPTIONAL).	RAM18560
C		RAM18570
C	DETERMINE RECEPTORS ACCORDING TO SIGNIFICANT SOURCES	RAM18580
C	IOPT(15) CONTROL OPTION, SIGNIFICANT POINT RECEPTORS?	RAM18590
C	IOPT(16) CONTROL OPTION, SIGNIFICANT AREA RECEPTORS?	RAM18600
1300	IF ((IOPT(15)+IOPT(16)).EQ.0) GO TO 1310	RAM18610
	TRAD=THETA*0.01745329	RAM18620
	SINT=SIN(TRAD)	RAM18630
	COST=COS(TRAD)	RAM18640
	CALL GREC	RAM18650
C	FILL IN RECEPTORS WITH HONEYCOMB ARRAY	RAM18660
C	IOPT(17) CONTROL OPTION, FILL IN HONEYCOMB RECEPTORS? 0=NO, 1=YES	RAM18670
1310	IF (IOPT(17).EQ.0) GO TO 1320	RAM18680

	WRITE (10,2600) HRMNU,HRMXU,HSMNU,HSMXU,GRDSPU	RAM18690
	CALL JMHON	RAM18700
1320	IF (NRECEP.NE.0) GO TO 1330	RAM18710
C	WRITE ERROR STATEMENT	RAM18720
	WRITE (10,2060)	RAM18730
	CALL WAUDIT	
	STOP	RAM18740
C	INITIALIZE CONCENTRATION SUMS	RAM18750
C	IF SIGNIFICANT OR HONEYCOMB RECEPTORS,WRITE CAUTIONING STATEMENT.	RAM18760
1330	IF ((IOPT(15)+IOPT(16)+IOPT(17)).GT.0) WRITE (10,2610)	RAM18770
C	REDEFINE NB AND NE IN CASE NON-CONSECUTIVE DAYS ARE BEING RUN	RAM18780
	IF (IOPT(8).EQ.0) GO TO 1340	RAM18790
	NB=IHSTRT	RAM18800
	NE=IHSTRT+NAVG-1	RAM18810
C		RAM18820
C-->-->-->	SECTION S - INITIALIZE FOR HOURLY LOOP.	RAM18830
C		RAM18840
C	INITIALIZE SUMS FOR CONC AND PARTIAL CONC FOR AVG PERIOD.	RAM18850
1340	DO 1370 K=1,NRECEP	RAM18860
	ACHI(K)=0.	RAM18870
	PCHI(K)=0.0	RAM18880
	DO 1350 I=1,11	RAM18890
1350	ASIGS(K,I)=0.	RAM18900
	DO 1360 I=1,26	RAM18910
1360	PSIGS(K,I)=0.0	RAM18920
1370	CONTINUE	RAM18930
C	IF SAVING PARTIAL CONCENTRATIONS, WRITE SECOND RECORD .	RAM18940
	IF (IOPT(40).EQ.0) GO TO 1380	RAM18950
	WRITE (10) NRECEP,NPT,NAS,(RREU(I),I=1,NRECEP),(SREU(I),I=1,NRECEP	RAM18960
	1)	RAM18970
C		RAM18980
C-->-->-->	SECTION T - BEGIN HOURLY LOOP.	RAM18990
C		RAM19000
1380	DO 1580 ID=NB,NE	RAM19010
	LH=ID	RAM19020
	IF (LH.LE.24) GO TO 1390	RAM19030
	LH=MOD(ID,24)	RAM19040
	IF (LH.EQ.1) IDATE(2)=DAY1	RAM19050
C	INITIALIZE SUMS FOR CONC AND PARTIAL CONC FOR HOURLY PERIODS.	RAM19060
1390	DO 1420 K=1,NRECEP	RAM19070
	AHCHI(K)=0.	RAM19080
	PHCHI(K)=0.0	RAM19090
	DO 1400 I=1,11	RAM19100
1400	AHSIGS(K,I)=0.	RAM19110
	DO 1410 I=1,26	RAM19120
1410	PHSIGS(K,I)=0.0	RAM19130
1420	CONTINUE	RAM19140
C	SET MET CONDITIONS FOR THIS HOUR	RAM19150
	THETA=QTHETA(LH)	RAM19160
C	DETERMINE WIND DIRECTION CONTROL, IWD, 90 DEG. QUADRANT OF WIND	RAM19170
C		RAM19180
	DO 1430 I=1,3	RAM19190
	IF (THETA.LE.DEG(I)) GO TO 1440	RAM19200
1430	CONTINUE	RAM19210
	I=4	RAM19220
1440	IWD=I	RAM19230
	U=QU(LH)	RAM19240
	HL=QHL(LH)	RAM19250
	TEMP=QTEMP(LH)	RAM19260
	KST=IKST(LH)	RAM19270
	TRAD=THETA*0.01745329	RAM19280
	SINT=SIN(TRAD)	RAM19290
	COST=COS(TRAD)	RAM19300
C	IF OPTION 9 IS 1, READ HOURLY EMISSIONS.	RAM19310
	IF (IOPT(9).EQ.0) GO TO 1450	RAM19320
C	WRITE ERROR STATEMENT	RAM19330
	IDCK=IDATE(1)*100000+IDATE(2)*100+LH	RAM19340
	READ (15) IDATA,(SOURCE(IPOL,I),I=1,NPT)	RAM19350
C	CHECK DATE	RAM19360
	IF (IDCK.EQ.IDATA) GO TO 1450	RAM19370

C	WRITE ERROR STATEMENT	RAM19380
	WRITE (IO,2070) IDCK,IDATA	RAM19390
	CALL WAUDIT	
	STOP	
C	CALCULATE POINT SOURCE CONTRIBUTIONS	RAM19400
1450	CALL PT	RAM19410
C	CHECK FOR AREA SOURCES	RAM19420
	IF (IOPT(6).NE.1) GO TO 1490	RAM19430
C	IOPT(10) CONTROL OPTION, HOURLY EMISSION INPUT? 0=NO, 1=YES	RAM19440
	IF (IOPT(10).EQ.0) GO TO 1480	RAM19450
	IDCK=IDATE(1)*100000+IDATE(2)*100+LH	RAM19460
C	READ HOURLY AREA SOURCE EMISSION RECORD	RAM19470
	READ (16) IDATA,(ASORC(IPOL,I),I=1,NAS)	RAM19480
C	CHECK DATE	RAM19490
	IF (IDCK.EQ.IDATA) GO TO 1460	RAM19500
C	WRITE ERROR STATEMENT	RAM19510
	WRITE (IO,2080) IDCK,IDATA	RAM19520
	CALL WAUDIT	RAM19530
	STOP	
C	CONVERT HOURLY AREA EMISSIONS FROM G/SEC TO G/SQ. M/SEC	RAM19540
1460	DO 1470 I=1,NAS	RAM19550
C	CONVERT SIDE LENGTH TO METERS.	RAM19560
C	NOTE: SIDE LENGTH HAD BEEN MULTIPLIED BY .5 ABOVE FOR TIME	RAM19570
C	CONSIDERATIONS	RAM19580
	SF=ASORC(5,I)*2000*CONTWO	RAM19590
1470	ASORC(IPOL,I)=ASORC(IPOL,I)/(SF*SF)	RAM19600
C	SET UP INTEGRATION TABLES FOR AREA SOURCE CALCULATIONS	RAM19610
1480	CALL JMH54	RAM19620
C	CALCULATE AREA SOURCE CONTRIBUTIONS	RAM19630
	CALL JMHARE	RAM19640
C	DETERMINE TOTAL CONCENTRATION.	RAM19650
1490	DO 1500 K=1,NRECEP	RAM19660
1500	GRANDT(K)=AHCHI(K)+PHCHI(K)	RAM19670
	IF (IOPT(41).EQ.0) GO TO 1510	RAM19680
C	WRITE HOURLY CONCENTRATIONS TO TAPE	RAM19690
C	THIS WILL GENERATE NPER*NAVG RECORDS.	RAM19700
	WRITE (12) IDATE(2),LH,(GRANDT(I),I=1,NRECEP)	RAM19710
C		RAM19720
C->->->->	SECTION U - CALCULATE AND STORE FOR HIGH-FIVE TABLE.	RAM19730
C		RAM19740
1510	NHR=NHR+1	RAM19750
C	IF OPTION 36 IS 1, DELETE COMPUTATIONS FOR AVG CONC.	RAM19760
C	FOR LENGTH OF RECORD AND HIGH-FIVE TABLE.	RAM19770
	IF (IOPT(36).EQ.1) GO TO 1570	RAM19780
C	CUMULATE CONCENTRATIONS FOR AVG TIMES AND LENGTH OF RECORD.	RAM19790
C		RAM19800
C	FOR DEFAULT OPTION DETERMINE CALM HOURS.	RAM19810
C	FOR CALM HOURS, CONCENTRATIONS AT EACH RECEPTOR ARE	RAM19820
C	SET EQUAL TO ZERO.	RAM19830
C	--- A CALM HOUR IS AN HOUR WITH A WIND SPEED	RAM19840
C	OF 1.00 M/S AND A WIND DIRECTION THE SAME	RAM19850
C	AS THE PREVIOUS HOUR.	RAM19860
	IF (IOPT(38).EQ.1.AND.QU(LH).LT.1.009.AND.ITMIN1.EQ.	RAM19870
	*IDUMR(LH)) THEN	RAM19880
	ICALM=ICALM+1	RAM19890
	DO 955 K=1,NRECEP	RAM19900
	GRANDT(K)=0.0	RAM19910
955	CONTINUE	RAM19920
	GO TO 971	RAM19930
	END IF	RAM19940
	DO 1530 K=1,NRECEP	RAM19950
	DO 1520 L=1,NAVT	RAM19960
1520	CONC(K,L)=CONC(K,L)+GRANDT(K)	RAM19970
1530	SUM(K)=SUM(K)+GRANDT(K)	RAM19980
C	STORE DATE FOR WHICH CONCS. HAVE BEEN CALCULATED.	RAM19990
971	JDAY=IDATE(2)	RAM20000
C	SUBROUTINE RANK IS CALLED WHENEVER A COUNTER	RAM20010
C	INDICATES THAT ENOUGH END TO END HOURLY CONCENTRATIONS	RAM20020
C	HAVE BEEN STORED OFF TO COMPLETE AN AVG TIME.	RAM20030
C	NP3, NP8, NP24, NPX ARE USED AS COUNTERS FOR EACH	RAM20040
		RAM20050

C	AVG TIME AND ARE ZEROED AFTER EACH CALL TO RANK.	RAM20060
C		RAM20070
C	FOR THE DEFAULT OPTION CALCULATE AVERAGE	RAM20080
C	CONCENTRATION FOR APPROPRIATE AVERAGING PERIOD.	RAM20090
C	SET UP CALM FLAG FOR ENTRY INTO SUBROUTINE RANK.	RAM20100
C		RAM20110
	IF(IOPT(38).EQ.0) GOTO 979	RAM20120
	CALL RANK(1)	RAM20130
	NP3=NP3+1	RAM20140
	IF(QU(LH).LT.1.009.AND.IDUMR(LH).EQ.ITMIN1)ICFL3=1	RAM20150
	IF(NP3.NE.3) GO TO 974	RAM20160
C	FOR 3 HOUR AVERAGING PERIOD DIVIDE SUM BY 3.0.	RAM20170
	DO 972 LQ=1,NRECEP	RAM20180
972	CONC(LQ,2)=CONC(LQ,2)/3.0	RAM20190
	LL2=2	RAM20200
	IF(ICFL3.EQ.1)LL2=22	RAM20210
	CALL RANK(LL2)	RAM20220
	NP3=0	RAM20230
	ICFL3=0	RAM20240
974	NP8=NP8+1	RAM20250
	IDIV8=IDIV8+1	RAM20260
	IF(QU(LH).LT.1.009.AND.IDUMR(LH).EQ.ITMIN1)THEN	RAM20270
	IDIV8=IDIV8-1	RAM20280
	ICFL8=1	RAM20290
	END IF	RAM20300
	IF(NP8.NE.8)GO TO 976	RAM20310
	IF(IDIV8.LT.6)IDIV8=6	RAM20320
	DIV8=IDIV8	RAM20330
C	FOR 8 HOUR AVERAGING PERIOD DIVIDE THE SUM OF THE HOURLY	RAM20340
C	CONCENTRATIONS BY THE NUMBER OF NON-CALM HOURS OR 6.0	RAM20350
C	WHICHEVER IS GREATER.	RAM20360
	DO 975 LQ=1,NRECEP	RAM20370
975	CONC(LQ,3)=CONC(LQ,3)/DIV8	RAM20380
	LL3=3	RAM20390
	IF(ICFL8.EQ.1)LL3=33	RAM20400
	CALL RANK(LL3)	RAM20410
	NP8=0	RAM20420
	IDIV8=0	RAM20430
	ICFL8=0	RAM20440
976	NP24=NP24+1	RAM20450
	IDIV24=IDIV24+1	RAM20460
	IF(QU(LH).LT.1.009.AND.IDUMR(LH).EQ.ITMIN1)THEN	RAM20470
	IDIV24=IDIV24-1	RAM20480
	ICFL24=1	RAM20490
	END IF	RAM20500
	IF(NP24.NE.24)GO TO 1011	RAM20510
	IF(IDIV24.LT.18)IDIV24=18	RAM20520
	DIV24=IDIV24	RAM20530
C	FOR 24 HOUR AVERAGING PERIOD DIVIDE THE SUM OF THE HOURLY	RAM20540
C	CONCENTRATIONS BY THE NUMBER OF NON-CALM HOURS OR 18,	RAM20550
C	WHICHEVER IS GREATER.	RAM20560
	DO 977 LQ=1,NRECEP	RAM20570
977	CONC(LQ,4)=CONC(LQ,4)/DIV24	RAM20580
	LL4=4	RAM20590
	IF(ICFL24.EQ.1)LL4=44	RAM20600
	CALL RANK(LL4)	RAM20610
	NP24=0	RAM20620
	IDIV24=0	RAM20630
	ICFL24=0	RAM20640
1011	ITMIN1=IDUMR(LH)	RAM20650
	GO TO 1570	RAM20660
C		RAM20670
C	WHEN DEFAULT OPTION IS NOT USED, DETERMINE ENTRY INTO	RAM20680
C	SUBROUTINE RANK FOR APPROPRIATE AVERAGING PERIOD.	RAM20690
C	RANKING BASED ON HIGH AVERAGING PERIOD SUM.	RAM20700
C		RAM20710
979	CALL RANK (1)	RAM20720
	NP3=NP3+1	RAM20730
	IF (NP3.NE.3) GO TO 1540	RAM20740
	CALL RANK (2)	RAM20750

1540	NP3=0	RAM20760
	NP8=NP8+1	RAM20770
	IF (NP8.NE.8) GO TO 1550	RAM20780
	CALL RANK (3)	RAM20790
	NP8=0	RAM20800
1550	NP24=NP24+1	RAM20810
	IF (NP24.NE.24) GO TO 1560	RAM20820
	CALL RANK (4)	RAM20830
	NP24=0	RAM20840
1560	IF (NAVT.EQ.4) GO TO 1570	RAM20850
	NPX=NPX+1	RAM20860
	IF (NPX.NE.NAV5) GO TO 1570	RAM20870
	CALL RANK (5)	RAM20880
	NPX=0	RAM20890
C		RAM20900
C-->-->-->	SECTION V - END HOURLY, AVERAGING TIME, AND DAILY LOOPS.	RAM20910
C		RAM20920
1570	IF (IOPT(24).EQ.1) GO TO 1580	RAM20930
C	IF IOPT(24) = 1, SKIP HOURLY OUTPUT.	RAM20940
	CALL OUTPT	RAM20950
1580	CONTINUE	RAM20960
C		RAM20970
C	END OF HOURLY LOOP	RAM20980
C		RAM20990
C	IF (NE.GT.24) IDATE(2)=ISTDAY	RAM21000
	DETERMINE AVG.-PER.CONCENTRATIONS.	RAM21010
	DO 1590 K=1,NRECEP	RAM21020
	ACHI(K)=ACHI(K)/NAVG	RAM21030
	PCHI(K)=PCHI(K)/NAVG	RAM21040
1590	GRANDT(K)=ACHI(K)+PCHI(K)	RAM21050
	IF (IOPT(42).EQ.0) GO TO 1600	RAM21060
C	WRITE PERIODIC CONC. TO DISK/TAPE- FOR LONG-TERM	RAM21070
C	APPLICATION. THIS STATEMENT WILL GENERATE 'NPER' RECORDS	RAM21080
	WRITE (13) IDATE(2),NE,(GRANDT(K),K=1,NRECEP)	RAM21090
1600	IF (IOPT(43).EQ.0) GO TO 1620	RAM21100
C	PUNCH AVG.-PER. CONC. CARDS (ONE FOR EACH RECEPTOR).	RAM21110
	DO 1610 K=1,NRECEP	RAM21120
	GWU=GRANDT(K)*1.0E+06	RAM21130
	A=ACHI(K)*1.0E+06	RAM21140
	B=PCHI(K)*1.0E+06	RAM21150
	WRITE (1,2090) RREU(K),SREU(K),GWU,A,B,K, IDATE,NE,NAVG	RAM21160
1610	CONTINUE	RAM21170
C	OUTPUT AVG.-PER. RESULTS	RAM21180
1620	IF (IOPT(32).EQ.1) GO TO 1630	RAM21190
	CALL OUTAV	RAM21200
1630	NP=NP+1	RAM21210
	NHRS=NHRS+NAVG	RAM21220
C	NEXT STATEMENT IS BRANCH FOR END OF RUN.	RAM21230
	IF (NP.GE.NPER) GO TO 1660	RAM21240
	IF (NHRS.LT.24) GO TO 1640	RAM21250
	IF (IOPT(39).EQ.0) GO TO 1150	RAM21260
C	NEXT STATEMENT CHECKS FOR END OF SEGMENTED RUN.	RAM21270
	IF (IDAY.GE.LDRUN) GO TO 1650	RAM21280
	GO TO 1150	RAM21290
C		RAM21300
C	END OF LOOP FOR CALENDAR DAYS	RAM21310
C		RAM21320
1640	NB=NB+NAVG	RAM21330
	NE=NE+NAVG	RAM21340
	IF (NB.LE.24) GO TO 1200	RAM21350
	NB=MOD(NB,24)	RAM21360
	NE=NB+NAVG-1	RAM21370
	GO TO 1200	RAM21380
C		RAM21390
C	END OF LOOP FOR AVERAGING PERIOD.	RAM21400
C		RAM21410
C	IF SEGMENTED RUN, TEMPORARILY STORE	RAM21420
C	HIGH-FIVE INFO ON UNIT 14 FILE.	RAM21430
1650	WRITE (14) IDAY,SUM,NHR,DAY1A,HRL,HMAXA,NDAY,IHR	RAM21440
	WRITE (10,2620) IDAY	RAM21450

GO TO 1750	RAM21460
1660 IF (IOPT(36).EQ.1) GO TO 1750	RAM21470
C	RAM21480
C->->->SECTION W - WRITE AVERAGE CONC. AND HIGH-FIVE TABLES.	RAM21490
C	RAM21500
C IF OPTION 36 = 0, WRITE AVERAGE CONCENTRATION.	RAM21510
C FOR LENGTH OF RECORD AND HIGH-FIVE TABLE.	RAM21520
DO 1670 J=1,NRECEP	RAM21530
STAR(1,J)=BLNK	RAM21540
STAR(2,J)=BLNK	RAM21550
1670 CONTINUE	RAM21560
WRITE (IO,2630) LINE1,LINE2,LINE3	RAM21570
HR2=NE	RAM21580
C FOR DEFAULT OPTION CALCULATE AND REPORT THE	RAM21590
C NUMBER OF CALMS FOR AVERAGING PERIOD.	RAM21600
IF(IOPT(38).EQ.1)THEN	RAM21610
NHR=NHR-ICALM	RAM21620
WRITE(6,1761)ICALM	RAM21630
END IF	RAM21640
C INITIALIZE PERIODIC CONC TO BEGIN RANKING FOR PERIODIC MAX	RAM21650
SUM(1)=SUM(1)/NHR	RAM21660
HF=SUM(1)	RAM21670
ID=1	RAM21680
C FIND HIGHEST AVERAGE CONC. AMONG RECEPTORS.	RAM21690
DO 1680 K=2,NRECEP	RAM21700
SUM(K)=SUM(K)/NHR	RAM21710
IF (SUM(K).LE.HF) GO TO 1680	RAM21720
ID=K	RAM21730
HF=SUM(K)	RAM21740
1680 CONTINUE	RAM21750
STAR(1,ID)=STR	RAM21760
C WRITE AVERAGE CONC.(HIGHEST HAS ASTERISK).	RAM21770
WRITE (IO,2640) DAY1A,HR1,DAY2,HR2	RAM21780
DO 1690 K=1,NRECEP	RAM21790
1690 WRITE (IO,2650) K,ITYPE(K),ICODE(K),(RNAME(J,K),J=1,2),RREU(K),SRER	RAM21800
LU(K),STAR(1,K),SUM(K)	RAM21810
STAR(1,ID)=BLNK	RAM21820
C LOOP TO WRITE HIGH-FIVE TABLE FOR 4 OR 5 AVG TIMES.	RAM21830
DO 1740 L=1,NAVT	RAM21840
C ASTERISKS DEPICT RECEPTORS WITH HIGHEST AND	RAM21850
C SECOND HIGHEST CONCENTRATIONS.	RAM21860
ID=1	RAM21870
IQ=1	RAM21880
A=HMAXA(1,1,L)	RAM21890
B=HMAXA(2,1,L)	RAM21900
DO 1710 K=2,NRECEP	RAM21910
IF (HMAXA(1,K,L).LE.A) GO TO 1700	RAM21920
A=HMAXA(1,K,L)	RAM21930
ID=K	RAM21940
1700 IF (HMAXA(2,K,L).LE.B) GO TO 1710	RAM21950
B=HMAXA(2,K,L)	RAM21960
IQ=K	RAM21970
1710 CONTINUE	RAM21980
STAR(1,ID)=STR	RAM21990
STAR(2,IQ)=STR	RAM22000
C WRITE HIGH-FIVE TABLE FOR AN AVERAGING TIME.	RAM22010
IF((IOPT(38).EQ.1.AND.L.EQ.1).OR.(IOPT(38).NE.1))THEN	RAM22020
WRITE (IO,2660) NTIME(L),TITLE(IP),(I,I=1,5)	RAM22030
END IF	RAM22040
IF(IOPT(38).EQ.1.AND.L.NE.1)THEN	RAM22050
WRITE (IO,2661) NTIME(L),TITLE(IP),(I,I=1,5)	RAM22060
END IF	RAM22070
DUM=ATIME(L)	RAM22080
DO 1730 K=1,NRECEP	RAM22090
C SET CALM FLAG FOR PRINTING.	RAM22100
C RESET HOUR VARIABLE FOR CALM HOURS.	RAM22110
IF(IOPT(38).EQ.1)THEN	RAM22120
DO 1712 J=1,5	RAM22130
CF(J)=BLNK	RAM22140
IF(IHR(J,K,L).GT.24)THEN	RAM22150

	IHR(J,K,L)=IHR(J,K,L)-100	RAM22160
	CF(J)=C	RAM22170
	END IF	RAM22180
1712	CONTINUE	RAM22190
	END IF	RAM22200
	IF(IOPT(38).EQ.1)GO TO 1711	RAM22210
C	CALCULATE AVERAGE CONCENTRATIONS WHEN	RAM22220
C	DEFAULT OPTION IS NOT ON.	RAM22230
	DO 1720 J=1,5	RAM22240
1720	HMAXA(J,K,L)=HMAXA(J,K,L)/DUM	RAM22250
1711	WRITE (10,2670) K,RREU(K),SREU(K),(STAR(J,K),HMAXA(J,K,L),CF(J),	RAM22260
	1NDAY(J,K,L),IHR(J,K,L),J=1,2),(HMAXA(J,K,L),CF(J),NDAY(J,K,L),	RAM22270
	2IHR(J,K,L),J=3,5)	RAM22280
1730	CONTINUE	RAM22290
C	INITIALIZE ASTERISK STORAGE TO BLANKS.	RAM22300
	STAR(1,ID)=BLNK	RAM22310
	STAR(2,IQ)=BLNK	RAM22320
1740	CONTINUE	RAM22330
C		RAM22340
C-->-->-->SECTION X - CLOSE OUT FILES.		RAM22350
C		RAM22360
1750	IF (IOPT(40).EQ.0) GO TO 1760	RAM22370
	END FILE 10	RAM22380
	END FILE 10	RAM22390
1760	IF (IOPT(41).EQ.0) GO TO 1770	RAM22400
	END FILE 12	RAM22410
	END FILE 12	RAM22420
1770	IF (IOPT(42).EQ.0) GO TO 1780	RAM22430
	END FILE 13	RAM22440
	END FILE 13	RAM22450
1780	WRITE (10,2680)	RAM22460
	CALL WAUDIT	
	STOP	RAM22470
C		RAM22480
C-->-->-->SECTION Y - FORMAT STATEMENTS.		RAM22490
C		RAM22500
C	INPUT FORMATS	RAM22510
C		RAM22520
1761	FORMAT(5X,T98,'# CALMS FOR PERIOD: ',I4)	RAM22530
1790	FORMAT (20A4/20A4/20A4)	RAM22540
1800	FORMAT (50I1)	RAM22550
1810	FORMAT (A4)	RAM22560
1820	FORMAT (3A4,8F8.2)	RAM22570
1830	FORMAT (3A4,6F10.2)	RAM22580
1840	FORMAT (26I3)	RAM22590
1850	FORMAT (2A4,2F10.3)	RAM22600
C		RAM22610
C	ERROR AND WARNING STATEMENT FORMATS	RAM22620
C		RAM22630
1860	FORMAT (1X,' NSIGP (THE NO. OF SIGNF POINT SOURCES) WAS FOUND',	TRAM22640
	10 EXCEED THE LIMIT (25). USER TRIED TO INPUT ',I3,' SOURCES',	RAM22650
	2***** EXECUTION TERMINATED *****')	RAM22660
1870	FORMAT (1X,' NSIGA (THE NO. OF SIGNIF. AREA SOURCES) WAS FOUND TO ',	RAM22670
	1' EXCEED THE LIMIT (10). USER TRIED TO INPUT ',I3,' SOURCES.',	RAM22680
	2***** EXECUTION TERMINATED *****')	RAM22690
1880	FORMAT (' USER TRIED TO INPUT MORE THAN ',I4,' POINT SOURCES. THIS	RAM22700
	1 GOES BEYOND THE CURRENT PROGRAM DIMENSIONS.')	RAM22710
1890	FORMAT (' USER TRIED TO INPUT MORE THAN ',I4,' AREA SOURCES. THIS	RAM22720
	1 GOES BEYOND THE CURRENT PROGRAM DIMENSIONS.')	RAM22730
1900	FORMAT (' DIMENSIONS TOO SMALL TO HOLD ARRAY ',I3,' BY ',I3)	RAM22740
1910	FORMAT (' AREA SOURCES, UNITS OR SIDE LENGTH SPECIFIED INCORRECTLY	RAM22750
	1; ERROR ON EAST MAX BOUNDARY.')	RAM22760
1920	FORMAT (' AREA SOURCES, UNITS OR SIDE LENGTH SPECIFIED INCORRECTLY	RAM22770
	1; ERROR ON NORTH MAX BOUNDARY.')	RAM22780
1930	FORMAT (' SOURCE ',I3,' IS ALREADY LOCATED AT POSITION (' ,I3,' ,',	IRAM22790
	13,') CHECK SOURCE ',I3)	RAM22800
1940	FORMAT (' AREA ARRAY IS TOO WIDE FOR PAGE SIZE, THEREFORE WILL NOT	RAM22810
	1 BE PRINTED')	RAM22820
1950	FORMAT (1H1,' ***ERROR---USER TRIED TO SPECIFY ',I4,' SIGNIFICANT	SRAM22830
	1 SOURCES, BUT IS ONLY ALLOWING ',I3,' TOTAL SIGNIFICANT SOURCES IN	TRAM22840

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2THIS RUN.',/2X,' RUN TERMINATED-CHECK INPUT DATA:' ) RAM22850
1960 FORMAT ('(MPS) THE INPUT SIGNIFICANT SOURCE NUMBER ', ' WAS FOUND TRAM22860
10 EQUAL ZERO - USER CHECK INPUT DATA.' ) RAM22870
1970 FORMAT (' THE INPUT LIMIT OF MAX DISTANCE FOR AREA INTEGRATION ', ' RAM22880
1 CONVERTS TO ', F10.3, ' KM WHICH EXCEEDS STORAGE ', ' LIMITATIONS. UPRAM22890
2 TO 116 KM DISTANCES ARE ALLOWED.' ) RAM22900
1980 FORMAT (47H ' ERROR IN SPECIFYING SIGNIF. POINT SOURCES ) RAM22910
1990 FORMAT ('ODISAGREEMENT OF IDENTIFIERS-', '/' SURFACE DATA FROM CARD RAM22920
1: STATION = ', I5, ' YEAR = ', I2, ' FROM MET FILE: STATRAM22930
2ION = ', I5, ' YEAR = ', I2, ' MIX HT DATA FROM CARD: STATION = ', I5 RAM22940
3, ' YEAR = ', I2, ' FROM MET FILE: STATION = ', I5, ' YEARRAM22950
4 = ', I2 ) RAM22960
2000 FORMAT (1X, '****USER EITHER TRIED TO INPUT MORE THAN 180 ', ' RECEPTRAM22970
IORS OR ENDR WAS NOT PLACED AFTER THE LAST RECEPTOR ', ' CARD *'/ *RAM22980
2*****EXECUTION TERMINATED*****') RAM22990
2010 FORMAT (1X, 'NO RECEPTORS HAVE BEEN CHOSEN') RAM23000
2020 FORMAT (1H0, ' DAYS DO NOT MATCH, IDAY = ', I4, ' IDAYS = ', I4) RAM23010
2030 FORMAT ('O RUN TERMINATED. CAN NOT WRITE FILES (OPTIONS 41, ' , ORAM23020
1R 42)'/1X, 'WHEN HAVING RAM GENERATE RECEPTORS FOR EACH AVG-PER', ' (RAM23030
2OPTIONS 15, 16, OR 17).') RAM23040
2040 FORMAT (' DATE ON MET. TAPE, ', I2, I3, ' , DOES NOT MATCH INTERNAL DARAM23050
1TE, ', I2, I3) RAM23060
2050 FORMAT (' HOUR ', I3, ' IS NOT PERMITTED. HOURS MUST BE DEFINED BETWRAM23070
1EEN 1 AND 24') RAM23080
2060 FORMAT (1X, 'NO RECEPTORS HAVE BEEN CHOSEN') RAM23090
2070 FORMAT (' DATE BEING PROCESSED IS = ', I8/1X, 'DATE OF HOURLY POINT RAM23100
1EMISSION RECORD IS = ', I8/1X, '***PLEASE CHECK EMISSION RECORDS ') RAM23110
2080 FORMAT (' DATE BEING PROCESSED IS = ', I8/1X, 'DATE OF HOURLY AREA EMRAM23120
1ISSION RECORD IS = ', I8/1X, '***PLEASE CHECK EMISSION RECORDS***') RAM23130
C RAM23140
C PUNCH CARD FORMAT(FOR OUTPUT, OPTION 43) RAM23150
C RAM23160
C RAM23170
C RAM23180
C RAM23190
C RAM23200
2100 FORMAT (1H1, T40, ' OUTPUT FROM ', A4, A1, ' RAM (VERSION 85364) ', /1X, RAM23210
1T40, ' AN AIR QUALITY DISPERSION MODEL IN ', /1X, T40, ' SECTION 1. GRAM23220
2UIDELINE MODELS ', /1X, T40, ' IN UNAMAP (VERSION 6) DEC 86 ', /1X, RAM23230
3, T40, ' SOURCE: UNAMAP FILE ON EPA'S UNIVAC 1110, RTP. NC.') RAM23240
2110 FORMAT (/1X, 20A4/1X, 20A4/1X, 20A4) RAM23250
2120 FORMAT ('O', T30, 'GENERAL INPUT INFORMATION'/2X, 'THIS IS THE ', A4, RAM23260
1A1, ' VERSION(81352) OF RAM FOR THE POLLUTANT ', A4, ' FOR ', I3, I3, RAM23270
2, '-HOUR PERIODS. '/2X, 'CONCENTRATION ESTIMATES BEGIN ON HOUR-', I2, ' RAM23280
3, ' JULIAN DAY-', I3, ' YEAR-', I2, ' ,'/1X, ' UNITS - THERE ARE ', F14, RAM23290
47, ' USER UNITS(INPUT UNITS) PER SMALLEST AREA SOURCE SQUARE SIDE LRAM23300
5LENGTH(INTERNAL UNIT)'/2X, 'CONONE - THERE ARE', F14.7, ' KILOMETERS PRAM23310
6ER USER UNIT'/2X, 'CONTWO - IT IS CALCULATED THAT THERE ARE', F14.7, RAM23320
7' KILOMETERS PER SMALLEST AREA SOURCE SQUARE SIDE LENGTH(INTERNAL RAM23330
8UNIT)'/2X, 'RECEPTOR HEIGHT IS ', F14.7, ' METERS') RAM23340
2130 FORMAT (1H0, 'THIS RUN WILL NOT CONSIDER ANY POLLUTANT LOSS.') RAM23350
2140 FORMAT (1H0, ' A HALF-LIFE OF ', F10.2, ' (SECONDS) HAS BEEN ASSUMED RAM23360
1 BY THE USER.') RAM23370
2150 FORMAT (1X, ' HIGH-FIVE SUMMARY CONCENTRATION TABLES ', ' WILL BE OUTRAM23380
1PUT FOR ', I3, ' AVERAGING PERIODS. '/' AVG TIMES ', ' OF 1, 3, 8, AND 2RAM23390
24 HOURS ARE AUTOMATICALLY DISPLAYED.') RAM23400
2160 FORMAT (1X, 'THE FIFTH AVERAGING PERIOD FOR THE HIGH ', '-FIVE TABLERAM23410
1S IS ', I3, ' HOURS') RAM23420
2170 FORMAT (1H0, T3, 'OPTION ', T16, 'OPTION LIST', T46, 'OPTION SPECIFICATRAM23430
1ION : 0= IGNORE OPTION'/1X, T68, ' 1= USE OPTION'/T25, 'TECHNICAL OPTRAM23440
2IONS'/1X, T7, I2, T16, 'NO STACK DOWNWASH', T70, I1/1X, T7, I2, T16, 'NO GRARAM23450
3DUAL PLUME RISE, ' T70, I1/1X, T7, I2, T16, 'USE BOUYANCY INDUCED DISPERRAM23460
4SION', T70, I1/1X, T7, I2, T16, 'NOT USED THIS VERSION', T70, I1) RAM23470
2180 FORMAT (1H0, T25, 'INPUT OPTIONS'/1X, T7, I2, T16, 'WILL YOU ', ' INPUT FORAM23480
1INT SOURCES?', T70, I1/1X, T7, I2, T16, 'WILL YOU INPUT AREA SOURCES?', TRAM23490
270, I1/1X, T7, I2, T16, 'WILL YOU USE EMISSIONS FROM PREVIOUS RUN? (UNIRAM23500
3T 9)', T70, I1/1X, T7, I2, T16, 'MET. DATA ON CARDS? (FROM UNIT', ' 11 OTHRAM23510
4ERWISE)', T70, I1/1X, T7, I2, T16, 'READ HOURLY PT. SOURCE' EMISSIONS (RAM23520
5UNIT 15)', T70, I1/1X, T7, I2, T16, 'READ HOURLY ', ' AREA SOURCE EMISSIONRAM23530
6NS (UNIT 16).', T70, I1/1X, T7, I2, T16, 'SPECIFY SIGNIF PT. SOURCES.' RAM23540

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7,T70,11/1X,T7,I2,T16,'SPECIFY SIGNIF. AREA ','SOURCES.',T70,11/1X, RAM23550
8T7,I2,T16,'NOT USED THIS VERSION',T70,11) RAM23560
2190 FORMAT (I10,T25,'RECEPTOR OPTIONS',/1X,T7,I2,T16,'WILL YOU ENTER ', RAM23570
1'RECEPTORS BY SPECIFYING COORDINATES?',T70,11/1X,T7,I2,T16,'DO', RAM23580
2YOU WANT RAM TO GENERATE RECEPTORS DOWNWIND',/1X,T7,T16,'OF',SIRAM23590
3GNIF. PT. SOURCES? (WILL DO SO BY AVG-PERIOD)',T70,11/1X,T7,I2,T16, RAM23600
46,'DO YOU WANT RAM TO GENERATE RECEPTORS DOWNWIND',/1X,T7,T16,'OF', RAM23610
5SIGNIF. AREA SOURCES?(WILL DO SO BY AVG-PERIOD)',T70,11/1X,T7,I2, RAM23620
6T16,'DO YOU WANT RAM TO GENERATE A HONEYCOMB ARRAY OF',/1X,T7,T16, RAM23630
7'RECEPTORS TO COVER A SPECIFIC AREA?',T70,11/1X,T7,I2,T16,'WILL YORAM23640
8U INPUT RADIAL DISTANCES(UP TO 5) TO GENERATE',/1X,T7,T16,'A POLARAM23650
9R COORDINATE RECEPTOR ARRAY',/1X,T7,T16,'(36 RECEP',TORS FOR EACH RAM23660
ADISTANCE)',T70,11/1X,T7,I2,T16,'NOT USED THIS', 'VERSION',T70,11) RAM23670
2200 FORMAT (I10,T25,'PRINTED OUTPUT OPTIONS',/1X,T7,I2,T16,'DELETE POI', RAM23680
1'NT SOURCE LIST',T70,11/1X,T7,I2,T16,'DELETE AREA SOURCE LIST A', RAM23690
2'ND MAP',T70,11/1X,T7,I2,T16,'DELETE EMISSIONS WITH HEIGHT TABLE', RAM23700
3T70,11/1X,T7,I2,T16,'DELETE RESULTANT MET. DATA SUMMARY FOR AVE',RRAM23710
4AGING PERIOD.',T70,11/1X,T7,I2,T16,'DELETE ALL HOURLY OUTPUT', (PRAM23720
5T.,AREA,& SUMMARIES)',T70,11/1X,T7,I2,T16,'DELETE HOURLY POI',NT RAM23730
6CONTRIBUTIONS',T70,11/1X,T7,I2,T16,'DELETE MET. DATA ON HR.',PT. RAM23740
7 CONTRIB.',T70,11/1X,T7,I2,T16,'DELETE PLUME HT. AND DIST.',TO FRAM23750
8INAL RISE ON',/1X,T7,T16,'HR. PT. CONTRIB.',T70,11/1X,T7,I2,T16,' RAM23760
9DELETE HOURLY AREA CONTRIBUTIONS',T70,11/1X,T7,I2,T16,'DELETE MET. RAM23770
A DATA ON HR. AREA CONTRIB.',T70,11/1X,T7,I2,T16,'DELETE HOURLY SUMRAM23780
BMARY.',T70,11/1X,T7,I2,T16,'DELETE MET.', 'DATA ON HOURLY SUMMARY.' RAM23790
C,T70,11) RAM23800
2210 FORMAT (1X,T7,I2,T16,'DELETE ALL AVG-PERIOD OUTPUT.',T70,11/1X,T7, RAM23810
1I2,T16,'DELETE POINT AVG-PERIOD CONTRIBUTIONS.',T70,11/1X,T7,I2,T16, RAM23820
26,'DELETE AREA AVG-PERIOD CONTRIBUTIONS.',T70,11/1X,T7,I2,T16,'DEL RAM23830
3ETE AVG-PERIOD SUMMARY.',T70,11/1X,T7,I2,T16,'DELETE AVE',RAGE CORAM23840
4NCENTRATIONS & HI-FIVE TABLE.',T70,11/1X,T7,I2,T16,'NOT', 'USED THRAM23850
5IS VERSION.',T70,11/1X,T25,'DEFAULT OPTION.', / RAM23860
61X,T7,I2,T16,'SET DEFAULT OPTION.',T70,11) RAM23870
2220 FORMAT (I10,T25,'OTHER CONTROL AND OUTPUT OPTIONS:',/1X,T7,I2,T16,' RAM23880
1RUN IS PART OF A SEGMENTED RUN.',T70,11/1X,T7,I2,T16,'WRITE PAR', RAM23890
2TIAL CONC.TO DISK OR TAPE (UNIT 10).',T70,11/1X,T7,I2,T16,'WRIT', RAM23900
3E', 'HOURLY CONC.TO DISK OR TAPE (UNIT 12).',T70,11/1X,T7,I2,T16,' RAM23910
4WRITE AVG-PERIOD CONC.TO DISK OR TAPE (UNIT 13).',T70,11/1X,T7,I2, RAM23920
5T16,'PUNCH AVERAGING-PERIOD CONC. ON CARDS (UNIT 1).',T70,11/1X,T7, RAM23930
6,I2,T16,'NOT USED THIS VERSION.',T70,11/1X,T7,I2,T16,'NOT USED', RAM23940
7THIS VERSION.',T70,11/1X,T7,I2,T16,'NOT USED THIS VERSION.',T70,11, RAM23950
8/1X,T7,I2,T16,'NOT USED THIS VERSION.',T70,11/1X,T7,I2,T16,'NOT USRAM23960
9ED THIS VERSION.',T70,11/1X,T7,I2,T16,'NOT USED THIS', 'VERSION.' RAM23970
A,T70,11/1X,T7,I2,T16,'NOT USED THIS VERSION.',T70,11) RAM23980
2230 FORMAT (I10,2X,'ANEMOMETER HEIGHT=',F10.2/3X,'WIND PROFILE WITH', RAM23990
1,'HEIGHT EXPONENTS CORRESPONDING TO STABILITY ARE AS FOLLOWS: /8X, RAM24000
2,FOR STABILITY A: ',F4.2,3X,' B: ',F4.2,3X,' C: ',F4.2,3X,' D: ', RAM24010
3,F4.2,3X,' E: ',F4.2,3X,' F: ',F4.2) RAM24020
2240 FORMAT ('0',T40,'POINT SOURCE INFORMATION',/1X,T5,'SOURCE',T23,'EARAM24030
1ST',T32,'NORTH',T40,'SO2(G/SEC) PART(G/SEC) STACK STACK',STACKRAM24040
2 STACK',3X,'POTEN. IMPACT',2X,'EFF',3X,' BUOY FLUX',/1X,T23,'COORRAM24050
3D',T32,'COORD', EMISSIONS EMISSIONS HT(M) TEMP(K) DIAM(M)' RAM24060
4,'VEL(M/SEC)(MICRO G/M**3) HT(M)',3X,'F',/1X,T17,' (USER URAM24070
5NITS)',T116,' M**4/S**3') RAM24080
2250 FORMAT (1X,I3,1X,3A4,1X,2F9.3,2F12.3,4F8.2,6PF13.3,0PF9.3,F9.3) RAM24090
2260 FORMAT ('0',T3,'SIGNIFICANT',A4,'POINT SOURCES',/1X,T8,'RANK',T2RAM24100
12,'CHI-MAX',T33,'SOURCE NO.',/1X,T17,'(MICROGRAMS/M**3)/1X) RAM24110
2270 FORMAT (1X,T9,I3,T18,6PF12.2,T35,I3) RAM24120
2280 FORMAT ('0',T20,'AREA SOURCE INFORMATION',/1X,T2,'SOURCE',T20,'EARAM24130
1ST',T28,'NORTH',T37,'SO2',T50,'PART',T61,'SIDE',T72,'EFFECTIVE SIGRAM24140
2NIFICANCE',/1X,T20,'COORD',T28,'COORD',T37,'EMISSIONS',T50,'EMISSIONRAM24150
3NS',T61,'LENGTH',T72,'HEIGHT',T81,'(G/M/SEC)/1X,T21,'(USER UNITS)RAM24160
4',T39,'(GRAMS/M**2/SEC)',T58,'(USER UNITS) (METERS)',/1X) RAM24170
2290 FORMAT (1X,T2,I3,1X,3A4,2F9.3,1X,2(1X,1PE11.4),2X,0PF6.3,5X,F6.3,2RAM24180
1X,1PE11.4) RAM24190
2300 FORMAT ('0',5X,'AREA SOURCE MAP ARRAY (IA)',/1X) RAM24200
2310 FORMAT (1X,I3,2X,4I13/1X) RAM24210
2320 FORMAT (/6X,4I13/1X) RAM24220
2330 FORMAT ('0THE ORIGIN IN INTERNAL UNITS IS ('F10.2,',',F10.2,')',/1RAM24230
1X,'THE SIZE OF THE AREA SOURCE ARRAY IS ('I5,',',',I5,','))' RAM24240

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2340 FORMAT (' RMIN=',F8.2,' RMAX=',F8.2,' SMIN=',F8.2,' SMAX=',F8.2,' RAM24250
1 (IN INTERNAL UNITS),) RAM24260
2350 FORMAT ('0'1X,T3,'SIGNIFICANT ',A4,' AREA SOURCES'//1X,T8,'RANK RAM24270
1',T20,'Q*LENGTH',T33,'SOURCE NO.'/1X,T19,'(G/M/SEC)/1X) RAM24280
2360 FORMAT (1X,T9,I3,T18,1PE12.4,T35,I3) RAM24290
2370 FORMAT (1X,'HEIGHT ABOVE 100M FOR POINT SOURCE',I4,3X,' HEIGHT=',F10.2,'FRAM24300
16.2,' (METERS)', EMISSIONS=',F10.2,' (G/SEC)',) RAM24310
2380 FORMAT ('0'4X,'TOTAL ',A4,' EMISSION AND CUMULATIVE FRACTION ACCORAM24320
1RDING TO HEIGHT'//1X,T12,'TOTAL POINT CUMULATIVE TOTAL AREARAM24330
2 CUMULATIVE'/1X,'HEIGHT(M) EMISSIONS(G/S) FRACTION EMISSIONRAM24340
3ONS(G/S) FRACTION'/1X) RAM24350
2390 FORMAT (1X,T2,I2,'-',I3,T11,F8.2,T26,F7.3,T41,F8.2,T56,F7.3) RAM24360
2400 FORMAT ('0',T2,'TOTAL',2X,F10.2,T39,F10.2) RAM24370
2410 FORMAT (1H0,21X,'ADDITIONAL INFORMATION ON SOURCES.'/1X,T21,'POINTRAM24380
1 SOURCE INFORMATION'/0',2X,'EMISSION INFORMATION FOR ',I4,' (NPT)RAM24390
2 POINT SOURCES HAS BEEN INPUT'/2X,I2,' SIGNIFICANT POINT SOURCERAM24400
3S (NSIGP) ',ARE TO BE USED FOR THIS RUN'/3X) RAM24410
2420 FORMAT (1H0,' USER SPECIFIED ',I3,' (NPT) SIGNIFICANT POINT ',SORAM24420
1URCES AS LISTED BY POINT SOURCE NUMBER: '/2X,25I5) RAM24430
2430 FORMAT (1X,'THE ORDER OF SIGNIFICANCE (IMPS) FOR 25', ' OR LESS POIRAM24440
1NT SOURCES USED IN THIS RUN AS LISTED BY POINT ',SOURCE NUMBER: '/RAM24450
22X,25I5) RAM24460
2440 FORMAT (1H0,T21,'AREA SOURCE INFORMATION'//2X,'EMISSION INFORMATIONRAM24470
1N FOR ',I4,' (NAS) AREA SOURCES HAVE BEEN DETERMINED BY RAM'/2X,I2RAM24480
2,' SIGNIFICANT AREA SOURCES (NSIGA) ARE TO BE USED FOR THIS RUN') RAM24490
2450 FORMAT (2X,'NUMBER OF AREA HEIGHT CLASSES (NHTS)=' ,I2/2X,'REPRESENTRAM24500
1TATIVE AREA SOURCE HEIGHTS FOR EACH HEIGHT CLASS (HINT) IN METERS RAM24510
2=' 3F10.2) RAM24520
2460 FORMAT (2X,'BREAK POINT HEIGHT BETWEEN THE AREA HEIGHT CLASSES (BPRAM24530
1H) IN METERS =',2F10.2) RAM24540
2470 FORMAT (2X,' FRACTION OF AREA SOURCE HEIGHT WHICH IS PHYSICAL HEIGRAM24550
1HT (FH) =',F10.3/2X,'LIMIT OF DISTANCE FOR AREA SOURCE INTEGRATIONRAM24560
2 TABLES (XLIM) IN USER UNITS =',F10.3/2X,'BOUNDARIES OF THE AREA 'RAM24570
3,'SOURCE GRID IN USER UNITS: '/1X,T6,'RMIN=',F10.3,5X,'RMAX=',F10.3RAM24580
4,5X,'SMIN=',F10.3,5X,'SMAX=',F10.3/2X,'SIZE(IRSIZ X ISSIZ) OF ',RAM24590
5' AREA SOURCE MAP ARRAY(IA) IN INTERNAL UNITS =',I3,' EAST-WEST ',RAM24600
6BY ',I3,' NORTH-SOUTH') RAM24610
2480 FORMAT (1H0,' USER SPECIFIED ',I3,' (NAS) SIGNIFICANT AREA ',SORAM24620
1URCES AS LISTED BY AREA SOURCE NUMBER: '/2X,25I5) RAM24630
2490 FORMAT (1X,T21,'THE ORDER OF SIGNIFICANCE (IMAS) FOR 10 OR LESS ',RAM24640
1' AREA SOURCE IS LISTED BY AREA SOURCE NUMBER: '/2X,10I5) RAM24650
2500 FORMAT (1H0,'SURFACE MET DATA FROM STATION(ISFCD) ',I6,' YEAR(ISFRAM24660
1CYR) 19',I2/2X,'MIXING HEIGHT DATA FROM STATION(IMXD) ',I6,' YEARRAM24670
2(IMXYR) 19',I2) RAM24680
2510 FORMAT (1H0,T21,'RECEPTOR INFORMATION') RAM24690
2520 FORMAT (1H0,'MPTER INTERNALLY GENERATES 36 RECEPTORS ',ON A CIRCRAM24700
1LE CORRESPONDING TO EACH NON-ZERO ',RADIAL DISTANCE FROM A CENTERRAM24710
2 POINT '/1X,T10,'COORDINATES ARE (USER UNITS): (' ,F8.3,' ,F8.3,')'RAM24720
3/1X,T10,'RADIAL DISTANCE(S) USER SPECIFIED (USER UNITS): ',5(F11.3RAM24730
4,' ,') RAM24740
2530 FORMAT (F4.1) RAM24750
2540 FORMAT ('0', RECEPTOR IDENTIFICATION EAST NORTH RAM24760
1'/1X,T30,'COORD',T39,'COORD'/1X,T31,'(USER UNITS)') RAM24770
2550 FORMAT (1X,T3,I3,1X,A1,8X,2A4,F13.3,F10.3) RAM24780
2560 FORMAT (/1X,' THE NUMBER OF DAYS PREVIOUSLY COMPLETED EQUAL ',RAM24790
1I3,' AND THE LAST DAY TO BE COMPLETED IN THIS RUN IS ',I3) RAM24800
2570 FORMAT ('INPUT MET DATA FOR ',I3,'-HR PERIOD STARTING AT HOUR: ',RAM24810
1I3,' YEAR',I3,' JULIAN DAY',I4/1X,T2,' HOUR THETA SPEED MIRAM24820
2XING TEMP STABILITY'/1X,T9,'(DEG) (M/S) HEIGHT(M) (DEG-KRAM24830
3) CLASS'/1X) RAM24840
2580 FORMAT (1X,T3,I2,4F9.2,6X,I1) RAM24850
2590 FORMAT ('0', 'RESULTANT MET CONDITIONS'//2X,'WIND DIRECTION=',F7.2,RAM24860
1T36,'RESULTANT WIND SPEED=',F7.2/2X,'AVERAGE WIND SPEED=',F7.2,T36RAM24870
2,'AVERAGE TEMP=',F7.2/2X,'WIND PERSISTENCE=',F6.3,T36,'MODAL STABIRAM24880
3LITY=',I2) RAM24890
2600 FORMAT ('0',T20,'GENERATED HONEYCOMB RECEPTORS'/1X,1X,'THE AREA TRAM24900
10 BE COVERED BY HONEYCOMB RECEPTORS IS BOUNDED BY: '/1X,' RMIN=',F1RAM24910
20.3,' RMAX=',F10.3,' SMIN=',F10.3,' SMAX=',F10.3/1X,'DISTANCE BETRAM24920
3WEEN HONEYCOMB RECEPTORS(GRIDSP) IN USER UNITS=',F7.3/1X,'RECEPTORAM24930
4R EAST NORTH') RAM24940

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2610 FORMAT (' PLEASE NOTE: THE RECEPTOR NUMBERS AND LOCATIONS GENERRAM24950
1ATED FOR THIS AVERAGING TIME PERIOD ARE DIFFERENT FROM THOSE GENERRAM24960
2ATED FOR',/18X,' THE PRECEEDING AVERAGING PERIOD. ') RAM24970
2620 FORMAT (1H0,' THIS SEGMENT OF A SEGMENTED RUN HAS COMPLETED',I5,' RAM24980
1(IDAY) DAYS. ') RAM24990
2630 FORMAT ('1',20A4/1X,20A4/1X,20A4) RAM25000
2640 FORMAT ('0',T9,' RECEPTORS'//1X,'RECEPTOR IDENTIFICATION RAM25010
1EAST NORTH ',T99,'AVGRAM25020
2 CONC FOR PERIOD',/1X,T30,'COORD',T39,'COORD
3 ',T94,'DAY',F4.0,'HR',F3.0,' TO DAY',F4.0,'HR',F3.0/1XRAM25040
4,T31,'(USER UNITS) ',T100,'RAM25050
5(MICROGRAMS/M**3)',/1X) RAM25060
2650 FORMAT (1X,T3,I3,1X,A1,I3,5X,2A4,5X,F8.2,2X,F8.2,T110,A1,6PF7.2) RAM25070
2660 FORMAT (1H1,T29,'FIVE HIGHEST ',I2,'-HOUR ',A4,' CONCENTRATIONS((ERAM25080
INDING ON JULIAN DAY, HOUR)',/1X,T55,'(MICROGRAMS/M**3)'//2X,'RECEPTRAM25090
2OR ',T38,4(I1,20X),I1,/1X) RAM25100
2661 FORMAT (1H1,T29,'FIVE HIGHEST ',I2,'-HOUR ',A4,' CONCENTRATIONS((ERAM25110
INDING ON JULIAN DAY, HOUR)',/1X,T55,'(MICROGRAMS/M**3)'//
21X,T36,'C-FLAG IDENTIFIES CONCENTRATIONS AFFECTED BY CALM HOURS'//RAM25130
32X,'RECEPTOR ',T38,4(I1,20X),I1,/1X) RAM25140
2670 FORMAT (1H,2X,I3,'( ',F7.2,' ',F7.2,' )',2(1X,A1,6PF9.2,A1,1X,'( ',IRAM25150
I3,' ',I2,' )',3(2X,6PF9.2,A1,1X,'( ',I3,' ',I2,' )',')) RAM25160
2680 FORMAT ('0 THIS RUN HAS TERMINATED NORMALLY. ') RAM25170
C RAM25180
END RAM25190

C
BLOCK DATA
C BLOCK DATA (VERSION 80336), PART OF RAM. RAM25210
C BLOCK DATA FOR RAM RAM25220
C COEFFICIENTS GENERATED WITH RURAL SIGMAS USING PGSYSZ &PGSZ RAM25230
C DIST OF MAX. CONC. FROM PT SOURCE = PXCOR(KST,IH)*H**PXEXR(KST,IH) RAM25240
C RELATIVE CONC. NORMALIZED FOR WIND SPEED FROM PT SOURCE, CHI*U/Q, = RAM25250
C PXUCOR(KST,IH)*H**PXUEXR(KST,IH) RAM25260
C DISTANCE OF MAX. CONC. FROM DOWNWIND EDGE OF AREA SOURCE = RAM25270
C AXCOR(KST,IH)*H**AXEXR(KST,IH) RAM25280
C IH=1 FOR H LESS THAN 20 METERS. RAM25290
C IH=2 FOR H FROM 20 TO 30 METERS. RAM25300
C IH=3 FOR H FROM 30 TO 50 METERS. RAM25310
C IH=4 FOR H FROM 50 TO 70 METERS. RAM25320
C IH=5 FOR H FROM 70 TO 100 METERS. RAM25330
C IH=6 FOR H FROM 100 TO 200 METERS. RAM25340
C IH=7 FOR H FROM 200 TO 300 METERS. RAM25350
C IH=8 FOR H FROM 300 TO 500 METERS. RAM25360
C IH=9 FOR H GREATER THAN 500 METERS. RAM25370
C RAM25380
C COMMON /AE/ HC1(10),PXUCOR(6,9),PXUEXR(6,9),PXCOR(6,9),PXEXR(6,9),RAM25390
1PXUCOF(6,9),PXUEXP(6,9),PXCOF(6,9),PXEXP(6,9),AXCOR(6,9),AXEXR(6,9),RAM25400
2),AXCOF(6,9),AXEXP(6,9) RAM25410
C RAM25420
DATA HC1 /10.,20.,30.,50.,70.,100.,200.,300.,500.,1000./ RAM25430
DATA PXCOR /.38964E-02,.54607E-02,.75278E-02,.11563E-01,.12743E-01RAM25440
1,.21051E-01,.59088E-02,.50774E-02,.74442E-02,.87095E-02,.10152E-01RAM25450
2,.10867E-01,.59366E-02,.67049E-02,.76095E-02,.14437E-01,.79376E-02RAM25460
3,.10552E-01,.10739E-01,.67199E-02,.75237E-02,.22618E-02,.38170E-02RAM25470
4,.13053E-02,.14425E-01,.10509E-01,.75283E-02,.22489E-02,.24006E-02RAM25480
5,.79956E-03,.7139E-01,.10418E-01,.75363E-02,.17287E-02,.15400E-02RAM25490
6,.14422E-03,.51107E-01,.10468E-01,.75324E-02,.12670E-02,.13842E-03RAM25500
7,.43952E-09,.50921E-01,.10472E-01,.75225E-02,.84890E-03,.10930E-06RAM25510
8,.13979E-02,.50996E-01,.10401E-01,.74961E-02,.19441E-03,.10859E-04RAM25520
9,.20000E+04/ RAM25530
DATA PXEXR /.10995E+01,.10757E+01,.10965E+01,.11383E+01,.12469E+01RAM25540
1,.12577E+01,.96054E+00,.11000E+01,.11002E+01,.12329E+01,.13228E+01RAM25550
2,.14784E+01,.95916E+00,.10182E+01,.10937E+01,.10843E+01,.13951E+01RAM25560
3,.14870E+01,.80763E+00,.10176E+01,.10966E+01,.15582E+01,.15823E+01RAM25570
4,.20212E+01,.73818E+00,.91238E+00,.10965E+01,.15595E+01,.16914E+01RAM25580
5,.21366E+01,.53282E+00,.91427E+00,.10963E+01,.16166E+01,.17878E+01RAM25590
6,.25085E+01,.47257E+00,.91337E+00,.10964E+01,.16753E+01,.22426E+01RAM25600
7,.49057E+01,.47321E+00,.91331E+00,.10966E+01,.17455E+01,.34951E+01RAM25610
8,.22807E+01,.47297E+00,.91440E+00,.10971E+01,.19827E+01,.27551E+01RAM25620
9,.00000E+00/ RAM25630
RAM25640

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DATA PXUCOR /.10401E+00,.12133E+00,.14273E+00,.15351E+00,.18855E+0RAM25650
10,.18668E+00,.77533E-01,.11728E+00,.14120E+00,.18239E+00,.20458E+0RAM25660
20,.34326E+00,.67228E-01,.10013E+00,.13963E+00,.19162E+00,.38998E+0RAM25670
30,.76271E+00,.40484E-01,.75308E-01,.13784E+00,.54357E+00,.72550E+0RAM25680
40,.22936E+01,.28539E-01,.66936E-01,.13615E+00,.52790E+00,.12908E+0RAM25690
51,.56943E+01,.14792E-01,.65799E-01,.13315E+00,.74832E+00,.28818E+0RAM25700
61,.40940E+03,.12403E-01,.64321E-01,.12927E+00,.10826E+01,.77020E+0RAM25710
72,.23011E+05,.12340E-01,.62874E-01,.12546E+00,.15580E+01,.68810E+0RAM25720
83,.46522E+06,.12245E-01,.60615E-01,.11952E+00,.22517E+01,.42842E+0RAM25730
93,.00000E+00/RAM25740
DATA PXUEXR /-.19460E+01,-.19774E+01,-.20086E+01,-.20742E+01,-.218RAM25750
122E+01,-.22176E+01,-.18479E+01,-.19661E+01,-.20050E+01,-.21317E+01RAM25760
2,-.22094E+01,-.24209E+01,-.18060E+01,-.19196E+01,-.20017E+01,-.214RAM25770
362E+01,-.23991E+01,-.26556E+01,-.16763E+01,-.18468E+01,-.19984E+01RAM25780
4,-.24128E+01,-.25578E+01,-.29371E+01,-.15940E+01,-.18191E+01,-.199RAM25790
555E+01,-.24059E+01,-.26934E+01,-.31511E+01,-.14513E+01,-.18153E+01RAM25800
6,-.19907E+01,-.24817E+01,-.28678E+01,-.40795E+01,-.14181E+01,-.181RAM25810
711E+01,-.19851E+01,-.25514E+01,-.34879E+01,-.48399E+01,-.14172E+01RAM25820
8,-.18071E+01,-.19799E+01,-.26152E+01,-.38719E+01,-.53670E+01,-.141RAM25830
960E+01,-.18012E+01,-.19721E+01,-.26744E+01,-.37956E+01,-.17020E+02RAM25840
A/RAM25850
DATA AXCOR /.68365E-02,.79134E-02,.11062E-01,.14818E-01,.17234E-01RAM25860
1,.19793E-01,.92054E-02,.94211E-02,.11254E-01,.13875E-01,.91114E-02RAM25870
2,.65416E-02,.12311E-01,.11151E-01,.11079E-01,.53876E-02,.48999E-02RAM25880
3,.17087E-02,.19297E-01,.13824E-01,.11267E-01,.42195E-02,.17526E-02RAM25890
4,.13715E-03,.32619E-01,.13833E-01,.11119E-01,.30122E-02,.11144E-02RAM25900
5,.73510E-06,.53524E-01,.13821E-01,.11115E-01,.22334E-02,.20868E-04RAM25910
6,.28987E-05,.55881E-01,.13920E-01,.11152E-01,.11204E-02,.21361E-05RAM25920
7,.20000E+04,.55160E-01,.13838E-01,.11153E-01,.61078E-03,.10114E-03RAM25930
8,.20000E+04,.55799E-01,.13881E-01,.11140E-01,.61554E-03,.20000E+04RAM25940
9,.20000E+04/RAM25950
DATA AXEXR /.10103E+01,.10748E+01,.10960E+01,.12112E+01,.13211E+01RAM25960
1,.14994E+01,.91095E+00,.10166E+01,.10903E+01,.12332E+01,.15339E+01RAM25970
2,.18689E+01,.82547E+00,.96699E+00,.10949E+01,.15113E+01,.17163E+01RAM25980
3,.22636E+01,.71059E+00,.91206E+00,.10906E+01,.15738E+01,.19791E+01RAM25990
4,.29084E+01,.58703E+00,.91191E+00,.10937E+01,.16531E+01,.20856E+01RAM26000
5,.41392E+01,.47949E+00,.91210E+00,.10938E+01,.17181E+01,.29494E+01RAM26010
6,.38412E+01,.47136E+00,.91075E+00,.10932E+01,.18483E+01,.33796E+01RAM26020
7,.00000E+00,.47363E+00,.91178E+00,.10932E+01,.19546E+01,.27033E+01RAM26030
8,.00000E+00,.47178E+00,.91129E+00,.10933E+01,.19534E+01,.00000E+00RAM26040
9,.00000E+00/RAM26050
C COEFFICIENTS GENERATED WITH URBAN SIGMAS USING BRYSZ & BRZ RAM26060
C DIST OF MAX. CONC. FROM PT SOURCE = PXCOF(KST,IH)*H**PXEXP(KST,IH) RAM26070
C RELATIVE CONC. NORMALIZED FOR WIND SPEED FROM PT SOURCE, CHI*U/Q, = RAM26080
C PXUCOF(KST,IH)*H**PXUEXP(KST,IH) RAM26090
C DISTANCE OF MAX. CONC. FROM DOWNWIND EDGE OF AREA SOURCE = RAM26100
C AXCOF(KST,IH)*H**AXEXP(KST,IH) RAM26110
C IH=1 FOR H LESS THAN 20 METERS. RAM26120
C IH=2 FOR H FROM 20 TO 30 METERS. RAM26130
C IH=3 FOR H FROM 30 TO 50 METERS. RAM26140
C IH=4 FOR H FROM 50 TO 70 METERS. RAM26150
C IH=5 FOR H FROM 70 TO 100 METERS. RAM26160
C IH=6 FOR H FROM 100 TO 200 METERS. RAM26170
C IH=7 FOR H FROM 200 TO 300 METERS. RAM26180
C IH=8 FOR H FROM 300 TO 500 METERS. RAM26190
C IH=9 FOR H GREATER THAN 500 METERS. RAM26200
C RAM26210
C RAM26220
DATA PXCOF /.29000E-02,.29000E-02,.33389E-02,.49374E-02,.76841E-02RAM26230
1,.76841E-02,.31586E-02,.31586E-02,.34293E-02,.50285E-02,.65931E-02RAM26240
2,.65931E-02,.31977E-02,.31977E-02,.36114E-02,.45861E-02,.51435E-02RAM26250
3,.51435E-02,.34513E-02,.34513E-02,.34298E-02,.43860E-02,.33140E-02RAM26260
4,.33140E-02,.36196E-02,.36196E-02,.33575E-02,.39506E-02,.19672E-02RAM26270
5,.19672E-02,.41677E-02,.41677E-02,.32748E-02,.32439E-02,.63291E-03RAM26280
6,.63291E-03,.50465E-02,.50465E-02,.31556E-02,.21446E-02,.19145E-03RAM26290
7,.19145E-03,.60289E-02,.60289E-02,.30537E-02,.12214E-02,.12483E-03RAM26300
8,.12483E-03,.77521E-02,.77521E-02,.29817E-02,.39130E-03,.11337E-03RAM26310
9,.11337E-03/RAM26320
DATA PXEXP /.10000E+01,.10000E+01,.10205E+01,.10141E+01,.10829E+01RAM26330
1,.10829E+01,.97149E+00,.97149E+00,.10116E+01,.10080E+01,.11340E+01RAM26340


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2,.11340E+01,.96787E+00,.96787E+00,.99634E+00,.10350E+01,.12070E+01RAM26350
3,.12070E+01,.94836E+00,.94836E+00,.10095E+01,.10465E+01,.13194E+01RAM26360
4,.13194E+01,.93716E+00,.93716E+00,.10145E+01,.10711E+01,.14421E+01RAM26370
5,.14421E+01,.90654E+00,.90654E+00,.10200E+01,.11139E+01,.16884E+01RAM26380
6,.16884E+01,.87043E+00,.87043E+00,.10270E+01,.11920E+01,.19141E+01RAM26390
7,.19141E+01,.83924E+00,.83924E+00,.10327E+01,.12907E+01,.19890E+01RAM26400
8,.19890E+01,.79879E+00,.79879E+00,.10365E+01,.14738E+01,.20045E+01RAM26410
9,.20045E+01/
DATA PXUCOF / .16808E+00,.16808E+00,.20927E+00,.20378E+00,.18861E+00RAM26420
10,.18861E+00,.15945E+00,.15945E+00,.20527E+00,.20229E+00,.21253E+00RAM26430
20,.21253E+00,.14777E+00,.14777E+00,.19871E+00,.20011E+00,.24888E+00RAM26440
30,.24888E+00,.13262E+00,.13262E+00,.18908E+00,.19685E+00,.30041E+00RAM26450
40,.30041E+00,.11745E+00,.11745E+00,.17767E+00,.19301E+00,.34521E+00RAM26460
50,.34521E+00,.91943E-01,.91943E-01,.15327E+00,.18499E+00,.34368E+00RAM26470
60,.34368E+00,.65533E-01,.65533E-01,.11984E+00,.17445E+00,.23640E+00RAM26480
70,.23640E+00,.47345E-01,.47345E-01,.89821E-01,.16720E+00,.15537E+00RAM26490
80,.15537E+00,.29993E-01,.29993E-01,.56100E-01,.16747E+00,.11009E+00RAM26500
90,.11009E+00/
DATA PXUEXP / -.19722E+01,-.19722E+01,-.19896E+01,-.19965E+01,-.206RAM26510
149E+01,-.20649E+01,-.19546E+01,-.19546E+01,-.19831E+01,-.19940E+01RAM26520
2,-.21047E+01,-.21047E+01,-.19322E+01,-.19322E+01,-.19736E+01,-.199RAM26530
308E+01,-.21512E+01,-.21512E+01,-.19045E+01,-.19045E+01,-.19609E+01RAM26540
4,-.19867E+01,-.21993E+01,-.21993E+01,-.18759E+01,-.18759E+01,-.194RAM26550
562E+01,-.19820E+01,-.22320E+01,-.22320E+01,-.18228E+01,-.18228E+01RAM26560
6,-.19142E+01,-.19728E+01,-.22310E+01,-.22310E+01,-.17589E+01,-.175RAM26570
789E+01,-.18677E+01,-.19617E+01,-.21604E+01,-.21604E+01,-.17019E+01RAM26580
8,-.17019E+01,-.18172E+01,-.19543E+01,-.20868E+01,-.20868E+01,-.162RAM26590
984E+01,-.16284E+01,-.17414E+01,-.19545E+01,-.20314E+01,-.20314E+01RAM26600
A/
DATA AXCOF / .44505E-02,.44505E-02,.50000E-02,.68776E-02,.10026E-01RAM26610
1,.10026E-01,.45289E-02,.45289E-02,.50000E-02,.68258E-02,.76276E-02RAM26620
2,.76276E-02,.47786E-02,.47786E-02,.50000E-02,.63099E-02,.51380E-02RAM26630
3,.51380E-02,.52938E-02,.52938E-02,.50000E-02,.59067E-02,.29303E-02RAM26640
4,.29303E-02,.57593E-02,.57593E-02,.50000E-02,.52626E-02,.16889E-02RAM26650
5,.16889E-02,.68765E-02,.68765E-02,.50000E-02,.39429E-02,.74769E-03RAM26660
6,.74769E-03,.82988E-02,.82988E-02,.50000E-02,.22800E-02,.39161E-03RAM26670
7,.39161E-03,.99556E-02,.99556E-02,.50000E-02,.10882E-02,.29900E-03RAM26680
8,.29900E-03,.12206E-01,.12206E-01,.50000E-02,.28165E-03,.25538E-03RAM26690
9,.25538E-03/
DATA AXEXP / .96437E+00,.96437E+00,.10000E+01,.10199E+01,.11356E+01RAM26700
1,.11356E+01,.95855E+00,.95855E+00,.10000E+01,.10224E+01,.12269E+01RAM26710
2,.12269E+01,.94276E+00,.94276E+00,.10000E+01,.10455E+01,.13430E+01RAM26720
3,.13430E+01,.91659E+00,.91659E+00,.10000E+01,.10624E+01,.14866E+01RAM26730
4,.14866E+01,.89676E+00,.89676E+00,.10000E+01,.10896E+01,.16163E+01RAM26740
5,.16163E+01,.85826E+00,.85826E+00,.10000E+01,.11523E+01,.17932E+01RAM26750
6,.17932E+01,.82277E+00,.82277E+00,.10000E+01,.12557E+01,.19153E+01RAM26760
7,.19153E+01,.79086E+00,.79086E+00,.10000E+01,.13853E+01,.19626E+01RAM26770
8,.19626E+01,.75807E+00,.75807E+00,.10000E+01,.16028E+01,.19880E+01RAM26780
9,.19880E+01/
C
END
C
FUNCTION ANGARC(DELM,DELN)
C      FUNCTION ANGARC (VERSION 80336), PART OF RAM.
C      THIS SUBROUTINE IS REFERRED TO AS B IN THE COMMON STATEMENTS
C      DETERMINES APPROPRIATE ANGLE OF TAN(ANG) = DELM/DELN
C      WHICH IS REQUIRED FOR CALCULATION OF RESULTANT WIND DIRECTION.
C      DELM IS THE AVERAGE WIND COMPONENT IN THE EAST DIRECTION.
C      DELN IS THE AVERAGE WIND COMPONENT IN THE NORTH DIRECTION.
C      USES LIBRARY FUNCTION ATAN
C
10  IF (DELM) 10,40,80
20  IF (DELN) 20,30,20
    ANGARC=57.29578*ATAN(DELM/DELN)+180.
    RETURN
30  ANGARC=180.
    RETURN
40  IF (DELM) 50,60,70
50  ANGARC=270.
    RETURN
RAM26870
RAM26880
RAM26890
RAM26900
RAM26910
RAM26920
RAM26930
RAM26940
RAM26950
RAM26960
RAM26970
RAM26980
RAM26990
RAM27000
RAM27010
RAM27020
RAM27030
RAM27040

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60	ANGARC=0.	RAM27050
C	ANGARC=0. INDICATES INDETERMINATE ANGLE	RAM27060
	RETURN	RAM27070
70	ANGARC=090.	RAM27080
	RETURN	RAM27090
80	IF (DELM) 90,100,110	RAM27100
90	ANGARC=57.29578*ATAN(DELM/DELN)+360.	RAM27110
	RETURN	RAM27120
100	ANGARC=360.	RAM27130
	RETURN	RAM27140
110	ANGARC=57.29578*ATAN(DELM/DELN)	RAM27150
	RETURN	RAM27160
C	END	RAM27170
C		RAM27180
	SUBROUTINE SYSZ	RAM27200
C	SUBROUTINE SYSZ (VERSION 80336), PART OF RAM.	RAM27210
C	THIS SUBROUTINE REFERRED TO AS C IN THE COMMON STATEMENTS	RAM27220
C		RAM27230
	COMMON /AMOST/ DELH,FH,HINT(3),H,HL,IO,IOPT(50),KST,MUOR,NHTS,RC,RRAM27240	
	ICZ,SY,SZ,TEMP,TLOS,UPL,X,Y,Z	RAM27250
	DIMENSION XA(7),XB(2),XD(5),XE(8),XF(9),AA(8),BA(8),AB(3),	RAM27260
	1BB(3),AD(6),BD(6),AE(9),BE(9),AF(10),BF(10)	RAM27270
	DATA XA /5.,4.,3.,25.,2.,15.,1/	RAM27280
	DATA XB /4.,2/	RAM27290
	DATA XD /30.,10.,3.,1.,3/	RAM27300
	DATA XE /40.,20.,10.,4.,2.,1.,3.,1/	RAM27310
	DATA XF /60.,30.,15.,7.,3.,2.,1.,7.,2/	RAM27320
	DATA AA /453.85,346.75,258.89,217.41,179.52,170.22,158.08,122.8/	RAM27330
	DATA BA /2.1166,1.7283,1.4094,1.2644,1.1262,1.0932,1.0542,.9447/	RAM27340
	DATA AB /109.30,98.483,90.673/	RAM27350
	DATA BB /1.0971,0.98332,0.93198/	RAM27360
	DATA AD /44.053,36.650,33.504,32.093,32.093,34.459/	RAM27370
	DATA BD /0.51179,0.56589,0.60486,0.64403,0.81066,0.86974/	RAM27380
	DATA AE /47.618,35.420,26.970,24.703,22.534,21.628,21.628,23.331,2RAM27390	
	14.26/	RAM27400
	DATA BE /0.29592,0.37615,0.46713,0.50527,0.57154,0.63077,0.75660,0RAM27410	
	1.81956,0.8366/	RAM27420
	DATA AF /34.219,27.074,22.651,17.836,16.187,14.823,13.953,13.953,1RAM27430	
	14.457,15.209/	RAM27440
	DATA BF /0.21716,0.27436,0.32681,0.41507,0.46490,0.54503,0.63227,0RAM27450	
	1.68465,0.78407,0.81558/	RAM27460
C	ASSIGN 10 TO K	RAM27470
	IF (MUOR.EQ.2) ASSIGN 70 TO K	RAM27480
	RETURN	RAM27490
C		RAM27500
	ENTRY SYZ	RAM27510
	GO TO K, (10,70)	RAM27520
C		RAM27530
C	MCELROY-POOLER URBAN DISPERSION PARAMETERS FROM ST. LOUIS	RAM27540
C	EXPERIMENT AS PUT IN EQUATION FORM BY BRIGGS.	RAM27550
C	XK IS DISTANCE IN KM.	RAM27560
C	KST IS PASQUILL STABILITY CLASS.	RAM27570
C	SY AND SZ ARE IN METERS.	RAM27580
C	CONVERT X TO METERS	RAM27590
10	XM=1000.*X	RAM27600
	GO TO (20,20,30,40,50,50), KST	RAM27610
20	SY=0.32*XM/SQRT(1.+0.0004*XM)	RAM27620
	SZ=0.24*XM/SQRT(1.+0.001*XM)	RAM27630
	GO TO 60	RAM27640
30	SY=0.22*XM/SQRT(1.+0.0004*XM)	RAM27650
	SZ=0.2*XM	RAM27660
	GO TO 60	RAM27670
40	SY=0.16*XM/SQRT(1.+0.0004*XM)	RAM27680
	SZ=0.14*XM/SQRT(1.+0.0003*XM)	RAM27690
	GO TO 60	RAM27700
50	SY=0.11*XM/SQRT(1.+0.0004*XM)	RAM27710
	SZ=0.08*XM/SQRT(1.+0.0015*XM)	RAM27720
60	IF (SZ.GT.5000.) SZ=5000.	RAM27730
	RETURN	RAM27740

C		RAM27750
C	PASQUILL-GIFFORD PARAMETERS VALID FOR RURAL CONDITIONS.	RAM27760
C	VERTICAL DISPERSION PARAMETER VALUE, SZ DETERMINED BY	RAM27770
C	SZ = A * X ** B WHERE A AND B ARE FUNCTIONS OF BOTH STABILITY	RAM27780
C	AND RANGE OF X.	RAM27790
C	HORIZONTAL DISPERSION PARAMETER VALUE, SY DETERMINED BY	RAM27800
C	LOGARITHMIC INTERPOLATION OF PLUME HALF-ANGLE ACCORDING TO	RAM27810
C	DISTANCE AND CALCULATION OF 1/2.15 TIMES HALF-ARC LENGTH.	RAM27820
70	GO TO (80,110,140,150,180,210), KST	RAM27830
C	STABILITY A	RAM27840
80	TH=(24.167-2.5334*ALOG(X))/57.2958	RAM27850
	IF (X.GT.3.11) GO TO 240	RAM27860
	DO 90 ID=1,7	RAM27870
	IF (X.GE.XA(ID)) GO TO 100	RAM27880
90	CONTINUE	RAM27890
	ID=8	RAM27900
100	SZ=AA(ID)*X**BA(ID)	RAM27910
	GO TO 260	RAM27920
C	STABILITY B	RAM27930
110	TH=(18.333-1.8096*ALOG(X))/57.2958	RAM27940
	IF (X.GT.35.) GO TO 240	RAM27950
	DO 120 ID=1,2	RAM27960
	IF (X.GE.XB(ID)) GO TO 130	RAM27970
120	CONTINUE	RAM27980
	ID=3	RAM27990
130	SZ=AB(ID)*X**BB(ID)	RAM28000
	GO TO 250	RAM28010
C	STABILITY C	RAM28020
140	TH=(12.5-1.0857*ALOG(X))/57.2958	RAM28030
	SZ=51.141*X**0.91465	RAM28040
	GO TO 250	RAM28050
C	STABILITY D	RAM28060
150	TH=(8.3333-0.72382*ALOG(X))/57.2958	RAM28070
	DO 160 ID=1,5	RAM28080
	IF (X.GE.XD(ID)) GO TO 170	RAM28090
160	CONTINUE	RAM28100
	ID=6	RAM28110
170	SZ=AD(ID)*X**BD(ID)	RAM28120
	GO TO 250	RAM28130
C	STABILITY E	RAM28140
180	TH=(6.25-0.54287*ALOG(X))/57.2958	RAM28150
	DO 190 ID=1,8	RAM28160
	IF (X.GE.XE(ID)) GO TO 200	RAM28170
190	CONTINUE	RAM28180
	ID=9	RAM28190
200	SZ=AE(ID)*X**BE(ID)	RAM28200
	GO TO 250	RAM28210
C	STABILITY F	RAM28220
210	TH=(4.1667-0.36191*ALOG(X))/57.2958	RAM28230
	DO 220 ID=1,9	RAM28240
	IF (X.GE.XF(ID)) GO TO 230	RAM28250
220	CONTINUE	RAM28260
	ID=10	RAM28270
230	SZ=AF(ID)*X**BF(ID)	RAM28280
	GO TO 250	RAM28290
240	SZ=5000.	RAM28300
	GO TO 260	RAM28310
250	IF (SZ.GT.5000.) SZ=5000.	RAM28320
260	SY=465.116*X*SIN(TH)/COS(TH)	RAM28330
C	465.116 = 1000. (M/KM) / 2.15	RAM28340
	RETURN	RAM28350
C		RAM28360
	END	RAM28370
C		
C	SUBROUTINE SGZ	RAM28390
C	SUBROUTINE SGZ (VERSION 81352), PART OF RAM.	RAM28400
C	THIS SUBROUTINE IS REFERRED TO AS D IN THE COMMON STATEMENTS	RAM28410
C		RAM28420
	COMMON /AMOST/ DELH, FH, HINT(3), H, HL, IO, IOPT(50), KST, MUOR, NHTS, RC,	RAM28430
	ICZ, SY, SZ, TEMP, TLOS, UPL, X, Y, Z	RAM28440

	DIMENSION XA(7), XB(2), XD(5), XE(8), XF(9), AA(8), BA(8), AB(3),	RAM28450
	1BB(3), AD(6), BD(6), AE(9), BE(9), AF(10), BF(10)	RAM28460
	DATA XA /5.,4.,3.,25.,2.,15.,1/	RAM28470
	DATA XB /4.,2/	RAM28480
	DATA XD /30.,10.,3.,1.,3/	RAM28490
	DATA XE /40.,20.,10.,4.,2.,1.,3.,1/	RAM28500
	DATA XF /60.,30.,15.,7.,3.,2.,1.,7.,2/	RAM28510
	DATA AA /453.85,346.75,258.89,217.41,179.52,170.22,158.08,122.8/	RAM28520
	DATA BA /2.1166,1.7283,1.4094,1.2644,1.1262,1.0932,1.0542,.9447/	RAM28530
	DATA AB /109.30,98.483,90.673/	RAM28540
	DATA BB /1.0971,0.98332,0.93198/	RAM28550
	DATA AD /44.053,36.650,33.504,32.093,32.093,34.459/	RAM28560
	DATA BD /0.51179,0.56589,0.60486,0.64403,0.81066,0.86974/	RAM28570
	DATA AE /47.618,35.420,26.970,24.703,22.534,21.628,21.628,23.331,214.26/	RAM28580
	DATA BE /0.29592,0.37615,0.46713,0.50527,0.57154,0.63077,0.75660,0.81956,0.8366/	RAM28590
	DATA AF /34.219,27.074,22.651,17.836,16.187,14.823,13.953,13.953,14.457,15.209/	RAM28600
	DATA BF /0.21716,0.27436,0.32681,0.41507,0.46490,0.54503,0.63227,0.68465,0.78407,0.81558/	RAM28610
C	ASSIGN 10 TO K	RAM28620
	IF (MUOR.EQ.2) ASSIGN 70 TO K	RAM28630
	RETURN	RAM28640
C	ENTRY SIGZ	RAM28650
	GO TO K, (10,70)	RAM28660
C	MCELROY-POOLER URBAN SIGMA Z.	RAM28670
C	XM IS DISTANCE IN KM.	RAM28680
C	KST IS PASQUILL STABILITY CLASS.	RAM28690
C	SZ IS IN METERS.	RAM28700
C	CONVERT X TO METERS	RAM28710
10	XM=1000.*X	RAM28720
	GO TO (20,20,30,40,50,50), KST	RAM28730
20	SZ=0.24*XM*SQRT(1.+0.001*XM)	RAM28740
	GO TO 60	RAM28750
30	SZ=0.2*XM	RAM28760
	GO TO 60	RAM28770
40	SZ=0.14*XM/SQRT(1.+0.0003*XM)	RAM28780
	GO TO 60	RAM28790
50	SZ=0.08*XM/SQRT(1.+0.0015*XM)	RAM28800
60	IF (SZ.GT.5000.) SZ=5000.	RAM28810
	RETURN	RAM28820
C	PASQUILL-GIFFORD PARAMETER VALID FOR RURAL CONDITIONS.	RAM28830
C	VERTICAL DISPERSION PARAMETER VALUE, SZ DETERMINED BY	RAM28840
C	SZ = A * X ** B WHERE A AND B ARE FUNCTIONS OF BOTH STABILITY	RAM28850
C	AND RANGE OF X.	RAM28860
70	GO TO (80,110,140,150,180,210), KST	RAM28870
C	STABILITY A (10)	RAM28880
80	IF (X.GT.3.11) GO TO 240	RAM28890
	DO 90 ID=1,7	RAM28900
	IF (X.GE.XA(ID)) GO TO 100	RAM28910
90	CONTINUE	RAM28920
	ID=8	RAM28930
100	SZ=AA(ID)*X**BA(ID)	RAM28940
	GO TO 260	RAM28950
C	STABILITY B (20)	RAM28960
110	IF (X.GT.35.) GO TO 240	RAM28970
	DO 120 ID=1,2	RAM28980
	IF (X.GE.XB(ID)) GO TO 130	RAM28990
120	CONTINUE	RAM29000
	ID=3	RAM29010
130	SZ=AB(ID)*X**BB(ID)	RAM29020
	GO TO 250	RAM29030
C	STABILITY C (30)	RAM29040
140	SZ=61.141*X**0.91465	RAM29050
	GO TO 250	RAM29060
C	STABILITY D (40)	RAM29070
150	DO 160 ID=1,5	RAM29080
		RAM29090
		RAM29100
		RAM29110
		RAM29120
		RAM29130
		RAM29140

160	IF (X.GE.XD(ID)) GO TO 170	RAM29150
	CONTINUE	RAM29160
	ID=6	RAM29170
170	SZ=AD(ID)*X**BD(ID)	RAM29180
	GO TO 250	RAM29190
C	STABILITY E (50)	RAM29200
180	DO 190 ID=1,8	RAM29210
	IF (X.GE.XE(ID)) GO TO 200	RAM29220
190	CONTINUE	RAM29230
	ID=9	RAM29240
200	SZ=AE(ID)*X**BE(ID)	RAM29250
	GO TO 250	RAM29260
C	STABILITY F (60)	RAM29270
210	DO 220 ID=1,9	RAM29280
	IF (X.GE.XF(ID)) GO TO 230	RAM29290
220	CONTINUE	RAM29300
	ID=10	RAM29310
230	SZ=AF(ID)*X**BF(ID)	RAM29320
	GO TO 250	RAM29330
240	SZ=5000.	RAM29340
	RETURN	RAM29350
250	IF (SZ.GT.5000.) SZ=5000.	RAM29360
260	RETURN	RAM29370
C		RAM29380
	END	RAM29390
C		
	SUBROUTINE JMHREC	RAM29410
C		RAM29420
	SUBROUTINE JMHREC (VERSION 80336), PART OF RAM.	RAM29430
C	THIS SUBROUTINE IS REFERRED TO AS E IN THE COMMON STATEMENTS	RAM29440
C	THE PURPOSE OF THIS SUBROUTINE IS TO DETERMINE RECEPTORS FROM	RAM29450
C	SIGNIFICANT SOURCES.	RAM29460
	COMMON /AMOST/ DELH,FH,HINT(3),H,HL,IO,IOPT(50),KST,MUOR,NHTS,RC,	RAM29470
	ICZ,SY,SZ,TEMP,TLOS,UPL,X,Y,Z	RAM29480
	COMMON /AE/ HCL(10),PXUCOR(6,9),PXUEXR(6,9),PXCOR(6,9),PXEXR(6,9),	RAM29490
	IPXUCOF(6,9),PXUEXP(6,9),PXCOF(6,9),PXEXP(6,9),AXCOR(6,9),AXEXR(6,	RAM29500
	2),AXCOF(6,9),AXEXP(6,9)	RAM29510
	COMMON /AEFM/ ITYPE(180),ICODE(180),UNITS,RREU(180),SREU(180)	RAM29520
	COMMON /AEFGKM/ NRECEP,RREC(180),SREC(180),IDATE(2),LH,NPT	RAM29530
	COMMON /AEG/ SOURCE(9,250)	RAM29540
	COMMON /AEGIKM/ IPOL,CONTWO,SINT,COST,U,HANE,PL(6)	RAM29550
	COMMON /AEK/ ASORC(6,100)	RAM29560
	COMMON /AEM/ NSIGP,MPS(25),NSIGA,MAS(10)	RAM29570
	DATA ICHAR /'P'/' ,JCHAR /'A'/'	RAM29580
C		RAM29590
	ASSIGN 120 TO KNTRL	RAM29600
	ASSIGN 190 TO KNTRM	RAM29610
	IF (MUOR.EQ.1) GO TO 10	RAM29620
	ASSIGN 110 TO KNTRL	RAM29630
10	ASSIGN 180 TO KNTRM	RAM29640
C	RETURN	RAM29650
		RAM29660
	ENTRY GREC	RAM29670
	IF (NSIGP.EQ.0) GO TO 150	RAM29680
	IF (IOPT(15).EQ.0) GO TO 150	RAM29690
	WRITE (IO,270)	RAM29700
C		RAM29710
	LOOP ON SIGNIFICANT POINT SOURCES	RAM29720
C		RAM29730
	DO 140 IP=1,NSIGP	RAM29740
	X=0.0	RAM29750
	I=MPS(IP)	RAM29760
C	EAST AND NORTH COORDINATES OF THE SOURCE (INTERNAL UNITS)	RAM29770
	RS=SOURCE(1,I)	RAM29780
	SS=SOURCE(2,I)	RAM29790
	Q=SOURCE(IPOL,I)	RAM29800
C	MODIFY WIND SPEED BY POWER LAW PROFILE IN ORDER TO TAKE INTO	RAM29810
C	ACCOUNT THE INCREASE IN WIND SPEED WITH HEIGHT.	RAM29820
	UPL=U*(SOURCE(5,I)/HANE)**PL(KST)	RAM29830
C	CALCULATE BUOYANCY PLUME RISE	RAM29840

	TS=SOURCE(6,I)	RAM29850
	IF (TS.GT.TEMP) GO TO 20	RAM29860
	HF=SOURCE(5,I)	RAM29870
	GO TO 80	RAM29880
20	F=SOURCE(9,I)*(TS-TEMP)/TS	RAM29890
	GO TO (30,30,30,30,50,60), KST	RAM29900
30	IF (F.GE.55.) GO TO 40	RAM29910
	HF=SOURCE(5,I)+21.425*F**0.75/UPL	RAM29920
	GO TO 80	RAM29930
40	HF=SOURCE(5,I)+38.71*F**0.6/UPL	RAM29940
	GO TO 80	RAM29950
50	DTHDZ=0.02	RAM29960
	GO TO 70	RAM29970
60	DTHDZ=0.035	RAM29980
70	S=9.80616*DTHDZ/TEMP	RAM29990
	HF=SOURCE(5,I)+2.6*(F/(UPL*S))**0.33333	RAM30000
C	DETERMINE PROPER HEIGHT CLASS	RAM30010
80	DO 90 IH=2,10	RAM30020
	IF (HF.LT.(HCL(IH)-.01)) GO TO 100	RAM30030
90	CONTINUE	RAM30040
	IH=10	RAM30050
100	IS=IH-1	RAM30060
	GO TO KNTRL, (110,120)	RAM30070
110	A=PXUCOR(KST,IS)	RAM30080
	B=PXUEXR(KST,IS)	RAM30090
	C=PXCOR(KST,IS)	RAM30100
	D=PXEXR(KST,IS)	RAM30110
	GO TO 130	RAM30120
120	A=PXUCOF(KST,IS)	RAM30130
	B=PXUEXP(KST,IS)	RAM30140
	C=PXCOF(KST,IS)	RAM30150
	D=PXEXP(KST,IS)	RAM30160
C	CALCULATE RELATIVE CONC. NORMALIZED FOR WIND SPEED	RAM30170
130	CONM=A*HF**B*Q/UPL	RAM30180
C	CALCULATE DISTANCE TO MAX. CONC. FROM POINT SOURCE.	RAM30190
C	X IN KM.	RAM30200
	X=C*HF**D	RAM30210
C	DO NOT ALLOW RECEPTORS BEYOND 1000 KM.	RAM30220
	IF (X.GT.1000.) GO TO 140	RAM30230
	NRECEP=NRECEP+2	RAM30240
	IF (NRECEP.GT.180) GO TO 260	RAM30250
C		RAM30260
C	TWO RECEPTORS ARE GENERATED FOR EACH SIGNIFICANT POINT SOURCE.	RAM30270
C	RECEPTORS ARE LOCATED AT A DISTANCE OF X AND AT 2X. X	RAM30280
C	IS THE LOCATION WHERE THE HIGHEST CONCENTRATION FROM THE IP-TH	RAM30290
C	POINT SOURCE IS EXPECTED. A RECEPTOR IS LOCATED AT A DIST	RAM30300
C	OF 2X TO ALLOW FOR THE INTERSECTION OF PLUMES FROM SEVERAL	RAM30310
C	POINT SOURCES. THE CHARACTERS "A" FOR AREA SOURCE AND "P"	RAM30320
C	FOR POINT SOURCES SIGNIFY WHICH TYPE OF SOURCE CAUSED THE	RAM30330
C	GENERATION OF A SPECIFIC RECEPTOR.	RAM30340
	K=NRECEP-1	RAM30350
	ITYPE(K)=ICHAR	RAM30360
	ICODE(K)=I	RAM30370
C	CALCULATE EAST AND NORTH COORDINATES(INTERNAL UNITS) OF THE	RAM30380
C	RECEPTOR. SINT AND COST REFER TO THE SINE AND COSINE OF THE	RAM30390
C	RESULTANT WIND DIRECTION.	RAM30400
	RREC(K)=RS-X*SINT/CONTWO	RAM30410
	SREC(K)=SS-X*COST/CONTWO	RAM30420
C	CONVERT TO USER UNITS FOR PRINT OUT.	RAM30430
	RREU(K)=RREC(K)*UNITS	RAM30440
	SREU(K)=SREC(K)*UNITS	RAM30450
	WRITE (10,280) K, ICHAR, I, RREU(K), SREU(K), CONM, X, HF, UPL	RAM30460
	X=2.0*X	RAM30470
	ITYPE(NRECEP)=ICHAR	RAM30480
	ICODE(NRECEP)=I	RAM30490
	RREC(NRECEP)=RS-X*SINT/CONTWO	RAM30500
	SREC(NRECEP)=SS-X*COST/CONTWO	RAM30510
C	CONVERT TO USER UNITS FOR PRINT OUT.	RAM30520
	RREU(NRECEP)=RREC(NRECEP)*UNITS	RAM30530
	SREU(NRECEP)=SREC(NRECEP)*UNITS	RAM30540

140	WRITE (IO,290) NRECEP, ICHAR, I, RREU(NRECEP), SREU(NRECEP), X, HF, UPL	RAM30550
C	CONTINUE	RAM30560
C	LOOP ON SIGNIFICANT AREA SOURCES	RAM30570
C	ONE RECEPTOR IS LOCATED ON THE DOWNWIND AZIMUTH FROM THE CENTER	RAM30580
C	OF EACH SIGNIFICANT AREA SOURCE AT A DISTANCE WHERE MAXIMUM	RAM30590
C	CONCENTRATION IS EXPECTED.	RAM30600
C		RAM30610
150	IF (NSIGA.EQ.0) GO TO 250	RAM30620
	IF (IOPT(16).EQ.0) GO TO 250	RAM30630
	WRITE (IO,300)	RAM30640
	DO 240 IP=1, NSIGA	RAM30650
	I=MAS(IP)	RAM30660
	WA=ASORC(5, I)	RAM30670
C	LOCATE SOURCE CENTER	RAM30680
	RS=ASORC(1, I)+WA	RAM30690
	SS=ASORC(2, I)+WA	RAM30700
	H=ASORC(6, I)	RAM30710
C	DETERMINE HEIGHT CLASS	RAM30720
C	IS = 1 FOR H LESS THAN 20 METERS.	RAM30730
C	IS = 2 FOR H FROM 20 TO 30 METERS.	RAM30740
C	IS = 3 FOR H FROM 30 TO 50 METERS.	RAM30750
	DO 160 IH=2, 3	RAM30760
	IF (H.LT.HCL(IH)-0.01) GO TO 170	RAM30770
160	CONTINUE	RAM30780
	IH=4	RAM30790
170	IS=IH-1	RAM30800
C	CALCULATE DISTANCE(KM) TO MAXIMUM CONCENTRATION.	RAM30810
	GO TO KNTRM, (180,190)	RAM30820
180	C=AXCOR(KST, IS)	RAM30830
	D=AXEXR(KST, IS)	RAM30840
	GO TO 200	RAM30850
190	C=AXCOF(KST, IS)	RAM30860
	D=AXEXP(KST, IS)	RAM30870
200	X=C*H**D	RAM30880
C	X IN KM.	RAM30890
	IF (COST.EQ.0.) GO TO 210	RAM30900
	A=ABS(WA/COST)	RAM30910
	IF (SINT.EQ.0.) GO TO 220	RAM30920
	B=ABS(WA/SINT)	RAM30930
	AB=AMIN1(A,B)	RAM30940
210	GO TO 230	RAM30950
	AB=ABS(WA/SINT)	RAM30960
220	GO TO 230	RAM30970
	AB=A	RAM30980
230	X=X+AB*CONTWO	RAM30990
	NRECEP=NRECEP+1	RAM31000
C	NO MORE THAN 180 RECEPTORS ARE ALLOWED.	RAM31010
	IF (NRECEP.GT.180) GO TO 260	RAM31020
C	DETERMINE RECEPTOR COORDINATES(INTERNAL UNITS)	RAM31030
	RREC(NRECEP)=RS-X*SINT/CONTWO	RAM31040
	SREC(NRECEP)=SS-X*COST/CONTWO	RAM31050
	RREU(NRECEP)=RREC(NRECEP)*UNITS	RAM31060
	SREU(NRECEP)=SREC(NRECEP)*UNITS	RAM31070
	WRITE (IO,280) NRECEP, JCHAR, I, RREU(NRECEP), SREU(NRECEP)	RAM31080
	ITYPE(NRECEP)=JCHAR	RAM31090
	ICODE(NRECEP)=I	RAM31100
240	CONTINUE	RAM31110
250	RETURN	RAM31120
260	WRITE (IO,310)	RAM31130
	NRECEP=180	RAM31140
	RETURN	RAM31150
C		RAM31160
270	FORMAT (1H0, T9, 'SIGNIFICANT POINT RECEPTORS'//1X, 'RECEPTOR #	RAM31170
	1 EAST NORTH PREDICTED MAX CONC. MAX. DIST EFF. HT U(PH	RAM31180
	2Y HT)'//1X, T38, '(MICROGRAMS/M**3)', T59, '(KM)', T70, '(M)', T80, '(M/SEC	RAM31190
	3)'//1X)	RAM31200
280	FORMAT (1X, T2, I3, 1X, A1, I3, 4X, F9.3, 3X, F9.3, 4X, 6PF12.2, 5X, OP3F10.3)	RAM31210
290	FORMAT (1X, T2, I3, 1X, A1, I3, 4X, F9.3, 3X, F9.3, 21X, 3F10.3)	RAM31220
300	FORMAT (1H0, T9, 'SIGNIFICANT AREA SOURCE RECEPTORS'//1X, 'RECEPTOR #	RAM31230
		RAM31240

310	1 EAST NORTH '//1X)	RAM31250
	FORMAT (' THE MAXIMUM NO. OF RECEPTORS HAS BEEN GENERATED'//1X,'	NRAM31260
	10 OTHERS WILL BE ACCEPTED')	RAM31270
C		RAM31280
	END	RAM31290
C		
	SUBROUTINE JMHON	RAM31310
C		RAM31320
C	SUBROUTINE JMHON (VERSION 80336), PART OF RAM.	RAM31330
C	THIS SUBROUTINE IS REFERRED TO AS F IN THE COMMON STATEMENTS	RAM31340
C	THIS ROUTINE GENERATES RECEPTORS IN A HONEYCOMB ARRANGEMENT.	RAM31350
	COMMON /AMOST/ DELH, FH, HINT(3), H, HL, IO, IOPT(50), KST, MUOR, NHTS, RC,	RRAM31360
	1CZ, SY, SZ, TEMP, TLOS, UPL, X, Y, Z	RAM31370
	COMMON /AEFM/ ITYPE(180), ICODE(180), UNITS, RREU(180), SREU(180)	RAM31380
	COMMON /AEFGKM/ NRECEP, RREC(180), SREC(180), IDATE(2), LH, NPT	RAM31390
	COMMON /AF/ GRIDSP, HRMIN, HRMAX, HSMIN, HSMAX	RAM31400
	DIMENSION HCOMBR(250), HCOMBS(250)	RAM31410
C	THE CHARACTER 'H' IDENTIFIES A RECEPTOR WHICH WAS GENERATED BY	RAM31420
C	THIS ROUTINE.	RAM31430
	DATA ICHAR //'H'/'	RAM31440
	DATA IO /6/	RAM31450
C		RAM31460
C	INITIALIZE SPACING PARAMETER FOR RECEPTOR GENERATION.	RAM31470
C	THE HORIZONTAL LOCATIONS OF ODD AND EVEN ROWS ARE STAGGERED.	RAM31480
C	THE FIRST HORIZONTAL RECEPTOR (EVEN ROW) IS AT A DISTANCE	RAM31490
C	OF .5 GRIDSP FROM THE MINIMUM HORIZONTAL DISTANCE IN CONTRAST	RAM31500
C	TO A DISTANCE OF GRIDSP FOR ODD ROWS.	RAM31510
	XINC=GRIDSP*0.5	RAM31520
	YINC=GRIDSP*0.866	RAM31530
	YCD=HSMIN+YINC/2.	RAM31540
	DUM=HRMAX-HRMIN	RAM31550
	NCOLS1=DUM/GRIDSP	RAM31560
	NCOLS2=(DUM+XINC)/GRIDSP	RAM31570
	NROWS=(HSMAX-HSMIN)/(2.*YINC)+1.	RAM31580
	NBEES=0	RAM31590
	DO 50 J=1, NROWS	RAM31600
C	THE STARTING LOCATION FOR THE GENERATION OF POSSIBLE HONEYCOMB	RAM31610
C	RECEPTORS IS THE SOUTH WEST CORNER OF THE DEFINED HONEYCOMB GRID	RAM31620
C	AREA.	RAM31630
	XCD1=HRMIN	RAM31640
	XCD2=HRMIN-XINC	RAM31650
C		RAM31660
C	GENERATION OF ODD ROWS.	RAM31670
C		RAM31680
C	THE FIRST POINT(ODD ROW) IS LOCATED AT THE DISTANCE OF GRIDSP	RAM31690
C	EAST FROM THE SOUTH WEST CORNER.	RAM31700
C		RAM31710
	DO 10 I=1, NCOLS1	RAM31720
	XCD1=XCD1+GRIDSP	RAM31730
	IF (XCD1.GT.HRMAX) GO TO 20	RAM31740
	NBEES=NBEES+1	RAM31750
C	NO MORE THAN 250 CANDIDATE RECEPTORS ARE ALLOWED.	RAM31760
	IF (NBEES.GT.250) GO TO 110	RAM31770
	HCOMBR(NBEES)=XCD1	RAM31780
	HCOMBS(NBEES)=YCD	RAM31790
10	CONTINUE	RAM31800
C	ROWS ARE LOCATED AT A PERPENDICULAR DISTANCE OF .866 TIMES GRIDSP	PRAM31810
C	ABOVE THE PRECEEDING ROW.	RAM31820
20	YCD=YCD+YINC	RAM31830
	IF (YCD.GT.HSMAX) GO TO 60	RAM31840
C		RAM31850
C	GENERATION OF EVEN ROWS	RAM31860
C		RAM31870
	DO 30 I=1, NCOLS2	RAM31880
	XCD2=XCD2+GRIDSP	RAM31890
	IF (XCD2.GT.HRMAX) GO TO 40	RAM31900
	NBEES=NBEES+1	RAM31910
	IF (NBEES.GT.250) GO TO 110	RAM31920
	HCOMBR(NBEES)=XCD2	RAM31930
	HCOMBS(NBEES)=YCD	RAM31940

30	CONTINUE	RAM31950
40	YCD=YCD+YINC	RAM31960
	IF (YCD.GT.HSMAX) GO TO 60	RAM31970
50	CONTINUE	RAM31980
C		RAM31990
C	ELIMINATE POSSIBLE HONEYCOMB RECEPTORS THAT ARE CLOSE TO OTHER	RAM32000
C	RECEPTORS.	RAM32010
60	NULIM=NRECEP	RAM32020
	DLIM=XINC*XINC	RAM32030
	DO 90 N=1,NBEES	RAM32040
	RH=HCOMBR(N)	RAM32050
	SH=HCOMBS(N)	RAM32060
C	IF NO PREVIOUS RECEPTORS, THERE WILL BE NO COMPARISONS	RAM32070
	IF (NRECEP.LE.0) GO TO 80	RAM32080
	DO 70 M=1,NULIM	RAM32090
	R=RREC(M)	RAM32100
	S=SREC(M)	RAM32110
	DUM1=ABS(R-RH)	RAM32120
	IF (DUM1.GT.XINC) GO TO 70	RAM32130
	DUM2=ABS(S-SH)	RAM32140
	IF (DUM2.GT.XINC) GO TO 70	RAM32150
	DISQ=DUM1*DUM1+DUM2*DUM2	RAM32160
C	IF THE DISTANCE BETWEEN A CURRENT RECEPTOR AND A POSSIBLE	RAM32170
C	HONEYCOMB RECEPTOR IS LESS THAN HALF THE GRIDSPACING,	RAM32180
C	THE POSSIBLE HONEYCOMB RECEPTOR IS DISCARDED.	RAM32190
	IF (DISQ.LT.DLIM) GO TO 90	RAM32200
70	CONTINUE	RAM32210
80	NRECEP=NRECEP+1	RAM32220
C	THE TOTAL NUMBER OF RECEPTORS CAN NOT EXCEED 180.	RAM32230
	IF (NRECEP.GT.180) GO TO 100	RAM32240
C	ADD NEW RECEPTOR COORDINATES (INTERNAL UNITS)	RAM32250
	RREC(NRECEP)=RH	RAM32260
	SREC(NRECEP)=SH	RAM32270
	ITYPE(NRECEP)=ICHAR	RAM32280
	ICODE(NRECEP)=0	RAM32290
C	CONVERT TO USER UNITS FOR PRINTOUT.	RAM32300
	RREU(NRECEP)=RREC(NRECEP)*UNITS	RAM32310
	SREU(NRECEP)=SREC(NRECEP)*UNITS	RAM32320
	WRITE (IO,120) NRECEP,ICHAR,RREU(NRECEP),SREU(NRECEP)	RAM32330
90	CONTINUE	RAM32340
	RETURN	RAM32350
100	WRITE (IO,130)	RAM32360
	NRECEP=180	RAM32370
	RETURN	RAM32380
110	WRITE (IO,140)	RAM32390
	CALL WAUDIT	RAM32400
	STOP	
C		RAM32410
120	FORMAT (1X,T3,I3,1X,A1,6X,F9.3,3X,F9.3)	RAM32420
130	FORMAT (' THE MAXIMUM NO. OF RECEPTORS HAS BEEN GENERATED'/1X,' NO	RAM32430
	1 OTHERS WILL BE ACCEPTED.')	RAM32440
140	FORMAT (' TOO MANY POSSIBLE HONEYCOMB RECEPTOR LOCATIONS HAVE ',	RAM32450
	1BEEN GENERATED. PLEASE REDEFINE BOUNDARIES OR GRID SPACING.')	RAM32460
C		RAM32470
	END	RAM32480
C		RAM32490
C	SUBROUTINE PT	
C	SUBROUTINE PT (VERSION 80336), PART OF RAM.	RAM32510
C	THIS SUBROUTINE IS REFERRED TO AS G IN THE COMMON STATEMENTS	RAM32520
C	THE PURPOSE OF THIS ROUTINE IS TO CALCULATE CONCENTRATIONS FROM	RAM32530
C	POINT SOURCES.	RAM32540
C		RAM32550
C	SECTION PT.A - COMMON AND DIMENSION.	RAM32560
C		RAM32570
	COMMON /AMOST/ DELH,FH,HINT(3),H,HL,IO,IOPT(50),KST,MUOR,NHTS,RC,	RAM32580
	1CZ,SY,SZ,TEMP,TLOS,UPL,X,Y,Z	RAM32590
	COMMON /AEFGKM/ NRECEP,RREC(180),SREC(180),IDATE(2),LH,NPT	RAM32600
	COMMON /AEG/ SOURCE(9,250)	RAM32610
	COMMON /AEGIKM/ IPOL,CONTWO,SINT,COST,U,HANE,PL(6)	RAM32620
		RAM32630

	COMMON /AGK/ PARTC(250)	RAM32640
	COMMON /AGM/ PSAV(250), HSAV(250), DH(250), DSAV(250), UPH(250), HPR(250)	RAM32650
	10) FP(250), PCHI(180), PHCHI(180), PSIGS(180,26), PHSIGS(180,26), IPSIGRAM32660	
	2S(250), GRANDT(180)	RAM32670
C		RAM32680
C	-->-->-->SECTION PT.B - INITIALIZE AND START RECEPTOR LOOP.	RAM32690
C		RAM32700
C	ZERO EFFECTIVE STACK HEIGHT FOR EACH SOURCE	RAM32710
C		RAM32720
C	NPT - THE NUMBER OF POINT SOURCES	RAM32730
C	DO 10 J=1,NPT	RAM32740
C	HSAV WILL BE USED TO STORE THE SOURCE PLUME HEIGHTS.	RAM32750
10	HSAV(J)=0.0	RAM32760
C	LOOP ON RECEPTORS	RAM32770
C	NRECEP - THE NUMBER OF RECEPTORS	RAM32780
C	DO 160 K=1,NRECEP	RAM32790
C		RAM32800
C	-->-->-->SECTION PT.C - START SOURCES LOOP, CALCULATE	RAM32810
C	UPWIND AND CROSSWIND DISTANCES.	RAM32820
C		RAM32830
C	DO 150 J=1,NPT	RAM32840
C	PARTC(J)=0.0	RAM32850
C	RQ - EAST COORDINATE OF THE SOURCE	RAM32860
C	RQ=SOURCE(1,J)	RAM32870
C	SQ - NORTH COORDINATE OF THE SOURCE	RAM32880
C	SQ=SOURCE(2,J)	RAM32890
C	DETERMINE UPWIND DISTANCE	RAM32900
C	XDUM,YDUM IN INTERNAL UNITS. X,Y IN KM.	RAM32910
C	RREC - EAST COORDINATE OF THE RECEPTOR	RAM32920
C	XDUM=RQ-RREC(K)	RAM32930
C	SREC - NORTH COORDINATE OF THE RECEPTOR	RAM32940
C	YDUM=SQ-SREC(K)	RAM32950
C	SINT AND COST ARE THE SIN AND COS OF THE WIND DIRECTION	RAM32960
C	CONTWO - MULTIPLIER CONSTANT TO CONVERT USER UNITS TO KM	RAM32970
C	X=(YDUM*COST+XDUM*SINT)*CONTWO	RAM32980
C	X IS THE UPWIND DISTANCE OF THE SOURCE FROM THE RECEPTOR.	RAM32990
C	IF X IS NEGATIVE, INDICATING THAT THE SOURCE IS DOWNWIND OF	RAM33000
C	THE RECEPTOR, THE CALCULATION IS TERMINATED ASSUMING NO	RAM33010
C	CONTRIBUTION FROM THAT SOURCE.	RAM33020
C	IF (X.LE.0.0) GO TO 150	RAM33030
C		RAM33040
C	DETERMINE CROSSWIND DISTANCE	RAM33050
C		RAM33060
C	Y=(YDUM*SINT-XDUM*COST)*CONTWO	RAM33070
C	H=HSAV(J)	RAM33080
C	SKIP PLUME RISE CALCULATION IF EFFECTIVE HT. HAS ALREADY BEEN	RAM33090
C	CALCULATED FOR THIS SOURCE	RAM33100
C	IF (H.EQ.0.0) GO TO 20	RAM33110
C	DELH=DH(J)	RAM33120
C		RAM33130
C	-->-->-->SECTION PT.D - EXTRAPOLATE WIND SPEED TO STACK TOP	RAM33140
C	CALCULATE PLUME RISE.	RAM33150
C		RAM33160
C	GO TO 100	RAM33170
C	MODIFY WIND SPEED BY POWER LAW PROFILE IN ORDER TO TAKE INTO	RAM33180
C	ACCOUNT THE INCREASE OF WIND SPEED WITH HEIGHT.	RAM33190
C	ASSUME WIND MEASUREMENTS ARE REPRESENTATIVE FOR HEIGHT = HANE.	RAM33200
C	THT IS THE PHYSICAL STACK HEIGHT	RAM33210
20	THT=SOURCE(5,J)	RAM33220
C	POINT SOURCE HEIGHT NOT ALLOWED TO BE LESS THAN 1 METER.	RAM33230
C	IF (THT.LT.1.) THT=1.	RAM33240
C	U - WIND SPEED AT HEIGHT 'HANE'	RAM33250
C	PL - POWER FOR THE WIND PROFILE	RAM33260
C	UPL - WIND AT THE PHYSICAL STACK HEIGHT	RAM33270
C	UPL=U*(THT/HANE)**PL(KST)	RAM33280
C	WIND SPEED NOT ALLOWED TO BE LESS THAN 1 METER/SEC.	RAM33290
C	IF (UPL.LT.1.) UPL=1.	RAM33300
C	STORE THE STACK TOP WIND FOR THE JTH SOURCE FOR THIS HOUR	RAM33310
C	UPH(J)=UPL	RAM33320
C	VS=SOURCE(8,J)	RAM33330

	BUOY=SOURCE(9,J)	RAM33340
	TS=SOURCE(6,J)	RAM33350
C	TEMP- THE AMBIENT AIR TEMPERATURE FOR THIS HOUR	RAM33360
	DELT=TS-TEMP	RAM33370
	F=BUOY*DELT/TS	RAM33380
C	IOPT(9) HOURLY EMISSION INPUT FROM TAPE/DISK? 0=NO, 1=YES.	RAM33390
C	IF (IOPT(9).EQ.0) GO TO 30	RAM33400
C	MODIFY EXIT VELOCITY AND BUOYANCY BY RATIO OF HOURLY EMISSIONS	RAM33410
C	TO AVERAGE EMISSIONS	RAM33420
	SCALE=SOURCE(IPOL,J)/PSAV(J)	RAM33430
	VS=VS*SCALE	RAM33440
	F=F*SCALE	RAM33450
30	D=SOURCE(7,J)	RAM33460
C	CALCULATE H PRIME WHICH TAKES INTO ACCOUNT STACK DOWNWASH	RAM33470
C	BRIGGS(1973) PAGE 4	RAM33480
	HPRM=THT	RAM33490
C	IF IOPT(1)=1, THEN NO STACK DOWNWASH COMPUTATION	RAM33500
	IF (IOPT(1).EQ.1) GO TO 40	RAM33510
	DUM=VS/UPL	RAM33520
	IF (DUM.LT.1.5) HPRM=THT+2.*D*(DUM-1.5)	RAM33530
C	'HPRM' IS BRIGGS' H-PRIME	RAM33540
	IF (HPRM.LT.0.) HPRM=0.	RAM33550
40	CONTINUE	RAM33560
C		RAM33570
C	CALCULATE PLUME RISE AND ADD H PRIME TO OBTAIN EFFECTIVE	RAM33580
C	STACK HEIGHT.	RAM33590
C		RAM33600
C	PLUME RISE CALCULATION	RAM33610
	IF (KST.GT.4) GO TO 60	RAM33620
C	PLUME RISE FOR UNSTABLE CONDITIONS	RAM33630
	IF (TS.LT.TEMP) GO TO 70	RAM33640
	IF (F.GE.55.) GO TO 50	RAM33650
C	DETERMINE DELTA-T FOR BUOYANCY-MOMENTUM CROSSOVER(F<55)	RAM33660
C	FOUND BY EQUATING BRIGGS(1969) EQ 5.2, P.59 WITH COMBINATION OF	RAM33670
C	BRIGGS(1971) EQUATIONS 6 AND 7, PAGE 1031 FOR F<55.	RAM33680
	DTMB=0.0297*TS*VS**0.33333/D**0.66667	RAM33690
	IF (DELT.LT.DTMB) GO TO 70	RAM33700
C	DISTANCE OF FINAL BUOYANT RISE(0.049 IS 14*3.5/1000)	RAM33710
C	BRIGGS(1971) EQN. 7, F<55, AND DIST TO FINAL RISE IS 3.5 XSTAR	RAM33720
C	DISTF IN KILOMETERS	RAM33730
	DISTF=0.049*F**0.625	RAM33740
C	COMBINATION OF BRIGGS(1971) EQNS. 6 AND 7, PAGE 1031 FOR F<55.	RAM33750
	DELH=21.425*F**0.75/UPL	RAM33760
	GO TO 90	RAM33770
C	DETERMINE DELTA-T FOR BUOYANCY-MOMENTUM CROSSOVER(F>55)	RAM33780
C	FOUND BY EQUATING BRIGGS(1969) EQ 5.2, P.59 WITH COMBINATION OF	RAM33790
C	BRIGGS(1971) EQUATIONS 6 AND 7, PAGE 1031 FOR F>55.	RAM33800
50	DTMB=0.00575*TS*VS**0.66667/D**0.33333	RAM33810
	IF (DELT.LT.DTMB) GO TO 70	RAM33820
C	DISTANCE OF FINAL BUOYANT RISE (0.119 IS 34*3.5/1000)	RAM33830
C	BRIGGS(1971) EQN. 7, F>55, AND DIST TO FINAL RISE IS 3.5 XSTAR.	RAM33840
C	DISTF IN KILOMETERS	RAM33850
	DISTF=0.119*F**0.4	RAM33860
C	COMBINATION OF BRIGGS(1971) EQNS. 6 AND 7, PAGE 1031 FOR F>55.	RAM33870
	DELH=38.71*F**0.6/UPL	RAM33880
	GO TO 90	RAM33890
C	PLUME RISE FOR STABLE CONDITIONS.	RAM33900
60	DTHDZ=0.02	RAM33910
	IF (KST.GT.5) DTHDZ=0.035	RAM33920
	S=9.80616*DTHDZ/TEMP	RAM33930
	IF (TS.LT.TEMP) GO TO 80	RAM33940
C	DETERMINE DELTA-T FOR BUOYANCY-MOMENTUM CROSSOVER(STABLE)	RAM33950
C	FOUND BY EQUATING BRIGGS(1975) EQ 59, P. 96 FOR STABLE BUOYANCY	RAM33960
C	RISE WITH BRIGGS(1969) EQ 4.28, P. 59 FOR STABLE MOMENTUM RISE.	RAM33970
	DTMB=0.019582*TEMP*VS*SQRT(S)	RAM33980
	IF (DELT.LT.DTMB) GO TO 80	RAM33990
C	STABLE BUOYANT RISE FOR WIND CONDITIONS.(WIND NOT ALLOWED LOW	RAM34000
C	ENOUGH TO REQUIRE STABLE RISE IN CALM CONDITIONS.)	RAM34010
C	BRIGGS(1975) EQ 59, PAGE 96.	RAM34020
	DELH=2.6*(F/(UPL*S))**0.33333	RAM34030

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C      COMBINATION OF BRIGGS(1975) EQ 48 AND EQ 59. NOTE DISTF IN KM. RAM34040
DISTF=0.0020715*UPL/SQRT(S) RAM34050
GO TO 90 RAM34060
C      UNSTABLE-NEUTRAL MOMENTUM RISE RAM34070
C      BRIGGS(1969) EQN. 5.2, PAGE 59 NOTE: MOST ACCURATE WHEN VS/U>4; RAM34080
C      TENDS TO OVERESTIMATE RISE WHEN VS/U<4 (SEE BRIGGS(1975) P. 78, RAM34090
C      FIGURE 4.) RAM34100
70 DELH=3.*VS*D/UPL RAM34110
DISTF=0. RAM34120
GO TO 90 RAM34130
C      STABLE MOMENTUM RISE RAM34140
80 DHA=3.*VS*D/UPL RAM34150
C      BRIGGS(1969) EQUATION 4.28, PAGE 59 RAM34160
DELH=1.5*(VS*VS*D*D*TEMP/(4.*TS*UPL))*0.333333/S**0.166667 RAM34170
IF (DHA.LT.DELH) DELH=DHA RAM34180
DISTF=0. RAM34190
C      STORE OFF PLUME HEIGHT(ETC.) FOR THIS SOURCE FOR USE WITH RAM34200
C      OTHER RECEPTORS. RAM34210
90 H=HPRM+DELH RAM34220
HSAV(J)=H RAM34230
DH(J)=DELH RAM34240
DSAV(J)=DISTF RAM34250
UPH(J)=UPL RAM34260
HPR(J)=HPRM RAM34270
FP(J)=F RAM34280
C      IF SOURCE-RECEPTOR DISTANCE IS GREATER OR EQUAL TO DISTANCE TO RAM34290
C      FINAL RISE, SKIP PLUME RISE CALCULATION AND USE FINAL RISE. RAM34300
100 IF (X.GE.DSAV(J)) GO TO 110 RAM34310
IF (IOPT(3).EQ.0.AND.IOPT(2).EQ.1) GO TO 110 RAM34320
C      CALCULATE GRADUAL PLUME RISE IF (1) THE USER SPECIFIES SO, RAM34330
C      OR (2) USER EMPLOYS CALCULATION OF INITIAL DISPERSION..... RAM34340
C      IN THIS CASE, USE OF FINAL EFFECTIVE HEIGHT IN THE CALCULATION RAM34350
C      OF DISPERSION COEFFICIENTS COULD LEAD TO MISLEADING VALUES SINCE RAM34360
C      SIGMA-Y,-Z = DELTA-H/3.5 RAM34370
DELH=160.*FP(J)**0.333333*X**0.666667/UPH(J) RAM34380
C      PLUME RISE FOR DISTANCE X(160 IS 1.6*1000**0.67 BECAUSE X IN KM) RAM34390
IF (DELH.GT.DH(J)) DELH=DH(J) RAM34400
IF (IOPT(2).EQ.1) GO TO 110 RAM34410
C      IF SPECIFYING CALCULATION OF INITIAL DISPERSION BUT ARE NOT RAM34420
C      SPECIFYING CALCULATION OF GRADUAL PLUME RISE, THEN DO NOT RAM34430
C      ADD THE NEW GRADUAL DELTA-H TO THE EFFECTIVE HEIGHT. OTHERWISE, RAM34440
C      CHECK THE GRADUAL RISE PLUME HEIGHT WITH FINAL EFFECTIVE HEIGHT RAM34450
C      AND SET THE PLUME HEIGHT TO THE SMALLER OF THE TWO VALUES. RAM34460
H=HPR(J)+DELH RAM34470
C      ADD PLUME RISE TO STACK HEIGHT FOR TOTAL EFFECTIVE STACK HT. RAM34480
C      END PLUME RISE CALCULATION RAM34490
110 UPL=UPH(J) RAM34500
C      C-->-->-->SECTION PT.E - CALCULATE THE CONTRIBUTION OF RAM34510
C      ONE SOURCE TO ONE RECEPTOR. RAM34520
C      RAM34530
IF (KST.GT.4) GO TO 120 RAM34540
IF (H.LT.HL) GO TO 120 RAM34550
PROD=0. RAM34560
GO TO 130 RAM34570
C      RCON CALCULATES RAM34580
C      THE RELATIVE CONCENTRATION , CHI/Q (SEC/M**3) RAM34590
120 CALL RCON RAM34600
C      CALCULATE TRAVEL TIME IN KM-SEC/M TO INCLUDE DECAY RATE OF RAM34610
C      POLLUTANT. RAM34620
TT=X/UPL RAM34630
C      TLOS IN METERS/KM-SEC, SO TT*TLOS IS DIMENSIONLESS RAM34640
C      INCLUDE THE POLLUTANT LOSS RAM34650
PROD=RC*SOURCE(IPOL,J)/EXP(TT*TLOS) RAM34660
C      IF HAFL IS ZERO, TLOS WILL START AS ZERO AND RAM34670
C      RESULT IN NO COMPUTATION OF POLLUTANT LOSS. RAM34680
C      INCREMENT CONCENTRATION AT K-TH RECEPTOR(G/M**3) RAM34690
C      PCHI - SUM FOR THE AVERAGING TIME AT RECEPTOR K RAM34700
130 PCHI(K)=PCHI(K)+PROD RAM34710
C      PHCHI - CONCENTRATION FOR THIS HOUR AT RECEPTOR K RAM34720
RAM34730

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	PHCHI(K)=PHCHI(K)+PROD	RAM34740
	KSIG=IPSIGS(J)	RAM34750
	IF (KSIG.EQ.0) GO TO 140	RAM34760
C	STORE CONCENTRATIONS FROM SIGNIFICANT SOURCES.(G/M**3)	RAM34770
	PSIGS(K,KSIG)=PSIGS(K,KSIG)+PROD	RAM34780
	PHSIGS(K,KSIG)=PHSIGS(K,KSIG)+PROD	RAM34790
	PSIGS(K,26)=PSIGS(K,26)+PROD	RAM34800
	PHSIGS(K,26)=PHSIGS(K,26)+PROD	RAM34810
140	PARTC(J)=PROD	RAM34820
C		RAM34830
C-->-->-->	SECTION PT.F - END SOURCE AND RECEPTOR LOOPS.	RAM34840
C		RAM34850
150	CONTINUE	RAM34860
C	END OF LOOP FOR SOURCES	RAM34870
C	WRITE PARTIAL CONCENTRATIONS ON DISK(G/M**3) IF IOPT(40) = 1.	RAM34880
	IF (IOPT(40).EQ.0) GO TO 160	RAM34890
C	USER PLEASE NOTE: PARTIAL CONC. IN G/M**3, NOT MICROGRAM/M**3	RAM34900
	WRITE (10) IDATE,LH,K,(PARTC(J),J=1,NPT)	RAM34910
160	CONTINUE	RAM34920
C	END OF LOOP FOR RECEPTORS	RAM34930
	RETURN	RAM34940
C		RAM34950
C***	SECTIONS OF SUBROUTINE PTR.	RAM34960
C	SECTION PT.A - COMMON AND DIMENSION.	RAM34970
C	SECTION PT.B - INITIALIZE AND START RECEPTOR LOOP.	RAM34980
C	SECTION PT.C - START SOURCES LOOP; CALCULATE UPWIND AND	RAM34990
	CROSSWIND DISTANCES.	RAM35000
C	SECTION PT.D - EXTRAPOLATE WIND SPEED TO STACK TOP;	RAM35010
	CALCULATE PLUME RISE.	RAM35020
C	SECTION PT.E - CALCULATE CONTRIBUTION FROM A SOURCE TO ONE	RAM35030
	RECEPTOR.	RAM35040
C	SECTION PT.F - END SOURCE AND RECEPTOR LOOPS.	RAM35050
		RAM35060
C	END	RAM35070
C		
	SUBROUTINE RCON	RAM35090
C	SUBROUTINE RCON (VERSION 80336), PART OF RAM.	RAM35100
C	THIS SUBROUTINE IS REFERRED TO AS H IN THE COMMON STATEMENTS	RAM35110
C-->-->-->	SECTION RCON.A - COMMON.	RAM35120
	COMMON /AMOST/ DELH,FH,HINT(3),H,HL,IO,IOPT(50),KST,MUOR,NHTS,RC,	RAM35130
	1CZ,SY,SZ,TEMP,TLOS,UPL,X,Y,Z	RAM35140
	DATA IO /6/	RAM35150
C		RAM35160
C-->-->-->	SECTION RCON.B - EXPLANATIONS AND COMPUTATIONS	RAM35170
	COMMON TO ALL CONDITIONS.	RAM35180
C		RAM35190
C	RCON DETERMINES RELATIVE CONCENTRATIONS, CHI/Q, FROM POINT SOURCES.	RAM35200
C	IT CALLS UPON SYZ TO OBTAIN STANDARD DEVIATIONS.	RAM35210
C	THE INPUT VARIABLES ARE....	RAM35220
C	UPL WIND SPEED (M/SEC)	RAM35230
C	Z RECEPTOR HEIGHT (M)	RAM35240
C	H EFFECTIVE STACK HEIGHT (M)	RAM35250
C	HL MIXING HEIGHT- TOP OF NEUTRAL OR UNSTABLE LAYER(M).	RAM35260
C	X DISTANCE RECEPTOR IS DOWNWIND OF SOURCE (KM)	RAM35270
C	Y DISTANCE RECEPTOR IS CROSSWIND FROM SOURCE (KM)	RAM35280
C	KST STABILITY CLASS	RAM35290
C	DELH PLUME RISE(METERS)	RAM35300
C	THE OUTPUT VARIABLES ARE....	RAM35310
C	SY HORIZONTAL DISPERSION PARAMETER	RAM35320
C	SZ VERTICAL DISPERSION PARAMETER	RAM35330
C	RC RELATIVE CONCENTRATION (SEC/M**3) ,CHI/Q	RAM35340
C	IO IS OUTPUT UNIT FOR WARNING OUTPUT.	RAM35350
C	THE FOLLOWING EQUATION IS SOLVED --	RAM35360
C	RC = (1/(2*PI*UPL*SIGMA Y*SIGMA Z))* (EXP(-0.5*(Y/SIGMA Y)**2)	RAM35370
C	(EXP(-0.5*((Z-H)/SIGMA Z)**2) + EXP(-0.5*((Z+H)/SIGMA Z)**2))	RAM35380
C	PLUS THE SUM OF THE FOLLOWING 4 TERMS K TIMES (N=1,K) --	RAM35390
C	FOR NEUTRAL OR UNSTABLE CASES:	RAM35400
C	TERM 1- EXP(-0.5*((Z-H-2NL)/SIGMA Z)**2)	RAM35410
C	TERM 2- EXP(-0.5*((Z+H-2NL)/SIGMA Z)**2)	RAM35420
C		RAM35430

C	TERM 3- EXP(-0.5*((Z-H+2NL)/SIGMA Z)**2)	RAM35440
C	TERM 4- EXP(-0.5*((Z+H+2NL)/SIGMA Z)**2)	RAM35450
C	NOTE THAT MIXING HEIGHT- THE TOP OF THE NEUTRAL OR UNSTABLE LAYER-	RAM35460
C	HAS A VALUE ONLY FOR STABILITIES 1-4, THAT IS, MIXING HEIGHT,	RAM35470
C	THE HEIGHT OF THE NEUTRAL OR UNSTABLE LAYER, DOES NOT EXIST FOR STABLE	RAM35480
C	LAYERS AT THE GROUND SURFACE- STABILITY 5 OR 6.	RAM35490
C	THE ABOVE EQUATION IS SIMILAR TO EQUATION (5.8) P 36 IN	RAM35500
C	WORKBOOK OF ATMOSPHERIC DISPERSION ESTIMATES WITH THE ADDITION	RAM35510
C	OF THE EXPONENTIAL INVOLVING Y.	RAM35520
C	IF STABLE, SKIP CONSIDERATION OF MIXING HEIGHT.	RAM35530
C	IF (KST.GE.5) GO TO 30	RAM35540
C	IF THE SOURCE IS ABOVE THE LID, SET RC = 0., AND RETURN.	RAM35550
C	IF (H.GT.HL) GO TO 10	RAM35560
10	IF (Z-HL) 30,30,20	RAM35570
10	IF (Z.LT.HL) GO TO 20	RAM35580
20	WRITE (10,260)	RAM35590
20	RC=0.	RAM35600
20	RETURN	RAM35610
C	IF X IS LESS THAN 1 METER, SET RC=0. AND RETURN. THIS AVOIDS	RAM35620
C	PROBLEMS OF INCORRECT VALUES NEAR THE SOURCE.	RAM35630
30	IF (X.LT.0.001) GO TO 20	RAM35640
C	CALL SYZ TO OBTAIN VALUES FOR SY AND SZ	RAM35650
C	CALL SYZ	RAM35660
C	SY = SIGMA Y, THE STANDARD DEVIATION OF CONCENTRATION IN THE	RAM35670
C	Y-DIRECTION (M)	RAM35680
C	SZ = SIGMA Z, THE STANDARD DEVIATION OF CONCENTRATION IN THE	RAM35690
C	Z-DIRECTION (M)	RAM35700
C	IF IOPT(3)=1, CONSIDER BUOYANCY INDUCED DISPERSION OF PLUME DUE	RAM35710
C	TO TURBULENCE DURING BUOYANT RISE.	RAM35720
C	IF (IOPT(3).EQ.0) GO TO 40	RAM35730
C	DUM=DELH/3.5	RAM35740
C	DUM=DUM*DUM	RAM35750
C	SY=SQRT(SY*SY+DUM)	RAM35760
C	SZ=SQRT(SZ*SZ+DUM)	RAM35770
40	C1=1.	RAM35780
40	IF (Y.EQ.0.0) GO TO 50	RAM35790
40	YD=1000.*Y	RAM35800
C	YD IS CROSSWIND DISTANCE IN METERS.	RAM35810
C	DUM=YD/SY	RAM35820
C	DUM=0.5*DUM*DUM	RAM35830
C	IF (DUM.GE.50.) GO TO 20	RAM35840
C	C1=EXP(DUM)	RAM35850
50	IF (KST.GT.4) GO TO 60	RAM35860
50	IF (HL.LT.5000.) GO TO 110	RAM35870
C	IF STABLE CONDITION OR UNLIMITED MIXING HEIGHT,	RAM35880
C	USE EQUATION 3.2 IF Z = 0, OR EQ 3.1 FOR NON-ZERO Z.	RAM35890
C	(EQUATION NUMBERS REFER TO WORKBOOK OF ATMOSPHERIC DISPERSION	RAM35900
C	ESTIMATES.)	RAM35910
60	C2=2.*SZ*SZ	RAM35920
60	IF (Z) 20,70,80	RAM35930
C	NOTE: AN ERRONEOUS NEGATIVE Z WILL RESULT IN ZERO CONCENTRATIONS	RAM35940
C	C-->-->SECTION RCON.C - STABLE OR UNLIMITED MIXING, Z IS ZERO.	RAM35950
C	C	RAM35960
70	C3=H*H/C2	RAM35970
70	IF (C3.GE.50.) GO TO 20	RAM35980
70	A2=1./EXP(C3)	RAM35990
C	WADE EQUATION 3.2.	RAM36000
C	RC=A2/(3.14159*UPL*SY*SZ*C1)	RAM36010
C	RETURN	RAM36020
C	C	RAM36030
C	C-->-->SECTION RCON.D - STABLE OR UNLIMITED MIXING, Z IS NON-ZERO.	RAM36040
C	C	RAM36050
80	A2=0.	RAM36060
80	A3=0.	RAM36070
80	CA=Z-H	RAM36080
80	CB=Z+H	RAM36090
80	C3=CA*CA/C2	RAM36100
80	C4=CB*CB/C2	RAM36110
80	IF (C3.GE.50.) GO TO 90	RAM36120
80		RAM36130

90	A2=1./EXP(C3)	RAM36140
	IF (C4.GE.50.) GO TO 100	RAM36150
	A3=1./EXP(C4)	RAM36160
C	WADE EQUATION 3.1.	RAM36170
100	RC=(A2+A3)/(6.28318*UPL*SY*SZ*C1)	RAM36180
	RETURN	RAM36190
C		RAM36200
C->->->->	SECTION RCON.E - UNSTABLE, ASSURED OF UNIFORM MIXING.	RAM36210
C		RAM36220
C	IF SIGMA-Z IS GREATER THAN 1.6 TIMES THE MIXING HEIGHT,	RAM36230
C	THE DISTRIBUTION BELOW THE MIXING HEIGHT IS UNIFORM WITH	RAM36240
C	HEIGHT REGARDLESS OF SOURCE HEIGHT OR RECEPTOR HEIGHT BECAUSE	RAM36250
C	OF REPEATED EDDY REFLECTIONS FROM THE GROUND AND THE MIXING HT	RAM36260
110	IF (SZ/HL.LE.1.6) GO TO 120	RAM36270
C	WADE EQUATION 3.5.	RAM36280
	RC=1./(2.5066*UPL*SY*HL*C1)	RAM36290
	RETURN	RAM36300
C	INITIAL VALUE OF AN SET = 0.	RAM36310
C	AN - THE NUMBER OF TIMES THE SUMMATION TERM IS EVALUATED	RAM36320
C	AND ADDED IN.	RAM36330
120	AN=0.	RAM36340
	IF (Z) 20,210,130	RAM36350
C		RAM36360
C->->->->	SECTION RCON.F - UNSTABLE, CALCULATE MULTIPLE EDDY	RAM36370
C	REFLECTIONS, Z IS NON-ZERO.	RAM36380
C		RAM36390
C	THE FOLLOWING STATEMENTS CALCULATE RC, THE RELATIVE CONC.	RAM36400
C	USING THE EQUATION DISCUSSED ABOVE. SEVERAL INTERMEDIATE	RAM36410
C	VARIABLES ARE USED TO AVOID REPEATING CALCULATIONS.	RAM36420
C	CHECKS ARE MADE TO BE SURE THAT THE ARGUMENT OF THE	RAM36430
C	EXPONENTIAL FUNCTION IS NEVER GREATER THAN 50 (OR LESS THAN	RAM36440
C	-50).	RAM36450
C	CALCULATE MULTIPLE EDDY REFLECTIONS FOR RECEPTOR HEIGHT Z.	RAM36460
130	A1=1./(6.28318*UPL*SY*SZ*C1)	RAM36470
	C2=2.*SZ*SZ	RAM36480
	A2=0.	RAM36490
	A3=0.	RAM36500
	CA=Z-H	RAM36510
	CB=Z+H	RAM36520
	C3=CA*CA/C2	RAM36530
	C4=CB*CB/C2	RAM36540
	IF (C3.GE.50.) GO TO 140	RAM36550
140	A2=1./EXP(C3)	RAM36560
	IF (C4.GE.50.) GO TO 150	RAM36570
150	A3=1./EXP(C4)	RAM36580
	SUM=0.	RAM36590
	THL=2.*HL	RAM36600
160	AN=AN+1.	RAM36610
	A4=0.	RAM36620
	A5=0.	RAM36630
	A6=0.	RAM36640
	A7=0.	RAM36650
	C5=AN*THL	RAM36660
	CC=CA-C5	RAM36670
	CD=CB-C5	RAM36680
	CE=CA+C5	RAM36690
	CF=CB+C5	RAM36700
	C6=CC*CC/C2	RAM36710
	C7=CD*CD/C2	RAM36720
	C8=CE*CE/C2	RAM36730
	C9=CF*CF/C2	RAM36740
	IF (C6.GE.50.) GO TO 170	RAM36750
	A4=1./EXP(C6)	RAM36760
170	IF (C7.GE.50.) GO TO 180	RAM36770
	A5=1./EXP(C7)	RAM36780
180	IF (C8.GE.50.) GO TO 190	RAM36790
	A6=1./EXP(C8)	RAM36800
190	IF (C9.GE.50.) GO TO 200	RAM36810
	A7=1./EXP(C9)	RAM36820
200	T=A4+A5+A6+A7	RAM36830

	SUM=SUM+T	RAM36840
	IF (T.GE.0.01) GO TO 160	RAM36850
	RC=A1*(A2+A3+SUM)	RAM36860
	RETURN	RAM36870
C		RAM36880
C->->->->	SECTION RCON.G - UNSTABLE, CALCULATE MULTIPLE EDDY	RAM36890
C	REFLECTIONS, Z IS ZERO.	RAM36900
C		RAM36910
C	CALCULATE MULTIPLE EDDY REFLECTIONS FOR GROUND LEVEL RECEPTOR	RAM36920
C	HEIGHT.	RAM36930
210	A1=1./(6.28318*UPL*SY*SZ*CL)	RAM36940
	A2=0.	RAM36950
	C2=2.*SZ*SZ	RAM36960
	C3=H*H/C2	RAM36970
	IF (C3.GE.50.) GO TO 220	RAM36980
	A2=2./EXP(C3)	RAM36990
220	SUM=0.	RAM37000
	THL=2.*HL	RAM37010
230	AN=AN+1.	RAM37020
	A4=0.	RAM37030
	A6=0.	RAM37040
	C5=AN*THL	RAM37050
	CC=H-C5	RAM37060
	CE=H+C5	RAM37070
	C6=CC*CC/C2	RAM37080
	C8=CE*CE/C2	RAM37090
	IF (C6.GE.50.) GO TO 240	RAM37100
	A4=2./EXP(C6)	RAM37110
240	IF (C8.GE.50.) GO TO 250	RAM37120
	A6=2./EXP(C8)	RAM37130
250	T=A4+A6	RAM37140
	SUM=SUM+T	RAM37150
	IF (T.GE.0.01) GO TO 230	RAM37160
	RC=A1*(A2+SUM)	RAM37170
	RETURN	RAM37180
C		RAM37190
C->->->->	SECTION RCON.H - FORMAT	RAM37200
260	FORMAT (1H0, 'BOTH H AND Z ARE ABOVE THE MIXING HEIGHT SO A RELIABLE	RAM37210
	IE COMPUTATION CAN NOT BE MADE.')	RAM37220
C		RAM37230
C		RAM37240
C***	SECTIONS OF SUBROUTINE RCON.	RAM37250
C	SECTION RCON.A - COMMON.	RAM37260
C	SECTION RCON.B - EXPLANATIONS AND COMPUTATIONS COMMON TO ALL	RAM37270
C	CONDITIONS.	RAM37280
C	SECTION RCON.C - STABLE OR UNLIMITED MIXING, Z IS ZERO.	RAM37290
C	SECTION RCON.D - STABLE OR UNLIMITED MIXING, Z IS NON-ZERO.	RAM37300
C	SECTION RCON.E - UNSTABLE, ASSURED OF UNIFORM MIXING.	RAM37310
C	SECTION RCON.F - UNSTABLE, CALCULATE MULTIPLE EDDY	RAM37320
C	REFLECTIONS; Z IS NON-ZERO.	RAM37330
C	SECTION RCON.G - UNSTABLE, CALCULATE MULTIPLE EDDY	RAM37340
C	REFLECTIONS; Z IS ZERO.	RAM37350
C	SECTION RCON.H - FORMAT.	RAM37360
C		RAM37370
C	END	RAM37380
C		
C	SUBROUTINE JMH54	RAM37400
C	SUBROUTINE JMH54 (VERSION 80336), PART OF RAM.	RAM37410
C	THIS SUBROUTINE IS REFERRED TO AS I IN THE COMMON STATEMENTS	RAM37420
C	THE PURPOSE OF THIS ROUTINE IS TO CALCULATE TABLES OF	RAM37430
C	CONCENTRATION NORMALIZED FOR WIND SPEED AND EMISSION RATE	RAM37440
C	FROM AREA SOURCES (CHI*U/Q). SUBROUTINE JMHICZU IS CALLED FOR	RAM37450
C	INTEGRATION OF RELATIVE CONCENTRATION.	RAM37460
C	INPUT VARIABLES ARE...	RAM37470
C	HINT- REPRESENTATIVE HEIGHTS FOR AREA SOURCES	RAM37480
C	NHTS- NUMBER OF HEIGHT CLASSES	RAM37490
C	Z- RECEPTOR HEIGHT(M)	RAM37500
C	XLIM- DISTANCE LIMIT ON INTEGRATION OF AREA SOURCES(KM)	RAM37510
C	TLOS- PARTIAL COMPUTATION RELATED TO POLLUTANT LOSS	RAM37520
C		RAM37530

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COMMON /AMOST/ DELH, FH, HINT(3), H, HL, IO, IOPT(50), KST, MUOR, NHTS, RC, BRAM37540
1CZ, SY, SZ, TEMP, TLOS, UPL, X, Y, Z RAM37550
COMMON /AEGIKM/ IPOL, CONTWO, SINT, COST, U, HANE, PL(6) RAM37560
COMMON /AIL/ CIN(3,200), XLIM RAM37570
COMMON /AIM/ HARE(3) RAM37580
C RAM37590
C CONCENTRATION TABLES ARE GENERATED FOR UP TO 3 HEIGHTS. RAM37600
DO 190 IH=1, NHTS RAM37610
H=HINT(IH) RAM37620
HARE(IH)=H RAM37630
IF (FH.EQ.1.) GO TO 10 RAM37640
PHT=H*H RAM37650
UPL=U*(PHT/HANE)**PL(KST) RAM37660
IF (UPL.LT.1.) UPL=1. RAM37670
H=((H-PHT)*5.)/UPL+PHT RAM37680
HARE(IH)=H RAM37690
GO TO 20 RAM37700
C MODIFY WIND SPEED BY POWER LAW PROFILE. RAM37710
10 IF (H.LT.1.0) H=1.0 RAM37720
UPL=U*(H/HANE)**PL(KST) RAM37730
IF (UPL.LT.1.0) UPL=1.0 RAM37740
C ZERO CONCENTRATION ARRAY RAM37750
20 DO 30 J=1,200 RAM37760
30 CIN(IH,J)=0.0 RAM37770
N=0 RAM37780
NC=10 RAM37790
CP=0.0 RAM37800
CI=0.0 RAM37810
JD=1 RAM37820
C DISTANCE IN KM. RAM37830
X=0.0 RAM37840
DELX=0.001 RAM37850
ID=1 RAM37860
40 CL=CP RAM37870
X=X+DELX RAM37880
C SUBROUTINE JMH CZ DETERMINES THE RELATIVE CONCENTRATION AT RAM37890
C VARYING DOWNWIND DISTANCES. RAM37900
CALL JMH CZ RAM37910
C CALCULATE TRAVEL TIME IN KM-SEC/M. RAM37920
TT=X/UPL RAM37930
C ADJUST RELATIVE CONCENTRATION BY POLLUTANT DECAY RATE. RAM37940
C TLOS IN METERS/KM-SEC, SO TT*TLOS IS DIMENSIONLESS. RAM37950
CP=RCZ/EXP(TT*TLOS) RAM37960
C INTEGRATED RELATIVE CONCENTRATION IS DIMENSIONLESS. RAM37970
C MULTIPLICATION BY 500. CONVERTS TO METERS AND DIVIDES BY 2. RAM37980
CI=500.*DELX*(CL+CP)+CI RAM37990
GO TO (50,90,120,150,180), JD RAM38000
C NORMALIZED CONCENTRATIONS ARE STORED IN TABLES FOR VARYING RAM38010
C DISTANCES AT VARYING TIME INTERVALS. THE FOLLOWING COMMENTS DETAIL RAM38020
C THE TABLE'S CONSTRUCTION. RAM38030
C DISTANCE<100M; CALCULATE EVERY 1 M, STORE EVERY 10 M, 0.01KM. RAM38040
50 IF (X-0.0993) 60,80,80 RAM38050
60 N=N+1 RAM38060
IF (N.LT.NC) GO TO 40 RAM38070
N=0 RAM38080
70 ID=(100.*X)+0.0008 RAM38090
C STORAGE LOCATIONS 1-9 CONTAIN INTEGRATIONS FOR 10-90 M. RAM38100
CIN(IH,ID)=CI RAM38110
GO TO 40 RAM38120
C DISTANCE 100-500M: CHANGE DELX TO 10M; STORE EVERY 10 M, 0.01KM. RAM38130
80 JD=2 RAM38140
DELX=0.01 RAM38150
GO TO 70 RAM38160
C STORAGE LOCATIONS 10-49 CONTAIN INTEGRATIONS FOR 100 M TO 490 M. RAM38170
90 IF (X-0.497) 70,100,100 RAM38180
C DISTANCE 500 -3000M; CHANGE DELX TO 100 M; STORE EVERY 100 M, 0.1KM RAM38190
100 JD=3 RAM38200
DELX=0.1 RAM38210
110 ID=(10.*X)+45.08 RAM38220
C STORAGE LOCATIONS 50-74 CONTAIN INTEGRATIONS FOR 500 M TO 2900 M. RAM38230

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	CIN(IH, ID)=CI	RAM38240
	GO TO 40	RAM38250
120	IF (X-2.95) 110,130,130	RAM38260
C	DISTANCE 3000-15,000M. ; CHANGE DELX TO 500 M; STORE EVERY 500 M,	RAM38270
C	0.5KM.	RAM38280
130	JD=4	RAM38290
	DELX=.5	RAM38300
140	ID=(2.*X)+69.08	RAM38310
C	STORAGE LOCATIONS 75-98 CONTAIN INTEGRATIONS FOR 3000 M TO	RAM38320
C	14.5 KM.	RAM38330
	CIN(IH, ID)=CI	RAM38340
	GO TO 40	RAM38350
150	IF (X-14.95) 140,160,160	RAM38360
C	DISTANCE >15,000M.; CHANGE DELX TO 1000M; STORE EVERY 1000 M,	RAM38370
C	1KM.	RAM38380
160	JD=5	RAM38390
	DELX=1.	RAM38400
170	ID=X+84.08	RAM38410
C	STORAGE LOCATIONS 99-200 CONTAIN INTEGRATIONS FOR 15 KM TO A	RAM38420
C	MAXIMUM OF 116 KM.	RAM38430
	CIN(IH, ID)=CI	RAM38440
	GO TO 40	RAM38450
180	IF (X-XLIM) 170,190,190	RAM38460
190	CONTINUE	RAM38470
	RETURN	RAM38480
C		RAM38490
	END	RAM38500
C		
	SUBROUTINE JMH CZ	RAM38520
C	SUBROUTINE JMH CZ (VERSION 80336), PART OF RAM.	RAM38530
C	THIS SUBROUTINE IS REFERRED TO AS J IN THE COMMON STATEMENTS	RAM38540
	COMMON /AMOST/ DELH, FH, HINT(3), H, HL, IO, IOPT(50), KST, MUOR, NHTS, RC,	RAM38550
	ICZ, SY, SZ, TEMP, TLOS, UPL, X, Y, Z	RAM38560
	DATA IO /6/	RAM38570
C		RAM38580
C	SUBROUTINE JMH CZ CALCULATES CHI*U/Q, RELATIVE CONCENTRATION	RAM38590
C	NORMALIZED FOR WIND SPEED AND EMISSION RATE, FOR A RECEPTOR	RAM38600
C	DOWNWIND OF A CROSSWIND INFINITE SOURCE (IN UNITS OF: PER METER	RAM38610
C	JMH CZ CALLS SUBROUTINE SGZ	RAM38620
C	THE INPUT VARIABLES ARE....	RAM38630
C	Z RECEPTOR HEIGHT (M)	RAM38640
C	H EFFECTIVE STACK HEIGHT (M)	RAM38650
C	HL MIXING HEIGHT- TOP OF NEUTRAL OR UNSTABLE LAYER(M)	RAM38660
C	(THROUGH COMMON/METCON/)	RAM38670
C	X DISTANCE RECEPTOR IS DOWNWIND OF SOURCE (KM)	RAM38680
C	KST STABILITY CLASS (THROUGH COMMON /METCON/)	RAM38690
C	THE OUTPUT VARIABLES ARE....	RAM38700
C	SZ VERTICAL DISPERSION PARAMETER.	RAM38710
C	RCZ RELATIVE CONCENTRATION HAS UNITS OF: PER METER.	RAM38720
C	THE FOLLOWING EQUATION IS SOLVED --	RAM38730
C	$RC = (1/2.5066 * \sigma Z) * ((EXP(-.05*((Z-H)/\sigma Z)**2)$	RAM38740
C	$+ (EXP(-0.5*((Z+H)/\sigma Z)**2))$	RAM38750
C	PLUS THE SUM OF THE FOLLOWING 4 TERMS K TIMES (N=1,K) --	RAM38760
C	FOR NEUTRAL OR UNSTABLE CASES:	RAM38770
C	TERM 1- $EXP(-0.5*((Z-H-2NL)/\sigma Z)**2)$	RAM38780
C	TERM 2- $EXP(-0.5*((Z+H-2NL)/\sigma Z)**2)$	RAM38790
C	TERM 3- $EXP(-0.5*((Z-H+2NL)/\sigma Z)**2)$	RAM38800
C	TERM 4- $EXP(-0.5*((Z+H+2NL)/\sigma Z)**2)$	RAM38810
C	2.5066 IS THE SQUARE ROOT OF 2 * PI	RAM38820
C	NOTE THAT MIXING HEIGHT- THE TOP OF THE NEUTRAL OR UNSTABLE LAYER-	RAM38830
C	HAS A VALUE ONLY FOR STABILITIES 1-4, THAT IS, MIXING HEIGHT	RAM38840
C	DOES NOT EXIST FOR STABLE LAYERS AT THE GROUND SURFACE- STABILITY	RAM38850
C	5 OR 6.	RAM38860
C	THE SUBROUTINE CALCULATES RC, THE RELATIVE CONCENTRATION,	RAM38870
C	USING THE EQUATION DISCUSSED ABOVE. SEVERAL INTERMEDIATE	RAM38880
C	VARIABLES ARE USED TO AVOID REPEATING CALCULATIONS.	RAM38890
C	CHECKS ARE MADE TO BE SURE THAT THE ARGUMENT OF THE	RAM38900
C	EXPONENTIAL FUNCTION IS NEVER GREATER THAN 50 (OR LESS THAN	RAM38910
C	-50). IF 'AN' BECOMES GREATER THAN 45, A LINE OF OUTPUT IS	RAM38920
C	PRINTED INFORMING OF THIS.	RAM38930

C	IO IS OUTPUT UNIT FOR OUTPUT	RAM38940
C	IF STABLE, SKIP CONSIDERATION OF MIXING HEIGHT.	RAM38950
C	IF (KST.GE.5) GO TO 30	RAM38960
C	IF THE SOURCE IS ABOVE THE LID, SET RC = 0., AND RETURN.	RAM38970
	IF (H.GT.HL) GO TO 10	RAM38980
10	IF (Z-HL) 30,30,20	RAM38990
	IF (Z.LT.HL) GO TO 20	RAM39000
	WRITE (IO,240)	RAM39010
20	RCZ=0.	RAM39020
	RETURN	RAM39030
C	IF X IS LESS THAN 1 METER, SET RC=0. AND RETURN. THIS AVOIDS	RAM39040
C	PROBLEMS OF INCORRECT VALUES NEAR THE SOURCE.	RAM39050
30	IF (X.LT.0.001) GO TO 20	RAM39060
	CALL SIGZ	RAM39070
C	SZ = SIGMA Z, THE STANDARD DEVIATION OF CONCENTRATION IN THE	RAM39080
C	Z-DIRECTION (M)	RAM39090
	IF (KST.GT.4) GO TO 40	RAM39100
	IF (HL.LT.5000) GO TO 90	RAM39110
C	IF STABLE CONDITION OR UNLIMITED MIXING HEIGHT:	RAM39120
40	C2=2.*SZ*SZ	RAM39130
	IF (Z) 20,50,60	RAM39140
C	FOR Z = ZERO:	RAM39150
50	C3=H*H/C2	RAM39160
	IF (C3.GE.50.) GO TO 20	RAM39170
	RCZ=2./(2.5066*SZ*EXP(C3))	RAM39180
	RETURN	RAM39190
C	FOR NON-ZERO Z:	RAM39200
60	A2=0.	RAM39210
	A3=0.	RAM39220
	CA=Z-H	RAM39230
	CB=Z+H	RAM39240
	C3=CA*CA/C2	RAM39250
	C4=CB*CB/C2	RAM39260
	IF (C3.GE.50.) GO TO 70	RAM39270
	A2=1./EXP(C3)	RAM39280
70	IF (C4.GE.50.) GO TO 80	RAM39290
	A3=1./EXP(C4)	RAM39300
80	RCZ=(A2+A3)/(2.5066*SZ)	RAM39310
	RETURN	RAM39320
C	IF SIGMA-Z IS GREATER THAN 1.6 TIMES THE MIXING HEIGHT,	RAM39330
C	THE DISTRIBUTION BELOW THE MIXING HEIGHT IS UNIFORM WITH	RAM39340
C	HEIGHT REGARDLESS OF SOURCE HEIGHT.	RAM39350
90	IF (SZ/HL.LE.1.6) GO TO 100	RAM39360
	RCZ=1./HL	RAM39370
	RETURN	RAM39380
C	INITIAL VALUE OF AN SET = 0.	RAM39390
C	AN THE NUMBER OF TIMES THE SUMMATION TERM IS EVALUATED	RAM39400
C	AND ADDED IN.	RAM39410
100	AN=0.	RAM39420
	IF (Z) 20,190,110	RAM39430
C	NOTE: AN ERRONEOUS NEGATIVE Z WILL RESULT IN ZERO CONCENTRATIONS.	RAM39440
C	CALCULATE MULTIPLE EDDY REFLECTIONS FOR ELEVATED RECEPTOR HEIGHT.	RAM39450
110	A1=1./(2.5066*SZ)	RAM39460
	C2=2.*SZ*SZ	RAM39470
	A2=0.	RAM39480
	A3=0.	RAM39490
	CA=Z-H	RAM39500
	CB=Z+H	RAM39510
	C3=CA*CA/C2	RAM39520
	C4=CB*CB/C2	RAM39530
	IF (C3.GE.50.) GO TO 120	RAM39540
	A2=1./EXP(C3)	RAM39550
120	IF (C4.GE.50.) GO TO 130	RAM39560
	A3=1./EXP(C4)	RAM39570
130	SUM=0.	RAM39580
	THL=2.*HL	RAM39590
140	AN=AN+1.	RAM39600
	A4=0.	RAM39610
	A5=0.	RAM39620
	A6=0.	RAM39630

	A7=0.	RAM39640
	C5=AN*THL	RAM39650
	CC=CA-C5	RAM39660
	CD=CB-C5	RAM39670
	CE=CA+C5	RAM39680
	CF=CB+C5	RAM39690
	C6=CC*CC/C2	RAM39700
	C7=CD*CD/C2	RAM39710
	C8=CE*CE/C2	RAM39720
	C9=CF*CF/C2	RAM39730
	IF (C6.GE.50.) GO TO 150	RAM39740
150	A4=1./EXP(C6)	RAM39750
	IF (C7.GE.50.) GO TO 160	RAM39760
	A5=1./EXP(C7)	RAM39770
160	IF (C8.GE.50.) GO TO 170	RAM39780
	A6=1./EXP(C8)	RAM39790
170	IF (C9.GE.50.) GO TO 180	RAM39800
	A7=1./EXP(C9)	RAM39810
180	T=A4+A5+A6+A7	RAM39820
	SUM=SUM+T	RAM39830
	IF (T.GE.0.01) GO TO 140	RAM39840
	RCZ=A1*(A2+A3+SUM)	RAM39850
	RETURN	RAM39860
C	CALCULATE MULTIPLE EDDY REFLECTIONS FOR GROUND LEVEL RECEPTOR HT.	RAM39870
190	A1=1./(2.5066*SZ)	RAM39880
	A2=0.	RAM39890
	C2=2.*SZ*SZ	RAM39900
	C3=H*H/C2	RAM39910
	IF (C3.GE.50.) GO TO 200	RAM39920
	A2=2./EXP(C3)	RAM39930
200	SUM=0.	RAM39940
	THL=2.*HL	RAM39950
210	AN=AN+1.	RAM39960
	A4=0.	RAM39970
	A6=0.	RAM39980
	C5=AN*THL	RAM39990
	CC=H-C5	RAM40000
	CE=H+C5	RAM40010
	C6=CC*CC/C2	RAM40020
	C8=CE*CE/C2	RAM40030
	IF (C6.GE.50.) GO TO 220	RAM40040
	A4=2./EXP(C6)	RAM40050
220	IF (C8.GE.50.) GO TO 230	RAM40060
	A6=2./EXP(C8)	RAM40070
230	T=A4+A6	RAM40080
	SUM=SUM+T	RAM40090
	IF (T.GE.0.01) GO TO 210	RAM40100
	RCZ=A1*(A2+SUM)	RAM40110
	RETURN	RAM40120
C		RAM40130
240	FORMAT (1H0,'BOTH H AND Z ARE ABOVE THE MIXING HEIGHT SO A RELIABLE COMPUTATION CAN NOT BE MADE.')	RAM40140
C		RAM40150
	END	RAM40160
C		RAM40170
	SUBROUTINE JMHARE	RAM40180
C		RAM40190
C	SUBROUTINE JMHARE (VERSION 80336), PART OF RAM.	RAM40200
C	THIS SUBROUTINE IS REFERRED TO AS K IN THE COMMON STATEMENTS	RAM40210
C		RAM40220
C	THE FUNCTION OF THIS SUBROUTINE IS TO CALCULATE THE CONCENTRATIONS	RAM40230
C	AT EACH RECEPTOR DUE TO AREA SOURCES. THE HANNAH TECHNIQUE	RAM40240
C	IS USED TO EXAMINE THE AREA SOURCES ALONG AN UPWIND LINE FROM	RAM40250
C	THE RECEPTOR. SUBROUTINE JMHFOL IS CALLED TO INTERPOLATE CONC.	RAM40260
C	INPUT VARIABLES ARE ...	RAM40270
C	NHTS- THE NUMBER OF AREA SOURCE HEIGHTS.	RAM40280
C	XLIM- DISTANCE LIMIT ON AREA INTEGRATION	RAM40290
C	IDATE - YEAR AND JULIAN DAY (IN COMMON/METDAT/)	RAM40300
C	LH- HOUR	RAM40310
C		RAM40320
	COMMON /AMOST/ DELH, FH, HINT(3), H, HL, IO, IOPT(50), KST, MUOR, NHTS, RC, RRAM40330	RAM40330

1	ICZ,SY,SZ,TEMP,TLOS,UPL,X,Y,Z	RAM40340
	COMMON /AEFGKM/ NRECEP,RREC(180),SREC(180),IDATE(2),LH,NPT	RAM40350
	COMMON /AEGIKM/ IPOL,CONTWO,SINT,COST,U,HANE,PL(6)	RAM40360
	COMMON /AEK/ ASORC(6,100)	RAM40370
	COMMON /AKG/ PARTC(250)	RAM40380
	COMMON /AK/ BPH(2),RMIN,SMIN,RMAX,SMAX,NAS,IRSIZE,ISSIZE,IA(25,25)	RAM40390
1	IWD,IASIGS(100),NBP	RAM40400
	COMMON /AKL/ IH,NS,KREC	RAM40410
	COMMON /AKM/ BPHM(2),ACHI(180),AHCHI(180),ASIGS(180,11),AHSIGS(180,11)	RAM40420
	DIMENSION ADEL(4),ADELS(4)	RAM40430
	DATA ADEL /0.001,0.001,-0.001,-0.001/	RAM40440
	DATA ADELS /0.001,-0.001,-0.001,0.001/	RAM40450
C		RAM40460
C	CALCULATE MODIFIED BREAK-POINT HEIGHTS, IF NECESSARY	RAM40470
	DO 10 I=1,NBP	RAM40480
	H=BPH(I)	RAM40490
	BPHM(I)=H	RAM40500
	IF (FH.EQ.1.) GO TO 10	RAM40510
	PHT=FH*H	RAM40520
	UPL=U*(PHT/HANE)**PL(KST)	RAM40530
	IF (UPL.LT.1.) UPL=1.	RAM40540
	BPHM(I)=((H-PHT)*5.)/UPL+PHT	RAM40550
10	CONTINUE	RAM40560
C	DEL: SMALL EAST-WEST INCREMENT DEPENDENT ON WIND DIRECTION	RAM40570
C	USED TO STEP INTO NEXT UPWIND AREA SOURCE.	RAM40580
	DEL=ADEL(IWD)	RAM40590
C	DELS: SMALL NORTH-SOUTH INCREMENT DEPENDENT ON WIND DIRECTION	RAM40600
C	USED TO STEP INTO NEXT UPWIND AREA SOURCE	RAM40610
	DELS=ADELS(IWD)	RAM40620
C	SUBTRACT 1 SO THAT POINT IN SOUTHWEST CORNER OF AREA SOURCE	RAM40630
C	REGION WILL HAVE IA INDEX OF (1,1).	RAM40640
	RMINI=RMIN-1.	RAM40650
	SMINI=SMIN-1.	RAM40660
C		RAM40670
C	LOOP ON RECEPTORS	RAM40680
C	UNITS FOR GEOMETRIC CALCULATIONS ARE INTERNAL UNITS.	RAM40690
	DO 290 KREC=1,NRECEP	RAM40700
C	ZERO PARTIAL CONCENTRATION ARRAY	RAM40710
	DO 20 I=1,NAS	RAM40720
20	PARTC(I)=0.0	RAM40730
	XL=0.0	RAM40740
	CONCL=0.0	RAM40750
	IHL=0	RAM40760
C	SEARCH FOR UPWIND AREA SOURCES WHICH CONTRIBUTE TO THE K-TH	RAM40770
C	RECEPTOR, BEGINNING AT THE K-TH RECEPTOR LOCATION.	RAM40780
	RRE=RREC(KREC)	RAM40790
	SRE=SREC(KREC)	RAM40800
C	SUBTRACT MINIMUM AND STEP UPWIND INTO AREA SOURCE,	RAM40810
C	THEN INTEGERIZE TO ACCESS SOURCE NUMBER IN IA ARRAY.	RAM40820
	IR=RRE-RMINI+DEL	RAM40830
	IS=SRE-SMINI+DELS	RAM40840
C	IS RECEPTOR WITHIN DEFINED LIMITS?	RAM40850
	IF ((RRE.LE.RMIN).OR.(RRE.GE.RMAX)) GO TO 230	RAM40860
	IF ((SRE.LE.SMIN).OR.(SRE.GE.SMAX)) GO TO 230	RAM40870
C		RAM40880
C	RECEPTOR IS WITHIN AREA SOURCE REGION.	RAM40890
		RAM40900
C		RAM40910
C	DETERMINE SOURCE NUMBER,NS, SOURCE CENTER(RC,SC),	RAM40920
C	HALF OF SOURCE SIDE LENGTH,D, SOURCE STRENGTH,QA, AND	RAM40930
	SOURCE HEIGHT HA.	RAM40940
30	IF ((IR.LE.0).OR.(IR.GT.IRSIZE)) GO TO 280	RAM40950
	IF ((IS.LE.0).OR.(IS.GT.ISSIZE)) GO TO 280	RAM40960
	NS=IA(IR,IS)	RAM40970
C	DO ONLY GEOMETRIC CALCULATIONS IF NS = 0.	RAM40980
	IF (NS.EQ.0) GO TO 60	RAM40990
	D=ASORC(5,NS)	RAM41000
	RC=ASORC(1,NS)+D	RAM41010
	SC=ASORC(2,NS)+D	RAM41020
	QA=ASORC(IPOL,NS)	RAM41030

	HA=ASORC(6,NS)	RAM41040
	IF (QA.LE.0.0) GO TO 70	RAM41050
C	USE POWER LAW DEPENDENT ON STABILITY CLASS TO MODIFY WIND SPEED	RAM41060
C	AT EFFECTIVE HEIGHT OF STACK.	RAM41070
C	VARY EFFECTIVE HEIGHT(M) ACCORDING TO WIND SPEED	RAM41080
C	HA- EFFECTIVE AREA SOURCE HEIGHT(M)	RAM41090
C	FH- FRACTION OF HA WHICH IS PHYSICAL HEIGHT	RAM41100
C	PHT- PHYSICAL STACK HEIGHT(M)	RAM41110
C	(HA-PHT) IS PLUME RISE	RAM41120
	PHT=FH*HA	RAM41130
	THT=PHT	RAM41140
	IF (PHT.LT.1.) THT=1.	RAM41150
	UPL=U*(THT/HANE)**PL(KST)	RAM41160
	IF (UPL.LT.1.) UPL=1.	RAM41170
	HA=((HA-PHT)*5.)/UPL+PHT	RAM41180
C	DETERMINE HEIGHT CLASS	RAM41190
	IH=NHTS	RAM41200
	GO TO (70,50,40), NHTS	RAM41210
40	IF (HA.LT.BPHM(2)) IH=2	RAM41220
50	IF (HA.LT.BPHM(1)) IH=1	RAM41230
	GO TO 70	RAM41240
C	SINCE SOURCE NO. IS ZERO, CALCULATE COORDINATES OF SOURCE CENTER	RAM41250
C	AND DEPENDING ON WIND DIRECTION BRANCH TO CODE WHICH DETERMINES	RAM41260
C	THE NEXT AREA SOURCE IN THE UPWIND DIRECTION.	RAM41270
60	D=.5	RAM41280
	RC=FLOAT(IR)+RMINI+D	RAM41290
	SC=FLOAT(IS)+SMINI+D	RAM41300
C	IWD IS 1 FOR THETA LESS THAN 90 DEG., 2 FOR 90-180 DEG, ETC.	RAM41310
70	GO TO (80,90,110,120), IWD	RAM41320
C	IWD=1	RAM41330
C	DETERMINE TWO UPWIND BOUNDARIES(NORTH AND EAST).	RAM41340
80	SB=SC+D	RAM41350
	GO TO 100	RAM41360
C	IWD=2	RAM41370
C	DETERMINE TWO UPWIND BOUNDARIES(SOUTH AND EAST).	RAM41380
90	SB=SC+D	RAM41390
100	RB=RC+D	RAM41400
	GO TO 140	RAM41410
C	IWD=3	RAM41420
C	DETERMINE TWO UPWIND BOUNDARIES(SOUTH AND WEST).	RAM41430
110	SB=SC+D	RAM41440
	GO TO 130	RAM41450
C	IWD=4	RAM41460
C	DETERMINE TWO UPWIND BOUNDARIES(NORTH AND WEST).	RAM41470
120	SB=SC+D	RAM41480
130	RB=RC+D	RAM41490
C	FIND LOCUS OF UPWIND RAY AND CLOSEST BORDER	RAM41500
140	IF (SINT.EQ.0.) GO TO 160	RAM41510
C	IF SIN=0. NORTH OR SOUTH BOUNDARY IS APPROPRIATE.	RAM41520
	XD1=(RB-RRE)/SINT	RAM41530
C	XD1 IS DISTANCE(USER UNITS) TO EAST OR WEST BOUNDARY,	RAM41540
C	WHICHEVER IS UPWIND.	RAM41550
	IF (COST.EQ.0.) GO TO 170	RAM41560
C	IF COS=0. EAST OR WEST BOUNDARY IS APPROPRIATE.	RAM41570
	XD2=(SB-SRE)/COST	RAM41580
C	XD2 IS DISTANCE(USER UNITS) TO NORTH OR SOUTH BOUNDARY,	RAM41590
C	WHICHEVER IS UPWIND.	RAM41600
	IF (XD1.LT.XD2) GO TO 170	RAM41610
150	RDUM=RRE+XD2*SINT+DELR	RAM41620
	SDUM=SB+DELS	RAM41630
C	RDUM,SDUM ARE COORDINATES OF INTERSECTION WITH BOUNDARY PLUS	RAM41640
C	SMALL INCREMENTS TO STEP INSIDE NEXT UPWIND SOURCE.	RAM41650
	DIST=XD2	RAM41660
C	DIST IS DISTANCE TO NEAREST BORDER.	RAM41670
	GO TO 180	RAM41680
160	XD2=(SB-SRE)/COST	RAM41690
	GO TO 150	RAM41700
170	RDUM=RB+DELR	RAM41710
	SDUM=SRE+XD1*COST+DELS	RAM41720
	DIST=XD1	RAM41730

180	DIST=DIST*CONTWO	RAM41740
C	DIST IS IN KM.	RAM41750
C	IF SOURCE NO. IS ZERO, PASS ON TO NEXT UPWIND AREA SOURCE	RAM41760
C	IF (NS.EQ.0) GO TO 210	RAM41770
C	IF EMISSION RATE < 10E-10, POLLUTANT CONTRIBUTION WILL BE	RAM41780
C	INSIGNIFICANT, GO ON TO NEXT UPWIND AREA SOURCE.	RAM41790
C	IF (QA.LE.10.0E-10) GO TO 210	RAM41800
C	(A SUBSTANTIAL SAVINGS IN COMPUTATION TIME IS EFFECTED IF A LARGER	RAM41810
C	AREA WITH NO EMISSIONS IS DEFINED WITH A ZERO SOURCE STRENGTH	RAM41820
C	AS OPPOSED TO LEAVING THE AREA UNDEFINED, THUS DEFAULTING TO THE	RAM41830
C	MIN.GRID SQ.SIZE WHEN SEARCHING FOR THE NEXT UPWIND SOURCE.)	RAM41840
C	THIS SOURCE TO RECEPTOR DISTANCE AND HEIGHT CLASS TO GET A VALU	RAM41850
C	FOR INTEGRATED XU/Q TO THIS DISTANCE BY INTERPOLATING IN TABLE	RAM41860
C	OF PRECALCULATED CHI*U/Q VALUES. SUBROUTINE JMHPOL PERFORMS THE	RAM41870
C	INTERPOLATION.	RAM41880
C	CALL JMHPOL (DIST,CONA)	RAM41890
C	XL(KM) IS THE UPWIND DISTANCE TO THE LAST INTERSECTION WITH A	RAM41900
C	BOUNDARY POINT.	RAM41910
C	IF (XL.LE.0) GO TO 190	RAM41920
C	IF (IH.NE.IHL) CALL JMHPOL (XL,CONCL)	RAM41930
190	DIFF=CONA-CONCL	RAM41940
C	THE CHI*U/Q DIFFERENCE IS MULTIPLIED BY EMISS. RATE AND DIVIDED	RAM41950
C	BY WIND SPEED WHICH HAS BEEN MOD.BY THE POWER LAW TO THE PROPER	RAM41960
C	HEIGHT. THIS CALCULATED VALUE, PROD, IS THE CONTRIBUTION OF SOURCE	RAM41970
C	NS TO THE TOTAL POLLUTANT CONCENTRATION AT THE K-TH RECEPTOR.	RAM41980
C	PROD=QA*DIFF/UPL	RAM41990
C	ACHI(KREC)=ACHI(KREC)+PROD	RAM42000
C	AHCHI(KREC)=AHCHI(KREC)+PROD	RAM42010
C	KSIG=IASIGS(NS)	RAM42020
C	IF (KSIG.EQ.0) GO TO 200	RAM42030
C	IF THE SOURCE IS SIGNIFICANT, STORE PARTIAL CONCENTRATION	RAM42040
C	ASIGS(KREC,KSIG)=ASIGS(KREC,KSIG)+PROD	RAM42050
C	AHSIGS(KREC,KSIG)=AHSIGS(KREC,KSIG)+PROD	RAM42060
C	ASIGS(KREC,11)=ASIGS(KREC,11)+PROD	RAM42070
C	AHSIGS(KREC,11)=AHSIGS(KREC,11)+PROD	RAM42080
200	CONCL=CONA	RAM42090
C	SAVE PARTIAL CONCENTRATION FOR ALL SOURCES	RAM42100
C	PARTC(NS)=PROD	RAM42110
C	IHL=IH	RAM42120
C	GO TO 220	RAM42130
210	IHL=0	RAM42140
220	XL=DIST	RAM42150
C	IS THIS POINT OUTSIDE SOURCE REGION?	RAM42160
C	IF ((RDUM.LE.RMIN).OR.(RDUM.GE.RMAX)) GO TO 280	RAM42170
C	IF ((SDUM.LE.SMIN).OR.(SDUM.GE.SMAX)) GO TO 280	RAM42180
C	IR, IS ARE IA INDICES FOR NEXT SOURCE	RAM42190
C	IR=RDUM-RMIN	RAM42200
C	IS=SDUM-SMIN	RAM42210
C	GO TO 30	RAM42220
C	RECEPTOR IS OUTSIDE AREA SOURCE REGION.	RAM42230
C		RAM42240
C		RAM42250
230	DXMIN=99999.	RAM42260
C	FIND THE INTERSECTION OF THE UPWIND AZIMUTH FROM THE RECEPTOR TO	RAM42270
C	THE NEAREST BORDER OF THE AREA SOURCE REGION.	RAM42280
C	ICNT=0	RAM42290
C	RM=RMIN	RAM42300
C	FIND LOCUS FOR RMIN, THEN RMAX	RAM42310
C	DO 250 L=1,2	RAM42320
C	RMR=RM-RRE	RAM42330
C	IF SINT IS ZERO, THERE IS NO LOCUS WITH THIS BOUNDARY.	RAM42340
C	IF (SINT.EQ.0.) GO TO 240	RAM42350
C	FIND NORTH COORDINATE OF LOCUS.	RAM42360
C	S=RMR*COST/SINT+SRE	RAM42370
C	IF (S.GT.SMAX) GO TO 240	RAM42380
C	IF (S.LT.SMIN) GO TO 240	RAM42390
C	FIND DISTANCE FROM RECEPTOR TO LOCUS.	RAM42400
C	DX=RMR*SINT+(S-SRE)*COST	RAM42410
C	IF DISTANCE IS NEGATIVE, THIS IS A DOWNWIND LOCUS, NOT UPWIND.	RAM42420
C	IF (DX.LT.0.) GO TO 240	RAM42430

C	IS THIS DISTANCE SHORTER THAN A PREVIOUS LOCUS?	RAM42440
	IF (DX.GE.DXMIN) GO TO 240	RAM42450
	RLOC=RM	RAM42460
	SLOC=S	RAM42470
	DXMIN=DX	RAM42480
C	COUNT THE NUMBER OF LOCI FOUND.	RAM42490
	ICNT=ICNT+1	RAM42500
240	RM=RMAX	RAM42510
250	CONTINUE	RAM42520
	SM=SMIN	RAM42530
C	FIND LOCUS FOR SMIN, THEN SMAX.	RAM42540
	DO 270 L=3,4	RAM42550
	SMS=SM-SRE	RAM42560
C	IF COSINE IS ZERO, THERE IS NO LOCUS WITH THIS BOUNDARY.	RAM42570
	IF (COST.EQ.0.) GO TO 260	RAM42580
C	FIND EAST COORDINATE OF LOCUS.	RAM42590
	R=SMS*SINT/COST+RRE	RAM42600
	IF (R.GT.RMAX) GO TO 260	RAM42610
	IF (R.LT.RMIN) GO TO 260	RAM42620
C	FIND DISTANCE FROM RECEPTOR TO LOCUS.	RAM42630
	DX=(R-RRE)*SINT+SMS*COST	RAM42640
C	IF DISTANCE IS NEGATIVE, THIS IS A DOWNWIND LOCUS, NOT UPWIND.	RAM42650
	IF (DX.LT.0.) GO TO 260	RAM42660
C	IS THIS DISTANCE SHORTER THAN A PREVIOUS LOCUS?	RAM42670
	IF (DX.GE.DXMIN) GO TO 260	RAM42680
	RLOC=R	RAM42690
	SLOC=SM	RAM42700
	DXMIN=DX	RAM42710
	ICNT=ICNT+1	RAM42720
260	SM=SMAX	RAM42730
270	CONTINUE	RAM42740
C	IF ICNT=0 NO LOCI WERE FOUND, THEREFORE NO AREA SOURCE CONTRIB.	RAM42750
C	AT THIS RECEPTOR.	RAM42760
	IF (ICNT.EQ.0) GO TO 280	RAM42770
	DIST=DXMIN	RAM42780
C	FIND THE DISTANCE TO THE NEAREST SOURCE IN KM	RAM42790
C	FIND CO-ORDINATES TO LOCATE SOURCE	RAM42800
C	DIST IS IN INTERNAL UNITS.	RAM42810
	XL=DIST*CONTWO	RAM42820
C	XL IS IN KM.	RAM42830
C	IR AND IS NOW ARE COORDINATES OF A POINT LYING IN THE NEXT	RAM42840
C	UPWIND AREA SOURCE.	RAM42850
	IR=RLOC+DELR-RMINI	RAM42860
	IS=SLOC+DELS-SMINI	RAM42870
	GO TO 30	RAM42880
C	WRITE PARTIAL CONCENTRATIONS TO DISK	RAM42890
280	IF (IOPT(40).EQ.0) GO TO 290	RAM42900
	WRITE (10) IDATE,LH,KREC,(PARTC(J),J=1,NAS)	RAM42910
290	CONTINUE	RAM42920
	RETURN	RAM42930
C	END	RAM42940
C		RAM42950
	SUBROUTINE JMHPO (X,CON)	RAM42970
C	SUBROUTINE JMHPO (VERSION 80336), PART OF RAM.	RAM42980
C	THIS SUBROUTINE IS REFERRED TO AS L IN THE COMMON STATEMENTS	RAM42990
C	INTERPOLATE FROM PRECALCULATED AREA TABLES.	RAM43000
C	THIS SUBROUTINE INTERPOLATES FROM A TABLE OF INTEGRATED VALUES	RAM43010
C	TO DETERMINE THE CONCENTRATION AT A RECEPTOR FROM AN AREA SOURCE	RAM43020
C	AT A GIVEN DISTANCE AND HEIGHT	RAM43030
C	INPUT VARIABLES ARE...	RAM43040
C	X - UPWIND DISTANCE IN KM.	RAM43050
C	IH - THE HEIGHT INDEX.	RAM43060
C	CON - RELATIVE CON. NORMALIZED FOR WIND SPEED, CHI*U/Q.	RAM43070
C	NS - CURRENT SOURCE NUMBER	RAM43080
C	KREC - CURRENT RECEPTOR NUMBER	RAM43090
C	XLIM - MAXIMUM DISTANCE FOR INTERPOLATION IN AREA TABLES	RAM43100
C		RAM43110
	COMMON /AIL/ CIN(3,200),XLIM	RAM43120
	COMMON /AKL/ IH,NS,KREC	RAM43130

	DATA IO /6/	RAM43140
	IF (X.LT.0.01) GO TO 50	RAM43150
	IF (X.GE.0.5) GO TO 10	RAM43160
C	FOR DISTANCES < 500M, CON. WAS STORED EVERY 10M.	RAM43170
C	STORAGE LOCATIONS 1-50 CONTAIN INTEGRATED CON. FOR 10 TO 500M.	RAM43180
	J=100.*X	RAM43190
	D=J	RAM43200
	XL=D/100.	RAM43210
	XU=XL+0.01	RAM43220
	GO TO 40	RAM43230
10	IF (X.GE.3.) GO TO 20	RAM43240
C	FOR DISTANCES FROM 500 TO 3,000KM CON. WAS STORED EVERY 100M.	RAM43250
C	STORAGE LOCATIONS 50-75 CONTAIN INTEGRATED CON. FOR 0.5 TO 3. KM.	RAM43260
	J=IFIX(10.*X)+45	RAM43270
	D=J-45	RAM43280
	XL=D/10.	RAM43290
	XU=XL+0.1	RAM43300
	GO TO 40	RAM43310
20	IF (X.GE.15.) GO TO 30	RAM43320
C	FOR DISTANCES 3 TO 15 KM, CON. WAS STORED EVERY 500M.	RAM43330
C	STORAGE LOCATIONS 75-99 CONTAIN INTEGRATED CON. FOR 3 TO 15 KM.	RAM43340
	J=IFIX(2.*X)+69	RAM43350
	D=J-69	RAM43360
	XL=D/2.	RAM43370
	XU=XL+0.5	RAM43380
	GO TO 40	RAM43390
C	FOR DISTANCES > 15,000M CON. WAS STORED EVERY 1000M.	RAM43400
C	STORAGE LOCATIONS 99-200 CONTAIN INTEGRATED CON. FOR 15 TO 116KM.	RAM43410
30	IF (X.GT.XLIM) GO TO 60	RAM43420
	J=IFIX(X)+84	RAM43430
	XL=J-84	RAM43440
	XU=XL+1.	RAM43450
40	K=J+1	RAM43460
C	RETRIEVE CONCENTRATIONS FOR INTERPOLATION ACCORDING TO HEIGHT	RAM43470
C	CLASS AND DISTANCE OUT.	RAM43480
	C1=CIN(IH,J)	RAM43490
	CON=C1+((X-XL)/(XU-XL))*(CIN(IH,K)-C1)	RAM43500
	RETURN	RAM43510
C	FOR DISTANCES < 100M, CON. WAS STORED IN CIN EVERY 10 M.	RAM43520
C	STORAGE LOCATION 1 CONTAINS INTEGRATED CON. FOR 10 M.	RAM43530
50	CON=100.*X*CIN(IH,1)	RAM43540
	RETURN	RAM43550
60	WRITE (IO,70) XLIM,NS,KREC	RAM43560
	CALL WAUDIT	
	STOP	
C		RAM43570
70	FORMAT (' ***THE INPUT VALUE OF XLIM, 'F10.2, ' IS SMALLER THAN TH	RAM43580
	IE CALCULATED DISTANCE FROM AREA SOURCE ',I4,' TO RECEPTOR ',I4,'**	RAM43590
	2*'/IX,'PLEASE REDEFINE XLIM')	RAM43600
C		RAM43610
	END	RAM43620
C		RAM43630
	SUBROUTINE OUTPT	
C		RAM43650
C	SUBROUTINE OUTPT (VERSION 80336), PART OF RAM.	RAM43660
C	THIS SUBROUTINE IS REFERRED TO AS M IN THE COMMON STATEMENTS	RAM43670
C	THIS SUBROUTINE PROVIDES OUTPUT CONCENTRATIONS IN	RAM43680
C	MICROGRAMS PER CUBIC METER FOR EACH HOUR IN TWO WAYS:	RAM43690
C	1) CONTRIBUTIONS FROM SIGNIFICANT SOURCES, AND	RAM43700
C	2) SUMMARIES.	RAM43710
C	BEYOND ENTRY POINT OUTAV THE SUBROUTINE PROVIDES	RAM43720
C	CONCENTRATION OUTPUT FOR EACH AVERAGING PERIOD AGAIN	RAM43730
C	IN THE ABOVE MANNER.	RAM43740
C		RAM43750
C-->-->-->SECTION OUTPT.A - COMMON, DIMENSION, AND DATA.		RAM43760
C		RAM43770
	COMMON /AMOST/ DELH,FH,HINT(3),H,HL,IO,IOPT(50),KST,MUOR,NHTS,RC,RR	RAM43780
	ICZ,SY,SZ,TEMP,TLOS,CPL,X,Y,Z	RAM43790
	COMMON /AEFM/ ITYPE(180),ICODE(180),UNITS,RREU(180),SREU(180)	RAM43800
	COMMON /AEFGKM/ NRECEP,NRECEP(180),SREC(180),IDATE(2),LH,NPT	RAM43810
	COMMON /AEGIM/ IPOL,CONTWO,SINT,COST,U,HANE,PL(6)	RAM43820

	COMMON /AEM/ NSIGP,MPS(25),NSIGA,MAS(10)	RAM43830
	COMMON /AGM/ PSAV(250),HSAV(250),DH(250),DSAV(250),UPH(250),HPR(250)	RAM43840
	10) ,FP(250),PCHI(180),PHCHI(180),PSIGS(180,26),PHSIGS(180,26),IPSIGRAM(250)	RAM43850
	2S(250),GRANDT(180)	RAM43860
	COMMON /AIM/ HARE(3)	RAM43870
	COMMON /AKM/ BPHM(2),ACHI(180),AHCHI(180),ASIGS(180,11),AHSIGS(180,11)	RAM43880
	1,11)	RAM43890
	COMMON /AM/ LINE1(20),LINE2(20),LINE3(20),IPOLU,QTHETA(24),QU(24),	RAM43900
	IQHL(24),QTEMP(24),IKST(24),NAVG,NB,RNAME(2,180)	RAM43910
	DIMENSION IRANK(180)	RAM43920
	DIMENSION GRANDS(180)	RAM43930
C		RAM43940
C-->-->-->	SECTION OUTPT.B - HOURLY CONTRIB. OUTPUT FROM PT. SOURCE	RAM43950
C		RAM43960
C	SKIP IF THERE ARE NO POINT SOURCES	RAM43970
	IF (IOPT(5).EQ.0) GO TO 100	RAM43980
C		RAM43990
C-->-->-->	SECTION OUTPT.B(1) DELETE HOURLY PT. SOURCE CONTRIB. OUTPUT?	RAM44000
	IF (IOPT(25).EQ.1) GO TO 100	RAM44010
C		RAM44020
C	PRODUCE POINT SOURCE CONTRIBUTION TITLE	RAM44030
	WRITE (IO,390) LINE1,LINE2,LINE3	RAM44040
	WRITE (IO,410) IPOLU,IDATE,LH	RAM44050
C		RAM44060
C-->-->-->	SECTION OUTPT.B(2) - DELETE MET. DATA FROM HOURLY PT.	RAM44070
C	SOURCE OUTPUT?	RAM44080
C		RAM44090
	IF (IOPT(26).EQ.1) GO TO 10	RAM44100
C		RAM44110
C	PRODUCE HOURLY MET. DATA	RAM44120
	WRITE (IO,530)	RAM44130
	WRITE (IO,540) LH,QTHETA(LH),QU(LH),QHL(LH),QTEMP(LH),IKST(LH)	RAM44140
10	WRITE (IO,520) HANE,PL(KST)	RAM44150
C		RAM44160
C-->-->-->	SECTION OUTPT.B(3) - DELETE FINAL PLUME HT. AND DIST. TO	RAM44170
C	FINAL RISE?	RAM44180
C		RAM44190
	IF (IOPT(27).EQ.1) GO TO 20	RAM44200
C		RAM44210
C	PRODUCE FINAL PLUME HT. AND DIST. TO FINAL RISE	RAM44220
	WRITE (IO,550) (I,I=1,10)	RAM44230
C	HSAV ARE CALCULATED PLUME HEIGHTS FOR THIS HOUR	RAM44240
	WRITE (IO,560) (HSAV(I),I=1,NPT)	RAM44250
C	DSAV ARE DISTANCES TO FINAL RISE FOR THIS HOUR.	RAM44260
	WRITE (IO,570) (DSAV(I),I=1,NPT)	RAM44270
C		RAM44280
C-->-->-->	SECTION OUTPT.B(4) - PRINT POINT CONTRIBUTIONS	RAM44290
C		RAM44300
20	IF (NSIGP.GT.10) GO TO 40	RAM44310
C	PRINT OUT FIRST PAGE AND TOTALS FOR 10 OR < SIGNIF. SOURCES	RAM44320
	WRITE (IO,430)	RAM44330
	WRITE (IO,440) (I,I=1,NSIGP)	RAM44340
	WRITE (IO,460)	RAM44350
	WRITE (IO,440) (MPS(I),I=1,NSIGP)	RAM44360
	WRITE (IO,470)	RAM44370
	DO 30 K=1,NRECEP	RAM44380
	WRITE (IO,480) K,(PHSIGS(K,I),I=1,NSIGP)	RAM44390
C	PRINT TOTALS	RAM44400
	WRITE (IO,490) PHSIGS(K,26),PHCHI(K)	RAM44410
30	CONTINUE	RAM44420
	GO TO 100	RAM44430
C		RAM44440
C	PRINT FIRST PAGE FOR MORE THAN 10 SIGNIFICANT SOURCES.	RAM44450
40	WRITE (IO,430)	RAM44460
	WRITE (IO,440) (I,I=1,10)	RAM44470
	WRITE (IO,500) (MPS(I),I=1,10)	RAM44480
	WRITE (IO,470)	RAM44490
	DO 50 K=1,NRECEP	RAM44500
	WRITE (IO,480) K,(PHSIGS(K,I),I=1,10)	RAM44510
50	IF (NSIGP.GT.20) GO TO 70	RAM44520

C		PRINT SECOND PAGE AND TOTALS FOR 11 TO 20 SIGNIFICANT SOURCES	RAM44530
C		WRITE (IO,390) LINE1,LINE2,LINE3	RAM44540
		WRITE (IO,410) IPOLU,IDATE,LH	RAM44550
		WRITE (IO,430)	RAM44560
		WRITE (IO,440) (I,I=11,NSIGP)	RAM44570
		WRITE (IO,460)	RAM44580
		WRITE (IO,440) (MPS(I),I=11,NSIGP)	RAM44590
		WRITE (IO,470)	RAM44600
		DO 60 K=1,NRECEP	RAM44610
		WRITE (IO,480) K,(PHSIG(K,I),I=11,NSIGP)	RAM44620
60		WRITE (IO,490) PHSIGS(K,26),PHCHI(K)	RAM44630
		GO TO 100	RAM44640
C			RAM44650
C		WRITE SECOND PAGE FOR MORE THAN 20 SIGNIFICANT SOURCES.	RAM44660
70		WRITE (IO,390) LINE1,LINE2,LINE3	RAM44670
		WRITE (IO,410) IPOLU,IDATE,LH	RAM44680
		WRITE (IO,430)	RAM44690
		WRITE (IO,440) (I,I=11,20)	RAM44700
		WRITE (IO,500) (MPS(I),I=11,20)	RAM44710
		WRITE (IO,470)	RAM44720
		DO 80 K=1,NRECEP	RAM44730
		WRITE (IO,480) K,(PHSIG(K,I),I=11,20)	RAM44740
80		WRITE (IO,390) LINE1,LINE2,LINE3	RAM44750
		WRITE (IO,410) IPOLU,IDATE,LH	RAM44760
		WRITE (IO,430)	RAM44770
C			RAM44780
C		WRITE LAST PAGE AND TOTALS FOR MORE THAN 20 SIGNIF. SOURCES.	RAM44790
		WRITE (IO,440) (I,I=21,NSIGP)	RAM44800
		WRITE (IO,460)	RAM44810
		WRITE (IO,440) (MPS(I),I=21,NSIGP)	RAM44820
		WRITE (IO,470)	RAM44830
		DO 90 K=1,NRECEP	RAM44840
		WRITE (IO,480) K,(PHSIG(K,I),I=21,NSIGP)	RAM44850
90		WRITE (IO,490) PHSIGS(K,26),PHCHI(K)	RAM44860
C			RAM44870
C->->->->		SECTION OUTPT.C - HOURLY CONTRIB. FROM AREA SOURCE	RAM44880
C			RAM44890
C		SKIP IF THERE ARE NO AREA SOURCES	RAM44900
		IF (IOPT(6).EQ.0) GO TO 130	RAM44910
C			RAM44920
C->->->->		SECTION OUTPT.C(1) - DELETE HOURLY AREA CONTRIB.?	RAM44930
C			RAM44940
100		IF (IOPT(28).EQ.1) GO TO 130	RAM44950
C			RAM44960
C		PRODUCE AREA SOURCE CONTRIB. TITLE	RAM44970
		WRITE (IO,390) LINE1,LINE2,LINE3	RAM44980
		WRITE (IO,420) IPOLU,IDATE,LH	RAM44990
C			RAM45000
C->->->->		SECTION OUTPT.C(2) - DELETE HOURLY AREA MET. DATA	RAM45010
C			RAM45020
		IF (IOPT(29).EQ.1) GO TO 110	RAM45030
C			RAM45040
C		PRODUCE HOURLY AREA SOURCE MET. DATA	RAM45050
		WRITE (IO,530)	RAM45060
		WRITE (IO,540) LH,QTHETA(LH),QU(LH),QHL(LH),QTEMP(LH),IKST(LH)	RAM45070
C			RAM45080
C->->->->		SECTION OUTPT.C(3) - PRINT AREA CONTRIBUTIONS	RAM45090
C			RAM45100
110		WRITE (IO,520) HANE,PL(KST)	RAM45110
		WRITE (IO,400) HARE,BPHM	RAM45120
		WRITE (IO,430)	RAM45130
		WRITE (IO,440) (I,I=1,NSIGA)	RAM45140
		WRITE (IO,450)	RAM45150
		WRITE (IO,440) (MAS(I),I=1,NSIGA)	RAM45160
		WRITE (IO,470)	RAM45170
		DO 120 K=1,NRECEP	RAM45180
		WRITE (IO,480) K,(AHSIGS(K,I),I=1,NSIGA)	RAM45190
120		WRITE (IO,490) AHSIGS(K,11),AUCHI(K)	RAM45200
C			RAM45210
			RAM45220

C-->-->-->SECTION OUTPT.D - HOURLY SUMMARY TABLE	RAM45230
C	RAM45240
C-->-->-->SECTION OUTPT.D(1) - DELETE HOURLY SUMMARIES?	RAM45250
C	RAM45260
130 IF (IOPT(30).EQ.1) RETURN	RAM45270
C	RAM45280
PRODUCE HOURLY SUMMARY TITLE	RAM45290
WRITE (IO,390) LINE1,LINE2,LINE3	RAM45300
WRITE (IO,510) IPOLU,IDATE,LH	RAM45310
C	RAM45320
C-->-->-->SECTION OUTPT.D(2) - DELETE HOURLY MET. DATA?	RAM45330
C	RAM45340
IF (IOPT(31).EQ.1) GO TO 140	RAM45350
PRODUCE HOURLY SUMMARY TABLE MET. DATA	RAM45360
WRITE (IO,530)	RAM45370
WRITE (IO,540) LH,QTHETA(LH),QU(LH),QHL(LH),QTEMP(LH),IKST(LH)	RAM45380
140 WRITE (IO,520) HANE,PL(KST)	RAM45390
IF (IOPT(6).EQ.1) WRITE (IO,400) HARE,BPHM	RAM45400
WRITE (IO,580)	RAM45410
C	RAM45420
C-->-->-->SECTION OUTPT.D(3) - RANK CONCENTRATIONS	RAM45430
C	RAM45440
DO 150 K=1,NRECEP	RAM45450
GRANDS(K)=GRANDT(K)	RAM45460
C	RAM45470
DO 170 I=1,NRECEP	RAM45480
CMAX=-1.0	RAM45490
DO 160 K=1,NRECEP	RAM45500
IF (GRANDT(K).LE.CMAX) GO TO 160	RAM45510
CMAX=GRANDT(K)	RAM45520
LMAX=K	RAM45530
160 CONTINUE	RAM45540
IRANK(LMAX)=I	RAM45550
GRANDT(LMAX)=-1.0	RAM45560
170 CONTINUE	RAM45570
C	RAM45580
C-->-->-->SECTION OUTPT.D(4) - PRINT SUMMARY TABLE	RAM45590
C	RAM45600
DO 180 K=1,NRECEP	RAM45610
180 WRITE (IO,590) K,ITYPE(K),ICODE(K),(RNAME(J,K),J=1,2),RREU(K),SREURAM45620	
1(K),PHSIGS(K,26),PHCHI(K),AHSIGS(K,11),AHCHI(K),GRANDS(K),IRANK(K)	RAM45630
RETURN	RAM45640
C	RAM45650
C	RAM45660
C-->-->-->SECTION OUTPT.E - ENTRY POINT FOR AVERAGING TIME	RAM45670
C	RAM45680
ENTRY OUTAV	RAM45690
C	RAM45700
AT THIS ENTRY POINT, CONCENTRATION OUTPUT	RAM45710
C	RAM45720
IN MICROGRAMS PER CUBIC METER ARE PRINTED FOR THE	RAM45730
C	RAM45740
AVERAGING PERIOD. CONTRIBUTIONS AND/OR SUMMARY	
C	RAM45750
INFORMATION IS AVAILABLE.	RAM45760
C-->-->-->SECTION OUTPT.E(1) - AVG. CONC. OVER SPEC. TIME PERIOD	RAM45770
C	RAM45780
SKIP IF THERE ARE NO POINT SOURCE CONTRIBUTIONS PRINTED OUT	RAM45790
IF (IOPT(5).EQ.0) GO TO 290	RAM45800
C	RAM45810
CALCULATE AVERAGE POINT CONTRIBUTIONS.	RAM45820
DO 190 K=1,NRECEP	RAM45830
190 PSIGS(K,26)=PSIGS(K,26)/NAVG	RAM45840
IF (IOPT(33).EQ.1) GO TO 290	RAM45850
DO 210 K=1,NRECEP	RAM45860
DO 200 I=1,NSIGP	RAM45870
200 PSIGS(K,I)=PSIGS(K,I)/NAVG	RAM45880
210 CONTINUE	RAM45890
C	RAM45900
C-->-->-->SECTION OUTPT.F - AVG. PERIOD PT. CONTRIB.	RAM45910
C	RAM45920
SKIP IF THERE ARE NO POINT SOURCES	
C	

C-->-->-->SECTION OUTPT.F(2) - PRINT AVG. PERIOD PT. SOURCE CONTRIB.	RAM45930
WRITE (IO,390) LINE1,LINE2,LINE3	RAM45940
WRITE (IO,600) NAVG,IPOLU,IDATE,NB,HANE,PL	RAM45950
IF (NSIGP.GT.10) GO TO 230	RAM45960
C	RAM45970
C PRINT OUT FIRST PAGE AND TOTALS FOR 10 OR < SIGNIF. SOURCES	RAM45980
WRITE (IO,440) (I,I=1,NSIGP)	RAM45990
WRITE (IO,460)	RAM46000
WRITE (IO,440) (MPS(I),I=1,NSIGP)	RAM46010
WRITE (IO,470)	RAM46020
DO 220 K=1,NRECEP	RAM46030
WRITE (IO,480) K,(PSIGS(K,I),I=1,NSIGP)	RAM46040
C PRINT TOTALS	RAM46050
220 WRITE (IO,490) PSIGS(K,26),PCHI(K)	RAM46060
GO TO 290	RAM46070
C	RAM46080
C PRINT FIRST PAGE FOR MORE THAN 10 SIGNIF SOURCES	RAM46090
230 WRITE (IO,440) (I,I=1,10)	RAM46100
WRITE (IO,500) (MPS(I),I=1,10)	RAM46110
WRITE (IO,470)	RAM46120
DO 240 K=1,NRECEP	RAM46130
240 WRITE (IO,480) K,(PSIGS(K,I),I=1,10)	RAM46140
IF (NSIGP.GT.20) GO TO 260	RAM46150
C	RAM46160
C PRINT SECOND PAGE AND TOTALS FOR 11 TO 20 SIGNIF SOURCES	RAM46170
WRITE (IO,390) LINE1,LINE2,LINE3	RAM46180
WRITE (IO,600) NAVG,IPOLU,IDATE,NB,HANE,PL	RAM46190
WRITE (IO,440) (I,I=11,NSIGP)	RAM46200
WRITE (IO,460)	RAM46210
WRITE (IO,440) (MPS(I),I=11,NSIGP)	RAM46220
WRITE (IO,470)	RAM46230
DO 250 K=1,NRECEP	RAM46240
WRITE (IO,480) K,(PSIGS(K,I),I=11,NSIGP)	RAM46250
250 WRITE (IO,490) PSIGS(K,26),PCHI(K)	RAM46260
GO TO 290	RAM46270
C	RAM46280
C WRITE SECOND PAGE FOR MORE THAN 20 SIGNIF SOURCES	RAM46290
260 WRITE (IO,390) LINE1,LINE2,LINE3	RAM46300
WRITE (IO,600) NAVG,IPOLU,IDATE,NB,HANE,PL	RAM46310
WRITE (IO,440) (I,I=11,20)	RAM46320
WRITE (IO,500) (MPS(I),I=11,20)	RAM46330
WRITE (IO,470)	RAM46340
DO 270 K=1,NRECEP	RAM46350
270 WRITE (IO,480) K,(PSIGS(K,I),I=11,20)	RAM46360
C	RAM46370
C WRITE LAST PAGE AND TOTALS FOR MORE THAN 20 SIGNIF SOURCES	RAM46380
WRITE (IO,390) LINE1,LINE2,LINE3	RAM46390
WRITE (IO,600) NAVG,IPOLU,IDATE,NB,HANE,PL	RAM46400
WRITE (IO,440) (I,I=21,NSIGP)	RAM46410
WRITE (IO,460)	RAM46420
WRITE (IO,440) (MPS(I),I=21,NSIGP)	RAM46430
WRITE (IO,470)	RAM46440
DO 280 K=1,NRECEP	RAM46450
WRITE (IO,480) K,(PSIGS(K,I),I=21,NSIGP)	RAM46460
280 WRITE (IO,490) PSIGS(K,26),PCHI(K)	RAM46470
C	RAM46480
C-->-->-->SECTION OUTPT.G - AVG.PERIOD AREA CONTRIB.	RAM46490
C	RAM46500
C-->-->-->SECTION OUTPT.G(1) - DELETE AVG. PERIOD AREA SOURCE CONTRIB?	RAM46510
290 IF (IOPT(6).EQ.0) GO TO 340	RAM46520
C CALCULATE AVERAGE AREA CONTRIBUTIONS.	RAM46530
DO 300 K=1,NRECEP	RAM46540
300 ASIGS(K,11)=ASIGS(K,11)/NAVG	RAM46550
IF (IOPT(34).EQ.1) GO TO 340	RAM46560
DO 320 K=1,NRECEP	RAM46570
DO 310 I=1,NSIGA	RAM46580
310 ASIGS(K,I)=ASIGS(K,I)/NAVG	RAM46590
320 CONTINUE	RAM46600
C	RAM46610
C-->-->-->SECTION OUTPT.G(2) - PRINT AVG. PERIOD AREA SOURCE CONTRIB.	RAM46620

C	WRITE (IO,390) LINE1,LINE2,LINE3	RAM46630
	WRITE (IO,610) NAVG,IPOLU,IDATE,NB,HANE,PL	RAM46640
	WRITE (IO,440) (I,I=1,NSIGA)	RAM46650
	WRITE (IO,450)	RAM46660
	WRITE (IO,440) (MAS(I),I=1,NSIGA)	RAM46670
	WRITE (IO,470)	RAM46680
	DO 330 K=1,NRECEP	RAM46690
	WRITE (IO,480) K,(ASIGS(K,I),I=1,NSIGA)	RAM46700
330	WRITE (IO,490) ASIGS(K,11),ACHI(K)	RAM46710
C		RAM46720
C-->-->-->SECTION OUTPT.H - AVG. PERIOD SUMMARY		RAM46730
C		RAM46740
C-->-->-->SECTION OUTPT.H(1) - DELETE AVG. PERIOD SUMMARY?		RAM46750
C		RAM46760
340	IF (IOPT(35).EQ.1) RETURN	RAM46770
C		RAM46780
C	PRINT AVG. PERIOD SUMMARY	RAM46790
	WRITE (IO,390) LINE1,LINE2,LINE3	RAM46800
	WRITE (IO,620) NAVG,IPOLU,IDATE,NB,HANE,PL	RAM46810
	WRITE (IO,580)	RAM46820
C	RANK CONCENTRATIONS	RAM46830
	DO 350 K=1,NRECEP	RAM46840
350	GRANDS(K)=GRANDT(K)	RAM46850
	DO 370 I=1,NRECEP	RAM46860
	CMAX=-1.0	RAM46870
	DO 360 K=1,NRECEP	RAM46880
	IF (GRANDT(K).LE.CMAX) GO TO 360	RAM46890
	CMAX=GRANDT(K)	RAM46900
	LMAX=K	RAM46910
360	CONTINUE	RAM46920
	IRANK(LMAX)=I	RAM46930
370	GRANDT(LMAX)=-1.0	RAM46940
	DO 380 K=1,NRECEP	RAM46950
380	WRITE (IO,590) K,ITYPE(K),ICODE(K),(RNAME(J,K),J=1,2),RREU(K),SREURAM46970	RAM46980
	1(K),PSIGS(K,26),PCHI(K),ASIGS(K,11),ACHI(K),GRANDS(K),IRANK(K)	RAM46990
C		RAM47000
	RETURN	RAM47010
C		RAM47020
C-->-->-->SECTION OUTPT.J - FORMATS		RAM47030
C		RAM47040
390	FORMAT ('1',20A4/1X,20A4/1X,20A4)	RAM47050
400	FORMAT (1H0,T40,'AREA HTS: ',F8.3,',',F8.3,',',F8.3,'; SEPARATIRAM47060	RAM47070
410	FORMAT ('0',T30,A4,'CONTRIBUTION(MICROGRAMS/M**3) FROM SIGNIFICANRAM47080	RAM47090
420	FORMAT ('0',T30,A4,'CONTRIBUTION(MICROGRAMS/M**3) FROM SIGNIFICANRAM47100	RAM47110
430	FORMAT (1H0,T5,'RANK')	RAM47120
440	FORMAT ('+',T12,10(I3,7X))	RAM47130
450	FORMAT ('+',T113,'TOTAL TOTAL'/1X,T113,'SIGNIF ALL AREA'/1XRAM47140	RAM47150
460	FORMAT ('+',T113,'TOTAL TOTAL'/1X,T113,'SIGNIF ALL POINT'/1RAM47160	RAM47170
470	FORMAT (1X,T113,'POINT SOURCES'/1X,'SOURCE #')	RAM47180
480	FORMAT (1X,T113,'RECEP #')	RAM47190
490	FORMAT (1X,I3,2X,6P10F10.3)	RAM47200
500	FORMAT ('+',T109,6P2F10.3)	RAM47210
510	FORMAT (1H0,'SOURCE #',T12,10(I3,7X))	RAM47220
	FORMAT ('0',T25,A4,'SUMMARY CONCENTRATION TABLE(MICROGRAMS/M**3)	RAM47230
	1'5X,I2,'/','I4,' : HOUR',I2/1X)	RAM47240
520	FORMAT (1H+,T60,'ANEMOM HT: ',F6.2,' PL: ',F6.2)	RAM47250
530	FORMAT (1X,T2,'HOUR THETA SPEED MIXING TEMP STABILITY'/RAM47260	RAM47270
	11X,T9,'(DEG) (M/S) HEIGHT(M) (K) CLASS'/1X)	RAM47280
540	FORMAT (1X,T3,I2,4F9.2,6X,I1)	RAM47290
550	FORMAT (1H0,8X,10I11/)	RAM47300
560	FORMAT (' FINAL HT (M) ',10F11.2)	RAM47310
570	FORMAT (' DIST FIN HT (KM)',10F11.3)	RAM47320
580	FORMAT (1X,'RECEPTOR NO. EAST NORTH ',2X,5('TOTALRAM47330	RAM47340
	1 FROM '),'CONCENTRATION'/1X,T46,'SIGN',IF POINT ALL POINT SRAM47310	RAM47320
	2IGNIF AREA ALL AREA ALL SOURCES',5X,'RANK'/1X,T48.4('SOURCERAM47320	


```

590 3S',6X)/1X) RAM47330
600 FORMAT (1X,T3,I3,1X,A1,I3,2X,2A4,F11.3,F12.3,6P5F13.4,6X,I3) RAM47340
    FORMAT ('0',T22,I2,-'HOUR AVERAGE',A4,'CONTRIBUTION(MICROGRAMS/MRAM47350
1**3) FROM SIGNIFICANT POINT SOURCES',5X,I2,'/',I3,'START HOUR:',RAM47360
2,I2//1X,T20,'ANEMOM HT:',F4.0,3X,PL: A-',F4.2,2X,'B-',F4.2,'C-RAM47370
3',F4.2,2X,'D-',F4.2,2X,'E-',F4.2,2X,'F-',F4.2/1X,T5,'RANK') RAM47380
610 FORMAT ('0',T22,I2,-'HOUR AVERAGE',A4,'CONTRIBUTION(MICROGRAMS/MRAM47390
1**3) FROM SIGNIFICANT AREA SOURCES',5X,I2,'/',I3,'START HOUR:',RAM47400
2I2//1X,T20,'ANEMOM HT:',F4.0,2X,PL: A-',F4.2,2X,'B-',F4.2,2X,'C-RAM47410
3-',F4.2,2X,'D-',F4.2,2X,'E-',F4.2,2X,'F-',F4.2/1X,T5,'RANK') RAM47420
620 FORMAT ('0',T25,I2,-'HOUR AVERAGE',A4,'SUMMARY CONCENTRATION TABRAM47430
1LE(MICROGRAMS/M**3)',5X,I2,'/',I3,'START HOUR:',I2//1X,T20,'ANERAM47440
2MOM HT:',F4.0,2X,PL: A-',F4.2,2X,'B-',F4.2,2X,'C-',F4.2,2X,'DRAM47450
3-',F4.2,2X,'E-',F4.2,2X,'F-',F4.2/1X) RAM47460
C END RAM47470
C RAM47480
C SUBROUTINE RANK (L) RAM47500
C SUBROUTINE RANK (VERSION 80336), PART OF RAM. RAM47510
C THIS SUBROUTINE IS REFERRED TO AS N IN THE COMMON STATEMENTS RAM47520
C CALLED BY RAM TO ARRANGE CONCENTRATIONS OF VARIOUS AVG RAM47530
C TIMES INTO HIGH-FIVE TABLES...THAT IS, ARRAYS STORING RAM47540
C THE HIGHEST FIVE CONCENTRATIONS FOR EACH RECEPTOR FOR RAM47550
C EACH AVG TIME. RAM47560
C VARIABLES OUTPUT: RAM47570
C HMAXA(J,K,L) CONCENTRATIONS ACCORDING TO RAM47580
C J : RANK OF CONC. (1-5) RAM47590
C K : RECEPTOR NUMBER RAM47600
C L : AVG TIME RAM47610
C NDAY(J,K,L) : ASSOCIATED DAY OF CONC. RAM47620
C IHR(J,K,L) : ENDING HOUR OF CONC. RAM47630
C COMMON /AEFGKM/ NRECEP,RREC(180),SREC(180),IDATE(2),LH,NPT RAM47640
C COMMON /AN/ HMAXA(5,180,5),NDAY(5,180,5),IHR(5,180,5),CONC(180,5), RAM47650
1JDAY RAM47660
C IO=6 RAM47670
C RESET AVERAGING PERIOD FLAG AND SET CALM FLAG, LL. RAM47680
C CALMS ACCOUNTED FOR ONLY WHEN DEFAULT OPTION ON. RAM47690
C LL=0 RAM47700
C IF(L.GT.4)LL=1 RAM47710
C IF(L.EQ.22)L=2 RAM47720
C IF(L.EQ.33)L=3 RAM47730
C IF(L.EQ.44)L=4 RAM47740
C DO 50 K=1,NRECEP RAM47750
C IF (CONC(K,L).LE.HMAXA(5,K,L)) GO TO 50 RAM47760
C DO 10 J=1,5 RAM47770
C IF (CONC(K,L).GT.HMAXA(J,K,L)) GO TO 20 RAM47780
C CONCENTRATION IS ONE OF THE TOP FIVE RAM47790
10 CONTINUE RAM47800
C WRITE (IO,70) RAM47810
C GO TO 50 RAM47820
C THE FOLLOWING DO-LOOP HAS THE EFFECT OF INSERTING A NEW RAM47830
C CONCENTRATION ENTRY INTO ITS PROPER POSITION WHILE SHIFTING RAM47840
C DOWN THE 'OLD' LOWER CONCENTRATIONS THUS ESTABLISHING THE RAM47850
C 'HIGH-FIVE' CONCENTRATION TABLE. RAM47860
20 IF (J.EQ.5) GO TO 40 RAM47870
C DO 30 IJ=4,J,-1 RAM47880
C IJPL=IJ+1 RAM47890
C HMAXA(IJPL,K,L)=HMAXA(IJ,K,L) RAM47900
C NDAY(IJPL,K,L)=NDAY(IJ,K,L) RAM47910
C IHR(IJPL,K,L)=IHR(IJ,K,L) RAM47920
30 INSERT LATEST CONC, DAY AND ENDING HR INTO THE RAM47930
C PROPER RANK IN THE HIGH-FIVE TABLE RAM47940
C HMAXA(J,K,L)=CONC(K,L) RAM47950
C NDAY(J,K,L)=JDAY RAM47960
C IHR(J,K,L)=LH RAM47970
C ADD 100 TO HOUR TO SET CALM FLAG FOR MAIN. RAM47980
C IF(LL.EQ.1.AND.L.NE.1)IHR(J,K,L)=IHR(J,K,L)+100 RAM47990
50 CONTINUE RAM48000
C DO 60 K=1,NRECEP RAM48010
C RAM48020

```

```
60  CONC(K,L)=0.  
    CONTINUE  
    RETURN  
C  
70  FORMAT (1X,'    ****ERROR IN FINDING THE MAX CONCENTRATION***')  
C  
    END
```

RAM48030
RAM48040
RAM48050
RAM48060
RAM48070
RAM48080
RAM48090

APPENDIX B

JAPCA REPRINT

An Efficient Gaussian-Plume Multiple-Source Air Quality Algorithm

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The information presented in this paper is directed to air pollution scientists with an interest in applying air quality simulation models. RAM is the three letter designation for this efficient Gaussian-plume multiple-source air quality algorithm. RAM is a method of estimating short-term dispersion using the Gaussian steady-state model. This algorithm can be used for estimating air quality concentrations of relatively stable pollutants for averaging times from an hour to a day in urban areas from point and area sources. The algorithm is applicable for locations with level or gently rolling terrain where a single wind vector for each hour is a good approximation to the flow over the source area considered. Calculations are performed for each hour. Hourly meteorological data required are wind direction, wind speed, stability class, and mixing height. Emission information required of point sources consists of source coordinates, emission rate, physical height, stack gas volume flow and stack gas temperature. Emission information required of area sources consists of south-west corner coordinates, source area, total area emission rate and effective area source height. Computation time is kept to a minimum by the manner in which concentrations from area sources are estimated using a narrow plume hypothesis and using the area source squares as given rather than breaking down all sources to an area of uniform elements. Options are available to the user to allow use of three different types of receptor locations: 1) those whose coordinates are input by the user, 2) those whose coordinates are determined by the model and are downwind of significant point and area sources where maxima are likely to occur, and 3) those whose coordinates are determined by the model to give good area coverage of a specific portion of the region. Computation time is also decreased by keeping the number of receptors to a minimum.

The purpose of formulating RAM is to provide a readily available computer program based on the assumptions of steady-state Gaussian dispersion. RAM can be used for any short-term (one-hour to one-day) determination of urban air quality resulting from pollutants released from point and/or area sources. Urban planners can use RAM to determine the effects of new source locations and of control strategies upon short term air quality. If the input meteorological parameter values can be forecast with sufficient accuracy, control agency officials can use RAM to predict ambient air quality levels, primarily over the 24-hour averaging time, to 1) locate mobile air sampling units, and 2) assist with emission reduction tactics. Especially for control tactics, diurnal and day-to-day emission variations must be considered in the source inventory input to the model. For most of these uses, the optional feature to assist in locating maximum points should be utilized. Computations are organized so that execution of the program is rapid, thus real-time computations are feasible.

Briggs' plume rise equations are used to estimate effective height of point sources. Concentrations from the point sources are determined using distance crosswind and distance upwind from the receptor. Considerable time is saved in calculating concentrations from area sources by using a narrow plume

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simplification which considers sources upwind from a receptor to be representative of those affecting the receptor. Area source sizes are used as given in the inventory rather than creating an internal inventory of uniform elements.

The algorithm is applicable for locations with level or gently rolling terrain where a single wind vector for each hour is a reasonable approximation of the flow over the source area considered. A single mixing height and a single stability class for each hour are assumed representative of the area. The use of the RAM is restricted to relatively stable pollutants.

Options are available to allow the use of three different types of receptor locations: 1) those whose coordinates are input by the user, 2) those whose coordinates are determined by RAM and are downwind of significant point and area sources where maxima are likely to occur, and 3) those whose coordinates are determined by RAM to give good area coverage of a specific portion of the region. Options are also available concerning the detail of output produced.

The Algorithm

Inputs Required

The algorithm always requires emission and meteorological data, and depending on receptor options used, it may also require receptor data. Any convenient east-north rectangular coordinate system may be used since all conversion from user units to meters is performed internally by use of an input conversion factor.

A. Point source information consists of the following for each source:

1. East coordinate of source location, user units
2. North coordinate of source location, user units
3. Stack height (above ground), meters
4. Stack inside top diameter, meters
5. Stack gas temperature, °K
6. Stack gas velocity, m sec^{-1}
7. Pollutant emission rate, g sec^{-1}

B. Area source information consists of the following for each source:

1. East coordinate of the southwest corner of the area source, user units
2. North coordinate of the southwest corner of the area source, user units
3. Effective emission height, meters
4. Side length of area source, user units
5. Total pollutant emission rate for the area, g sec^{-1}

Area sources must be squares. They can be of various sizes, but their side length must be an integer multiple of a common side length. The term UNIT SQUARE refers to a source with this minimum common side length. The effective emission height of the area sources is assumed to be the effective height that occurs with a 5 m sec^{-1} wind. The effective height of the area sources can be varied with wind speed. Area emission rates are converted internally to $\text{g sec}^{-1} \text{ m}^{-2}$.

C. Meteorological data, representative of the region being considered, consists of hourly values of the following:

1. Wind direction, deg clockwise from North
2. Wind speed, m sec^{-1}
3. Stability class, dimensionless
4. Mixing height, meters

The stability class is that of Pasquill.

D. Receptor information, if required by user specification, consists of the following for each receptor:

1. East coordinate of the receptor location, user units
2. North coordinate of the receptor location, user units

Only one receptor height, z , above ground is allowed for a given execution of the model. This height can be zero or positive.

Basic Principles

The following assumptions are made: 1) Dispersion from points and area elements result in Gaussian distributions in both the horizontal and vertical directions through the dispersing plume, and therefore steady-state Gaussian plume equations can be used for point sources and the integration of these equations for area sources. 2) Concentration estimates may be made for each hourly period using the mean meteorological conditions appropriate for each hour. 3) The total concentration at a receptor is the sum of the concentrations estimated from all point and area sources, that is, concentrations are additive.

For point sources, the plume rise is calculated from the stack gas temperature, stack diameter, and stack gas velocity using the equations of Briggs.¹⁻³ The effective emission height is the physical stack height plus the plume rise.

In order to calculate contributions from point sources the upwind distance, x , and the crosswind distance, y , of each source from each receptor are calculated using Eq. A1 and A2

PLAN VIEW OF AREA SOURCES
SOURCE NUMBER IN LOWER LEFT CORNER
EMISSION RATE (G/SEC) IN PARENTHESES

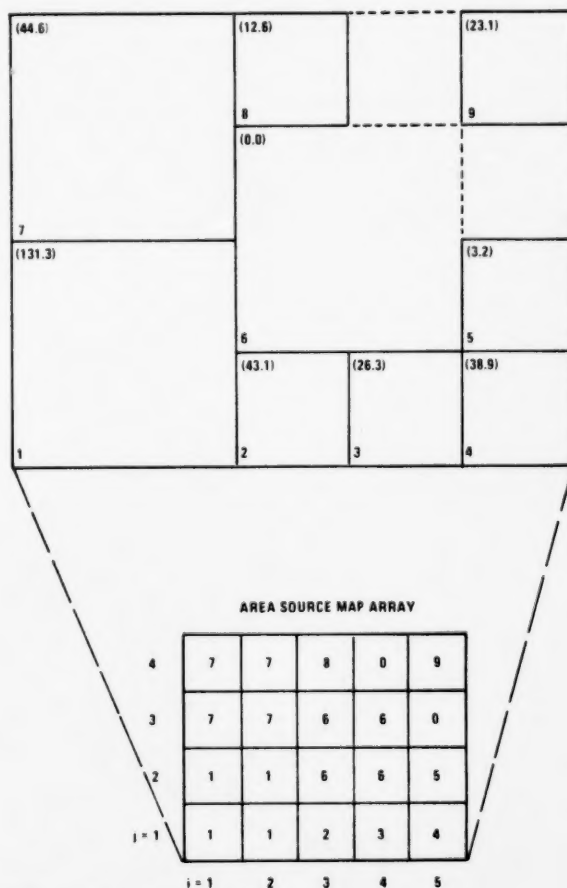


Figure 1. Plan view of area sources and area source map array.

in the Appendix. The dispersion parameter values, σ_y and σ_z are determined as a function of the upwind distance, x , and stability class (See p 374 of Pasquill⁴). The three equations used to estimate concentrations under various conditions of stability and mixing height (Equations A3, A4, and A5) are discussed in the Appendix. These equations are for a receptor height, z , above ground and simplify considerably when the receptor height is assumed to be at ground level, $z = 0$. (Those simplifications are incorporated into RAM.)

The total concentration at a receptor arising from the two-dimensional area-source distribution is calculated using the narrow plume simplification of Gifford and Hanna.⁵ This simplification is assumed because, on an urban scale, the plume from a point source release is normally quite narrow in comparison with the characteristic length scale for appreciable changes of the magnitude of the area-source emission rate itself. Under these circumstances the two-dimensional integral that expresses the total area-source contribution to concentration can be replaced approximately by a one-dimensional integral that only involves knowledge of the distribution of the area-source emissions along the line in the direction of the upwind azimuth from the receptor location, and the meteorologically-dependent function that specifies the crosswind-integrated concentration in the Gaussian plume from a point source. Further evidence for the validity of this approximation for treating area-source concentrations has been provided by some numerical tests of Thayer and Koch.⁶

In the use of this area source technique by Gifford and Hanna,⁵ area source emissions were assumed at ground level allowing integration upwind to be accomplished analytically. However, in our application of this technique within RAM, the area sources are considered to have an effective height, thus requiring the integration to be accomplished numerically. The equations used to estimate concentrations from area sources (Eq. A10 through A13) are given in the Appendix. The total concentration from all area sources is determined by performing the integration in the upwind direction until the farthest boundary of the source region is reached.

Concentrations at a receptor for periods longer than 1 hr are determined by averaging the hourly concentrations over the period of interest.

How Computations Are Made

Initially, a preprocessor program is used to store the emission inventory in a convenient form and perform any necessary conversions. A most important function of the preprocessor is to arrange the area sources in such a way as to minimize computation time for area source concentrations. Each area source number (area sources are numbered sequentially as the sources are input) is stored in a two dimensional array which essentially forms a map of the relative locations of all the area sources. Each element in the array corresponds to an area the size of a unit square (previously defined). Therefore a unit source will have its source number stored into one element of the array, whereas an area source that is 4 units by 4 units will have its source number stored into 16 elements of the array (4×4). Obviously area sources must be mutually exclusive; they must not overlap. Array elements corresponding to areas of the source region not covered by area sources will have a zero stored in the array. As will be explained later, it is to the advantage of the user to define areas 2×2 units or larger with no emissions as specific source areas with zero emissions (source 6, Figure 1). An example of a simplified source region and the resulting array are shown in Figure 1.

Concentration estimates are made hour-by-hour for up to 24 hr. This algorithm is not designed to determine average

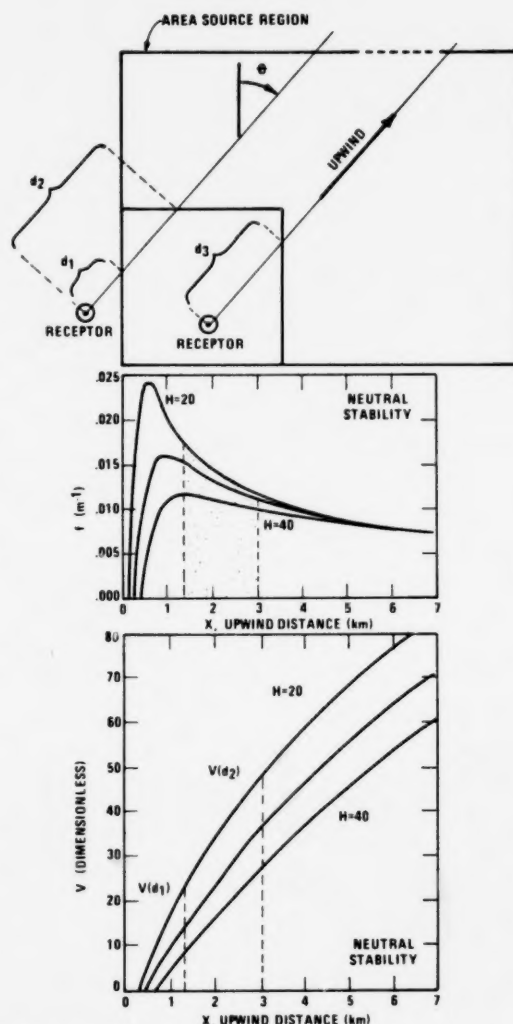


Figure 2. Features of area source estimates.

concentrations over periods longer than 24 hr. First, concentrations resulting from area sources are calculated. In an effort to reduce the total amount of computer time, tables (arrays) which contain relative concentrations, V , normalized for emission rate and wind speed, are calculated only once for each simulated hour using the appropriate stability and mixing height, and thereby eliminating all repetitive calculations. The function V is calculated from:

$$V(d) = \int_0^d f \, dx \quad (1)$$

and is the non-dimensional concentration resulting from an area source of given effective height extending upwind from a receptor to the distance, d . The function f , whose form depends on stability, and mixing height, is defined in the Appendix (Eq. A11, A12, and A13). The stored tables contain values of this integral obtained by numerical integration for a number of values of d . Both f and V for 3 area source heights are shown in Figure 2. Because $V(d)$ changes rapidly for small values of d , the numerical integration using the trapezoidal rule is done using varying size intervals, as small as 1 meter

for x less than 100 meters, and as large as 1 km for x greater than 15 km. The values of V are also stored for varying intervals of d (ranging from 10 m to 1 km), so that linear interpolation between stored values will result in an accurate estimate of V . For each effective area source height, up to a maximum of three, a V table is generated and stored at the beginning of each simulated hour.

The concentrations from the area sources are computed receptor by receptor. If the receptor is outside the source region (the rectangular region containing all the area sources), it is first determined if the upwind ray (the line pointed in the wind direction) intersects the source region. If it does not intersect the source region, no contribution from area sources at this receptor is calculated. If the upwind ray does intersect the source region, the distance, d_1 , (See Figure 2) along the ray to the source region is determined using Eq. A6 and A8 in the Appendix. The coordinates of this intersection point and consideration of wind direction provide direct access, through the area source map array, to the source number of the particular area source at this intersection point. Since all other source information is stored in arrays indexed on source number, the area source location (coordinates of SW corner), size, effective height, and emission rate are readily available.

Knowledge of the location and size of the area source permits the calculation of the intersection point of the upwind ray from the receptor with the area source boundary on the other side of the source (See Equations A6 through A9 in Appendix) and subsequently the calculation of distance (d_2) from the receptor to this point (Figure 2). These two distances, d_1 and d_2 , are then used to obtain linearly interpolated values of V from the tables, $V(d_2)$ and $V(d_1)$. The concentration from this source (assume this is source number i) is then given by:

$$\chi_{Ai} = (q_{Ai}/u)[V(d_2) - V(d_1)] \quad (2)$$

where χ_{Ai} is the concentration at the receptor from the i th area source, q_{Ai} is the area source emission rate from the i th area source, and u is the mean wind speed. $V(d_1)$ is subtracted since it represents the area source contribution not present. If, however, the emission rate is zero or the source number stored in the area source map array is zero, the source does not contribute to the concentration, but the intersection with the boundary and the distance to this intersection is determined as before.

After estimating the contribution of this area source to the receptor, the coordinates at the boundary furthest from the receptor are used to determine the next adjacent source entered by the upwind ray. The procedures are then repeated for this source and all other sources until the boundary of the area source region is reached by working upwind along the upwind ray.

In the case where the receptor is initially within the area source region, the coordinates of the receptor are used to determine within which area source the receptor lies. If the source number is zero, indicating no source area, the intersection point of the upwind ray and the upwind boundary of a unit square is determined and computation proceeds as above. If the receptor is within a numbered source area, the intersection point of the upwind ray and the upwind area source boundary, see Figure 2, as well as the distance, d_3 , to this point are determined. Then by interpolation in the V table corresponding to the appropriate area source height, the contribution to the concentration is computed as follows:

$$\chi_{Ai} = (q_{Ai}/u)V(d_3) \quad (3)$$

The next area source upwind is determined and computations proceed for the other upwind sources as above. The advantage

of specifying large areas of no emission, rather than leave them numbered as zero in the area source map array, is that the intersection of the upwind ray and the far boundary can be determined directly rather than stepping across a number of unit squares.

After the influence of area sources upon all receptors is calculated for a simulated hour the contribution from point sources is determined. Concentrations from point sources are also calculated receptor by receptor; and for each receptor, calculations are made source by source. The upwind distance, x , of the point source from the receptor is determined for this hour from the coordinates of the point source, the coordinates of the receptor, and the wind direction (See Eq. A1 in the Appendix). If this distance is negative, the source does not contribute to the receptor and the next source is examined. However, if the upwind distance is positive, the crosswind distance, y , and the ratio y/σ_y are determined next. If y/σ_y is greater than 10, the factor g_1 (See Appendix) is always so small that the contribution from this point source to the receptor is negligible. But with y/σ_y less than 10 an additional test must be made to see if the concentration is significant. If the factor g_1 multiplied by the point source emission rate is less than some specified threshold concentration, no further calculations are made for this source.

In most cases the concentration is above the threshold, and plume rise must be calculated for the source being considered provided that it was not calculated previously for estimates at another receptor for this simulated hour. A table of final plume heights and distance to the final rise is filled in as plume rise calculations are required, thus final plume rise is calculated only once for each source for each hour's simulation. If the upwind distance of the source from the receptor, x , is less than the distance to final plume rise, the gradual rise of the plume from stack top to final rise is considered, and the plume height at this nearer distance is used for estimates for this receptor. After the appropriate plume rise is obtained, the concentration at the receptor from this point source is calculated using the equation appropriate for stability class and mixing height as discussed in the Appendix. Concentrations from other point sources are similarly determined. Similar procedures are repeated then for each of the other receptors.

The total concentration at a receptor is the sum of the concentrations from area sources and from point sources. If any background concentration exists that is caused by sources outside the source region, it must be added to the concentration estimates from RAM.

Options

Three options are available regarding use of receptor locations in RAM. The first option allows coordinates of specific receptors to be entered as input.

Use of the second receptor option allows the user to specify how many significant point and how many significant area sources he wants to consider. The model then calculates the location of the maximum concentration from each significant point source using a plume rise calculation, the resultant wind direction, and the most frequently occurring (modal) stability class during the period modeled (24 hr or less). (It is not desirable to use this option if there are significant shifts of the wind during the period modeled, because the resultant direction will not represent the mean transport.) A receptor is located at the estimated point of maximum from each significant source, and another in the same direction but twice as far away. A receptor at this second distance may also have high concentrations for cases of overlapping plumes from several sources. Using this second receptor option there are two receptors established for each significant point source.

The second receptor option also determines the location of a single receptor downwind of each significant area source. Since the effective height of area sources are generally lower than point sources, the maximum concentration from the area source is calculated quite near the boundary of the source.

The location of the maximum concentrations from specific point and area sources will, of course, not necessarily be a location where the contribution from all sources will result in a maximum. Since the location of the maxima are highly dependent upon the dispersion parameter values, σ_y and σ_z , any modification of the algorithm that changes the way in which these dispersion parameters are calculated will also require extensive modifications to the subroutines, which determine the maximum distances from point and area sources, if the second receptor option is to be used.

The third receptor option allows for good area coverage of a specified portion of the region. The boundaries of the region to be covered and the spacing between receptors, w , are specified by the user. In order to cover the maximum area with the fewest number of stations, a hexagonal or 'honeycomb' grid is used. Receptor locations are at equal distances from nearby receptors so that if lines are drawn to all nearby receptors, six equilateral triangles will result. Also in order to keep the total number of receptors to a minimum, any potential receptor locations generated by the third option are deleted if they are within one-half w of any other existing receptor.

Several other options available are mainly used to delete special output when not required. These options are not as significant as the receptor options and will not be discussed here.

Summary

RAM is a steady state Gaussian algorithm applicable to urban areas for pollutants emitted from point and area sources. Calculations are made for one-hour time periods. Average concentrations may be obtained for time periods up to 24 hr.

Estimation of concentrations from point sources is straightforward. Briggs' plume rise equations are used. Upwind and crosswind distances of each source from each receptor are determined and concentration is estimated from various Gaussian equations.

Innovative techniques are used in keeping the number of receptors to a minimum and in the treatment of the area emission inventory. Except for the area source map array used for coordinating area source number with location, area source information is stored and used directly for a number of possible source sizes. A narrow plume simplification with consideration of source height of each area is used. The emission rates of the area sources in the source region along the upwind azimuth are considered representative of the area emission rates affecting the receptor from various distances upwind (narrow plume hypothesis). Determination, at the beginning of each simulated hour, of the effect of area sources extending to different distances upwind are stored in tabular form with a different table for each effective area source height (up to 3 heights allowed). Linear interpolation of these tabular values for each source, and receptor by receptor, to obtain concentrations from area sources saves considerable computer time.

The various receptor options in the model allow for versatility in the use of RAM. Coordinates corresponding to fixed locations, such as air quality sampling locations may be used. In attempting to estimate maximum concentrations for particular short-term periods, the option to select locations

downwind of particularly significant sources can be used. To insure good area coverage, an option is available to select additional receptors equally spaced from each other. These equally spaced receptors cover a particular defined region and are added only if other receptors have not been located in the vicinity of each proposed receptor location.

A user's guide for RAM is under preparation. One version of this algorithm has been applied to a 3-month urban data base related to sulfur dioxide. In order to assess the validity of the model, comparisons of these estimates with measurements are being accomplished by a group under Dr. Patrick Hamill at Clark College in Atlanta. It is anticipated that the algorithm will soon be made available to users as part of EPA's User's Network for Applied Modeling of Air Pollution (UNAMAP).

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Appendix

Dispersion and Analytic Geometry Equations Used in RAM

Expressions

These expressions are used in the discussions that follow:

$$g_1 = \exp(-0.5y^2/\sigma_y^2)$$

$$g_2 = \exp[-0.5(z - H)^2/\sigma_z^2] + \exp[-0.5(z + H)^2/\sigma_z^2]$$

$$g_3 = \sum_{N=-\infty}^{\infty} \{ \exp[-0.5(z - H + 2NL)^2/\sigma_z^2] + \exp[-0.5(z + H + 2NL)^2/\sigma_z^2] \}$$

(This infinite series converges rapidly and evaluation with N varying from -4 to $+4$ is usually sufficient.)

where

- H = effective height of emission, meters
- L = mixing height, the top of the unstable layer, meters
- y = crosswind distance, meters
- z = receptor height above ground, meters
- σ_y = standard deviation of plume concentration distribution in the horizontal, meters
- σ_z = standard deviation of plume concentration distribution in the vertical, meters

Point Source Computations

The upwind distance, x , and the crosswind distance, y , of a point source from a receptor are given by:

$$x = (S_p - S_r) \cos \theta + (R_p - R_r) \sin \theta \quad (\text{A1})$$

$$y = (S_p - S_r) \sin \theta - (R_p - R_r) \cos \theta \quad (\text{A2})$$

where R_p, S_p are the coordinates of the point source; R_r, S_r are the coordinates of the receptor, and θ is the wind direction (the direction from which the wind blows). The units of x and y will be the same as those of the coordinate system R, S . Frequently a conversion is required in order to express x , and y in meters or kilometers.

The contribution to the concentration, χ_p , from a single point source to a receptor is given by one of the three following equations where χ_p is in g m^{-3} , Q is point source emission rate in g sec^{-1} , u is wind speed in m sec^{-1} , and σ_y and σ_z are evaluated for the upwind distance x , and the stability class.

For stable conditions or unlimited mixing:

$$\chi_p = Qg_1g_2/(2\pi\sigma_y\sigma_zu) \quad (\text{A3})$$

In unstable or neutral conditions and if σ_z is greater than 1.6 times the mixing height, L , the distribution below the mixing height is uniform with height provided that both the effective height, H , and the receptor height, z , are below the mixing height:

$$\chi_p = Qg_1/[\sigma_yLu(2\pi)^{1/2}] \quad (\text{A4})$$

(If H or z is above the mixing height, $\chi_p = 0$.)

In all other unstable or neutral conditions, that is, if σ_z is less than 1.6 times the mixing height:

$$\chi_p = Qg_1g_3/(2\pi\sigma_y\sigma_zu) \quad (\text{A5})$$

Area Source Computations

Some analytic geometry relationships are used in estimating concentrations from area sources.

The distance, d_1 , along an upwind ray in the direction θ from a receptor R_r, S_r to a north-south boundary given by $R = R_b$ is:

$$d_1 = (R_b - R_r)/\sin \theta \quad (\text{A6})$$

The east coordinate of the locus of the boundary and the upwind ray is, of course, R_b . The north coordinate of this in-

tersection is:

$$S_L = S_r + d_1 \cos \theta \quad (\text{A7})$$

The distance, d_2 , along an upwind ray in the direction θ from a receptor R_r, S_r to an east-west boundary given by $S = S_b$ is:

$$d_2 = (S_b - S_r)/\cos \theta \quad (\text{A8})$$

The north coordinate of the locus of the boundary and the upwind ray is, S_b . The east coordinate of this intersection is:

$$R_L = R_r + d_2 \sin \theta \quad (\text{A9})$$

(Depending upon the units of the coordinate system R, S , the results of these equations may have to be multiplied by a factor to convert to meters).

The contribution of the concentration, χ_A , from a uniform area source directly upwind of a receptor is:

$$\chi_A = (q_A/u) \int_{x_1}^{x_2} f dx \quad (\text{A10})$$

where χ_A is in g m^{-3} , q_A is area source emission rate in $\text{g sec}^{-1} \text{m}^{-2}$, u is wind speed in m sec^{-1} , x_1 is the distance in meters from the receptor to the locus of the upwind ray (extending from the receptor) and the closest boundary of the area source, x_2 is the distance in meters from the receptor to the locus of the upwind ray (extending from the receptor) and the distant boundary of the area source, and f is given by one of the three equations below. The integral in the preceding equation is evaluated numerically.

For stable conditions or unlimited mixing:

$$f = g_2/[\sigma_z(2\pi)^{1/2}] \quad (\text{A11})$$

In unstable or neutral conditions and if σ_z is greater than 1.6 times the mixing height, L , the distribution below the mixing height is uniform with height provided that both the effective height, H , and the receptor height, z , are below the mixing height:

$$f = 1/L \quad (\text{A12})$$

(If H or z is above the mixing height, $f = 0$.)

In all other unstable or neutral conditions, that is, if σ_z is less than 1.6 times the mixing height:

$$F = g_3/[\sigma_z(2\pi)^{1/2}] \quad (\text{A13})$$